

OK RT

### SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 14112090 Date 5/28/12 Initials RT Region (A B C D) D  
 Site \_\_\_\_\_ Location 46320 306 St, Vermillion River  
 $Q_{100} = 19500$  <sup>Q<sub>100</sub> 8876</sup> by: drainage area ratio dammed flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 8876 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 154 ft. Flow angle at bridge = 0 ° Abut. Skew = 0 ° Effective Skew = 0 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_

Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_

Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 154 ft\*  $q_2 = Q_2/W_2 = 57.6$  ft<sup>2</sup>/s

Bridge Vel,  $V_2 = 5.4$  ft/s Final  $y_2 = q_2/V_2 = 10.7$  ft  $\Delta h = 0.6$  ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = 11.3$  ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0-1.5 ft 16.0  
 Low Steel Elev. = 14.1 ft 3.9  
 $n$  (Channel) = 0.075  
 $n$  (LOB) = 0.085  
 $n$  (ROB) = 0.030  
 Pier Width = 1.9 ft  
 Pier Length = 1.9 ft  
 # Piers for 100 yr = 4



#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 = 170$  ft

Width of left overbank flow at approach,  $W_{lob} = 0$  ft Average left overbank flow depth,  $y_{lob} = 0$  ft

Width of right overbank flow at approach,  $W_{rob} = 0$  ft Average right overbank flow depth,  $y_{rob} = 0$  ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x = 1.82$  From Figure 9  $W_2$  (effective) = 146.4 ft  $y_{cs} = 2.3$  ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 1.48 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006(q_2/y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

#### PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 = 1$   
 Froude # at bridge = 0.29 Using pier width  $a$  on Figure 11,  $\xi = 7.7$  Pier scour  $y_{ps} = 6.4$  ft

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} = 0$  ft right abutment,  $y_{aRT} = 0$  ft  
 Shape coefficient  $K_1 = 1.00$  for vertical-wall,  $0.82$  for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = 0$  and  $\psi_{RT} = 0$   
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) = 0$  ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) = 0$  ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pier

PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 14112090 Date 5/28/12 Initials RAT Region (A B C D) C

Site \_\_\_\_\_ Location 46320 306 S+

$Q_{500} =$ ~~34000~~ <sup>16400</sup> by: drainage area ratio W flood freq. anal. \_\_\_\_\_ regional regression eq. X

Bridge discharge ( $Q_2$ ) = 15394 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 154 ft. Flow angle at bridge = 0 ° Abut. Skew = 0 ° Effective Skew = 0 °

Width ( $W_2$ ) iteration = \_\_\_\_\_

Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_

Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 154 ft\*  $q_2 = Q_2/W_2 =$ 100 ft<sup>2</sup>/s

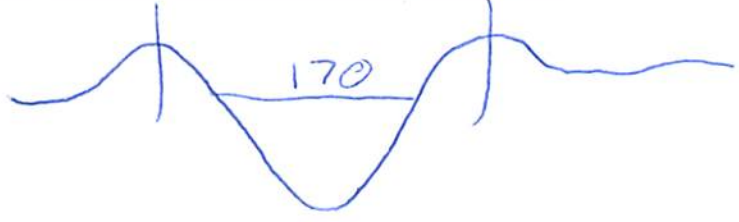
Bridge Vel,  $V_2 =$ 7.1 ft/s Final  $y_2 = q_2/V_2 =$ 14.1 ft  $\Delta h =$ 1 ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$ 15.1 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0-1.5ft ft  
 Low Steel Elev. = ~~14.1~~ ft  
 $n$  (Channel) = 0.075  
 $n$  (LOB) = 0.085  
 $n$  (ROB) = 0.030  
 Pier Width = 1.9 ft  
 Pier Length = 1.9 ft  
 # Piers for 500 yr = 4 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$ 170 ft

Width of left overbank flow at approach,  $W_{lob} =$ 0 ft Average left overbank flow depth,  $y_{lob} =$ 0 ft

Width of right overbank flow at approach,  $W_{rob} =$ 0 ft Average right overbank flow depth,  $y_{rob} =$ 0 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$ 243 From Figure 9  $W_2$  (effective) = 1464 ft  $y_{cs} =$ 3 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$ \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$ \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$ \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$ \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$ \_\_\_\_\_ From Figure 10,  $y_{cs} =$ \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$ 1

Froude # at bridge = 0.33 Using pier width  $a$  on Figure 11,  $\xi =$ 7.7 Pier scour  $y_{ps} =$ 6.5 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$ 0 ft right abutment,  $y_{aRT} =$ 0 ft

Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through

Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$ 0 and  $\psi_{RT} =$ 0

Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) =$ 0 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) =$ 0 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pie:

PGRM: Abutment

42.953533

96.94766



Route 306 St Stream Vermillion River MRM \_\_\_\_\_ Date 5/28/12 Initials RAT

Bridge Structure No. 14112090 Location 46320 306 St

GPS coordinates: N 42° 57' 12.8" taken from: USL abutment  centerline of ↑ MRM end \_\_\_\_\_  
W 96° 56' 49.4" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 1665.99 sq. mi.

The average bottom of the main channel was 16.0 ft below top of guardrail at a point 58 ft from left abutment.

Method used to determine flood flows: \_\_\_\_\_ Freq. Anal.  drainage area ratio  regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = <u>19500</u> Q <sub>10</sub> <u>8870</u>			Q <sub>500</sub> = <u>15399</u>		
Estimated flow passing through bridge	<u>8870</u>			<u>15399</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>1006</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>				<input checked="" type="checkbox"/>
Chance of Pressure flow		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

Q<sub>50</sub> Q<sub>25</sub> 16400

5/27  
5/22  
2 11.9 1750  
5 27.8 5050  
10 43.6 8870  
25 69.6 16400  
50 99 24300  
100 122 34600  
300 225 74000

Riprap at abutments?  Yes \_\_\_\_\_ No \_\_\_\_\_ Marginal - less than about half way up.  
 Evidence of past Scour?  Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know contraction  
 Debris Potential?  High \_\_\_\_\_ Med \_\_\_\_\_ Low - bridge entrances is blocked by a fallen trees.

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know \_\_\_\_\_ NA  
 Spur Dike \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know \_\_\_\_\_ NA  
 Other \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know \_\_\_\_\_ NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay  Sand \_\_\_\_\_ Gravel \_\_\_\_\_ Cobbles \_\_\_\_\_ Boulders \_\_\_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos  
1). main channel 7). main channel  
2). right abut 8). left ab  
3). right abut 9). main channel  
4). debris 10). left ab  
5). piers 11). left ab.  
6). right ab

Summary of Results

	Q <sub>100</sub> Q <sub>10</sub>	Q <sub>500</sub> Q <sub>25</sub>
Bridge flow evaluated	<u>8870</u>	<u>15399</u>
Flow depth at left abutment (yaLT), in feet	<u>0</u>	<u>0</u>
Flow depth at right abutment (yaRT), in feet	<u>0</u>	<u>0</u>
Contraction scour depth (ycs), in feet	<u>2.3</u>	<u>3</u>
Pier scour depth (yps), in feet	<u>6.4</u>	<u>6.5</u>
Left abutment scour depth (yas), in feet	<u>0</u>	<u>0</u>
Right abutment scour depth (yas), in feet	<u>0</u>	<u>0</u>
IFlow angle of attack	<u>0</u>	<u>0</u>

See Comments/Diagram for justification where required