

OK RT

### SCOUR ANALYSIS AND REPORTING FORM

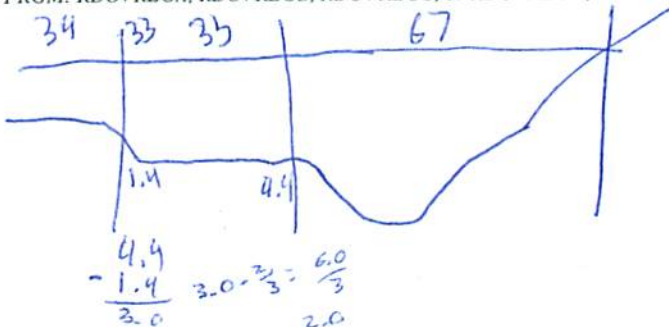
Bridge Structure No. 14103090 Date 5/28/12 Initials RAT Region (A B C D) C  
 Site \_\_\_\_\_ Location 16.6 mi N of Vermillion on 306 St  
 $Q_{100} =$  1120 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 1120 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 67 ft. Flow angle at bridge = 480 ° Abut. Skew = 0 ° Effective Skew = 40 °  
 Width ( $W_2$ ) iteration = ~~51.32~~ ~~40.6~~ 42.9  
 Avg. flow depth at bridge,  $y_2$  iteration = ~~6.6~~ ~~7.9~~ 7.2  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 42.9 ft\*  $q_2 = Q_2/W_2 =$  26.1 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  3.6 ft/s Final  $y_2 = q_2/V_2 =$  7.2 ft  $\Delta h =$  0.3 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  7.5 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 1ft ft  
 Low Steel Elev. = 11.6 ft  
 $n$  (Channel) = 0.045  
 $n$  (LOB) = ~~0.045~~  
 $n$  (ROB) = 0.040  
 Pier Width = 1.9 ft  
 Pier Length = 1.9 ft  
 # Piers for 100 yr = 2 ft



#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 =$  67 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  67 ft Average left overbank flow depth,  $y_{lob} =$  3.4 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  0 ft Average right overbank flow depth,  $y_{rob} =$  0 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  8.79 From Figure 9  $W_2$  (effective) = 39.1 ft  $y_{cs} =$  9.7 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} >= 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} >= D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

#### PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.24 Using pier width  $a$  on Figure 11,  $\xi =$  7.7 Pier scour  $y_{ps} =$  6.2 ft

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} =$  3.4 ft right abutment,  $y_{aRT} =$  0 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  12.2 and  $\psi_{RT} =$  0  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) =$  12.2 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) =$  0 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pier

PGRM: Abutment



**SCOUR ANALYSIS AND REPORTING FORM**

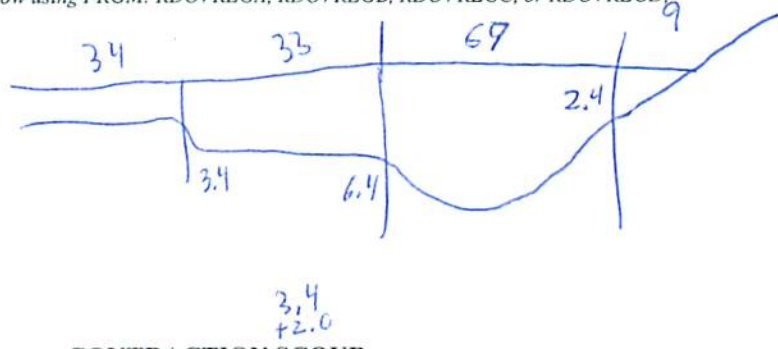
Bridge Structure No. 14103090 Date 5/28/12 Initials RAI Region (A B C D) C  
 Site \_\_\_\_\_ Location 11.6 mi N of Vermillion on 306 St  
 $Q_{500} =$  2140 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 2140 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 67 ft. Flow angle at bridge = 90 ° Abut. Skew = 0 ° Effective Skew = 40 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_  
 Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 51.32 ft\*  $q_2 = Q_2/W_2 =$  41.7 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  4.2 ft/s Final  $y_2 = q_2/V_2 =$  9.1 ft  $\Delta h =$  0.4 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  9.5 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD

Water Surface Elev. = 154 ft  
 Low Steel Elev. = 11.6 ft  
 $n$  (Channel) = 0.045  
 $n$  (LOB) = 0.045  
 $n$  (ROB) = 0.040  
 Pier Width = 1.9 ft  
 Pier Length = 1.9 ft  
 # Piers for 500 yr = 2 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  67 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  67 ft Average left overbank flow depth,  $y_{lob} =$  5.4 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  9 ft Average right overbank flow depth,  $y_{rob} =$  2.4 ft  
 Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  9.32 From Figure 9  $W_2$  (effective) = 47.5 ft  $y_{cs} =$  10.2 ft (with  $3.6 \cdot 2.5$  and  $10.5$  noted)

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2/y_1)^{7/6} =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.27 Using pier width  $a$  on Figure 11,  $\xi =$  7.7 Pier scour  $y_{ps} =$  6.3 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  5.4 ft right abutment,  $y_{aRT} =$  2.4 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  15.7 and  $\psi_{RT} =$  9.8  
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  15.7 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  9.8 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pie

PGRM: Abutment

Route 306 St Stream Vermillion River Overflow MRM \_\_\_\_\_ Date 5/28/12 Initials RAT

Bridge Structure No. 14103090 Location 11.6 mi N of Vermillion on 306 St

GPS coordinates: N 42° 57' 13.0" taken from: USL abutment  centerline of  MRM end \_\_\_\_\_  
W 96° 57' 31.5" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 7.65 sq. mi.

The average bottom of the main channel was 15.4 ft below top of guardrail at a point 43 ft from left abutment.

Method used to determine flood flows: \_\_\_\_\_ Freq. Anal. \_\_\_\_\_ drainage area ratio 1 regional regression equations.

5/22  
8/23

**MISCELLANEOUS CONSIDERATIONS**

Flows	Q <sub>100</sub> = <u>1120</u>			Q <sub>500</sub> = <u>2140</u>		
Estimated flow passing through bridge	<u>1120</u>			<u>2140</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>0</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Chance of Pressure flow		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

2 | 54  
5 | 169  
10 | 303  
25 | 555  
50 | 807  
100 | 1120  
500 | 2140

Riprap at abutments?  Yes \_\_\_\_\_ No \_\_\_\_\_ Marginal  
 Evidence of past Scour?  Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know  
 Debris Potential? \_\_\_\_\_ High \_\_\_\_\_ Med  Low

*contraction, abutment*

Does scour countermeasure(s) appear to have been designed?  
 Riprap  Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know \_\_\_\_\_ NA  
 Spur Dike \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know \_\_\_\_\_ NA  
 Other \_\_\_\_\_  Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know \_\_\_\_\_ NA

*- loose quartz*  
*trees on right bank*

**Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)**

Material Silt/Clay  Sand \_\_\_\_\_ Gravel \_\_\_\_\_ Cobbles \_\_\_\_\_ Boulders \_\_\_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos  
 1). main channel  
 2). right abutment  
 3). right ab  
 4). piers  
 5). abutment scour (left)  
 6). left ab  
 7). left ab  
 8). right ab  
 9). left OB  
 10). right OB  
 11). main channel  
 12). left OB  
 13). right OB

*Note: higher water mark is around 2ft below low steel. This is around the level of Q<sub>500</sub>.*

**Summary of Results**

	Q100	Q500
Bridge flow evaluated	<u>1120</u>	<u>2140</u>
Flow depth at left abutment (yaLT), in feet	<u>3.4</u>	<u>6.4</u>
Flow depth at right abutment (yaRT), in feet	<u>0</u>	<u>2.4</u>
Contraction scour depth (yca), in feet	<u>4.7</u>	<u>10.5 10.2</u>
Pier scour depth (yca), in feet	<u>6.2</u>	<u>6.3</u>
Left abutment scour depth (yas), in feet	<u>12.2</u>	<u>13.7</u>
Right abutment scour depth (yas), in feet	<u>0</u>	<u>9.8</u>
Flow angle of attack	<u>40</u>	<u>40</u>

See Comments/Diagram for justification where required