

OK RT

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 14109030 Date 5/25/12 Initials rch Region (A B C D)
Site Q50 Location 46290 300 St, Vermillion River
Q100 = 11780 by: drainage area ratio w flood freq. anal. regional regression eq. X
Bridge discharge (Q2) = 17000 11300 (should be Q100 unless there is a relief bridge, road overflow, or bridge overtopping)

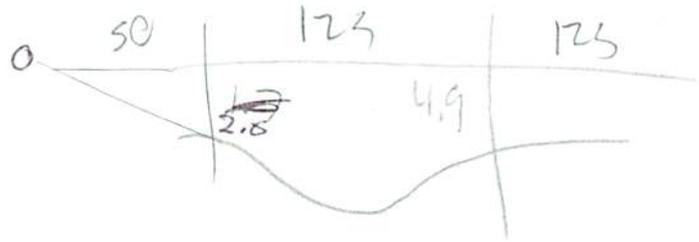
Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 125 ft. Flow angle at bridge = 10 degrees Abut. Skew = 0 degrees Effective Skew = 10 degrees
Width (W2) iteration = 123.1
Avg. flow depth at bridge, y2 iteration = 16.6
Corrected channel width at bridge Section = W2 times cos of flow angle = 123.1 ft\* q2 = Q2/W2 = 91.8 ft^2/s
Bridge Vel, V2 = 6.8 ft/s Final y2 = q2/V2 = 13.5 ft Delta h = 0.9 ft
Average main channel depth at approach section, y1 = Delta h + y2 = 14.5 ft

\* NOTE: repeat above calculations until y2 changes by less than 0.2 Effective pier width = L sin(q) + a cos(q)
If y2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0-4K ft
Low Steel Elev. = 22+15.9 ft
n (Channel) = 0.050
n (LOB) = 0.060 0.085
n (ROB) = 0.060 0.055
Pier Width = 1.4 ft
Pier Length = 1.4 ft
# Piers for 100 yr = 2 ft

11.6
26.8
4.7
15.9



CONTRACTION SCOUR

Width of main channel at approach section W1 = 125 ft
Width of left overbank flow at approach, Wlob = 50 ft Average left overbank flow depth, ylob = 1.3 ft
Width of right overbank flow at approach, Wrob = 125 ft Average right overbank flow depth, yrob = 4.9 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)
x = 2.88 From Figure 9 W2 (effective) = 120.3 ft ycs = 3.5 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)
Estimated bed material D50 = ft Average approach velocity, V1 = Q100/(y1W1) = ft/s
Critical approach velocity, Vc = 11.52y1^1/6 D50^1/3 = ft/s
If V1 < Vc and D50 >= 0.2 ft, use clear water equation below, otherwise use live bed scour equation above.
Dc50 = 0.0006(q2/y1^7/6)^3 = ft If D50 >= Dc50, chi = 0.0
Otherwise, chi = 0.122y1[q2/(D50^1/3 y1^7/6)]^6/7 - y1 = From Figure 10, ycs = ft

PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1), K2 = 1
Froude # at bridge = 0.33 Using pier width a on Figure 11, xi = 6.1 Pier scour yps = 5.2 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, yaLT = 1.3 ft right abutment, yaRT = 4.9 ft
Shape coefficient K1 = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
Using values for yaLT and yaRT on figure 12, psiLT = 5.5 and psiRT = 14.8
Left abutment scour, yas = psiLT(K1/0.55) = 5.5 ft Right abutment scour yas = psiRT(K1/0.55) = 14.8 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pier

PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

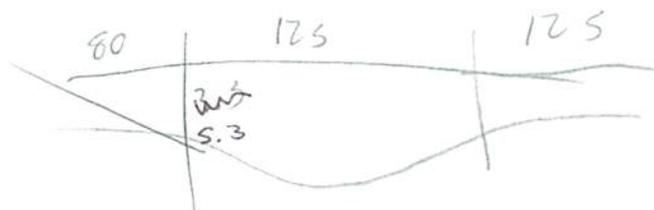
Bridge Structure No. 14109030 Date 5/25/12 Initials R. Al Region (A B C D)  
 Site \_\_\_\_\_ Location 46290 300 S+  
 $Q_{500} = \frac{37100}{323001700}$  by: drainage area ratio WV flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 50264 15653 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 123.1 ft. Flow angle at bridge = 10 ° Abut. Skew = 0 ° Effective Skew = 10 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_  
 Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 123.1 ft\*  $q_2 = Q_2/W_2 = \underline{177.2}$  ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 = \underline{8}$  ft/s Final  $y_2 = q_2/V_2 = \underline{15.9}$  ft  $\Delta h = \underline{1.3}$  ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = \underline{17.2}$  ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. 0-4ft ft  
 Low Steel Elev. = 15.9 ft  
 n (Channel) = 0.050  
 n (LOB) = 0.085  
 n (ROB) = 0.055  
 Pier Width = 6.4 ft  
 Pier Length = 1.4 ft  
 # Piers for 500 yr = 2 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 = \underline{123}$  ft  
 Width of left overbank flow at approach,  $W_{lob} = \underline{80}$  ft Average left overbank flow depth,  $y_{lob} = \frac{2.6 + 2.7}{5.3} = \underline{2.7}$  ft  
 Width of right overbank flow at approach,  $W_{rob} = \underline{123}$  ft Average right overbank flow depth,  $y_{rob} = \frac{4.9 + 7.1}{11.0} = \underline{7.6}$  ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x = \underline{5.14}$  From Figure 9  $W_2$  (effective) = 120.3 ft  $y_{cs} = \underline{5.8}$  ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 = \underline{1}$   
 Froude # at bridge = 0.35 Using pier width a on Figure 11,  $\xi = \underline{6.1}$  Pier scour  $y_{ps} = \underline{5.2}$  ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} = \underline{2.7}$  ft right abutment,  $y_{aRT} = \underline{7.6}$  ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = \underline{11}$  and  $\psi_{RT} = \underline{19.5}$   
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) = \underline{11}$  ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) = \underline{19.5}$  ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Pie

PRGM: Abutment

Route 300 St Stream Vermillion River MRM \_\_\_\_\_ Date 5/25/12 Initials RAT  
 Bridge Structure No. 14109030 Location 46290 300 St  
 GPS coordinates: N 43° 2' 24.9" E taken from: USL abutment  centerline of ↑ MRM end \_\_\_\_\_  
W 96° 56' 37.1" W Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 1536.34 sq. mi. 006  
 The average bottom of the main channel was 56.8 ft below top of guardrail at a point 43 ft from left abutment.  
 Method used to determine flood flows: \_\_\_\_\_ Freq. Anal.  drainage area ratio  regional regression equations.

<sup>Q<sub>50</sub></sup>  
**MISCELLANEOUS CONSIDERATIONS** <sup>Q<sub>100</sub></sup>

Flows	Q <sub>100</sub> = <del>18500</del> 11300			Q <sub>500</sub> = <del>32300</del> 17000		
Estimated flow passing through bridge	11300			15653		
Estimated road overflow & overtopping	0			1347		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>
Chance of Pressure flow		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

5/22  
 2 | 332  
 5 | 1530  
 10 | 3270  
 25 | 7080  
 50 | 11300  
 100 | 17000  
 500 | 37100

Riprap at abutments?  Yes \_\_\_\_\_ No \_\_\_\_\_ Marginal \_\_\_\_\_  
 Evidence of past Scour?  Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know <sup>piec contract</sup> \_\_\_\_\_  
 Debris Potential? \_\_\_\_\_ High  Med \_\_\_\_\_ Low \_\_\_\_\_

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know \_\_\_\_\_ NA  
 Spur Dike \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know \_\_\_\_\_ NA  
 Other \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know \_\_\_\_\_ NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay  Sand \_\_\_\_\_ Gravel \_\_\_\_\_ Cobbles \_\_\_\_\_ Boulders \_\_\_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos  
 1. Main channel      9. LAB  
 2. L. ab              10. LAB  
 3. Piers              11. ROB  
 4. ROB              12. ROB  
 5. Main channel      13. Main channel

Summary of Results

	<del>Q<sub>100</sub></del> Q <sub>50</sub>	<del>Q<sub>500</sub></del> Q <sub>100</sub>
Bridge flow evaluated	11300	<del>174</del> 15653
Flow depth at left abutment (yaLT), in feet	1.3	2.7
Flow depth at right abutment (yaRT), in feet	4.4	7.6
Contraction scour depth (ycs), in feet	3.5	5.9
Pier scour depth (yps), in feet	5.2	8.2 5.2
Left abutment scour depth (yas), in feet	5.5	11
Right abutment scour depth (yas), in feet	14.9	19.5
IFlow angle of attack	10	10

See Comments/Diagram for justification where required