

OK TRT

SCOUR ANALYSIS AND REPORTING FORM

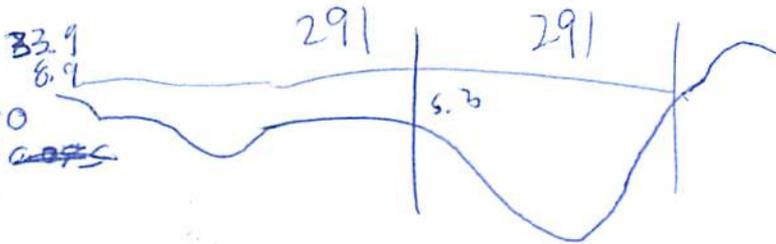
Bridge Structure No. 14117214 Date 5/27/12 Initials rat Region (A B C D) C
Site Location in Vermillion, 700 S. Dakota Ave Vermillion River
Q100 = 20300 40700 by: drainage area ratio flood freq. anal. regional regression eq.
Bridge discharge (Q2) = 40700 (should be Q100 unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 291 ft. Flow angle at bridge = 20 degrees Abut. Skew = 0 degrees Effective Skew = 20 degrees
Width (W2) iteration = 273.45 245.16 252.76 249.07
Avg. flow depth at bridge, y2 iteration = 17.2 16.9 18.2 17.9 18
Corrected channel width at bridge Section = W2 times cos of flow angle = 260.4 ft* 249.07 q2 = Q2/W2 = 163.4 ft^2/s
Bridge Vel, V2 = 9.1 ft/s Final y2 = q2/V2 = 18 ft Delta h = 1.7 ft
Average main channel depth at approach section, y1 = Delta h + y2 = 19.7 ft

* NOTE: repeat above calculations until y2 changes by less than 0.2 Effective pier width = L sin(q) + a cos(q)
If y2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD,

Water Surface Elev. = NA ft
Low Steel Elev. = 25 ft
n (Channel) = 0.060
n (LOB) = 0.075
n (ROB) = 0.075
Pier Width = 2.5 ft
Pier Length = 14.35 ft
Piers for 100 yr = 1



CONTRACTION SCOUR

Width of main channel at approach section W1 = 291 ft
Width of left overbank flow at approach, Wlob = 291 ft Average left overbank flow depth, ylob = 5.3 ft
Width of right overbank flow at approach, Wrob = 0 ft Average right overbank flow depth, yrob = 0 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

x = 5.29 From Figure 9 W2 (effective) = 2465 ft ycs = 6 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material D50 = ft Average approach velocity, V1 = Q100/(y1 W1) = ft/s

Critical approach velocity, Vc = 11.52 y1^1/6 D50^1/3 = ft/s

If V1 < Vc and D50 >= 0.2 ft, use clear water equation below, otherwise use live bed scour equation above.

Dc50 = 0.0006 (q2/y1^7/6)^3 = ft If D50 >= Dc50, chi = 0.0

Otherwise, chi = 0.122 y1 [q2 / (D50^1/3 y1^7/6)]^6/7 - y1 = From Figure 10, ycs = ft

PIER SCOUR CALCULATIONS

L/a ratio = 274 5.74 Correction factor for flow angle of attack (from Table 1), K2 = 1.85
Froude # at bridge = 0.38 Using pier width a on Figure 11, xi = 9.5 Pier scour yps = 15.2 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, yalT = 5.3 ft right abutment, yarT = 0 ft
Shape coefficient K1 = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
Using values for yalT and yarT on figure 12, psiLT = 15.6 and psiRT = 0
Left abutment scour, yas = psiLT (K1/0.55) = 15.6 ft Right abutment scour yas = psiRT (K1/0.55) = 0 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCSNEW

PGRM: Pier

PGRM: Abutment

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 14117214 Date 5/27/12 Initials Raj Region (A B C D) C
 Site _____ Location in Vermillion, 700 S. Dakota Ave.
 $Q_{500} =$ 36900 ⁹⁵¹⁰⁰ by: drainage area ratio flood freq. anal. _____ regional regression eq.
 Bridge discharge (Q_2) = 85100 (should be Q_{500} unless there is a relief bridge, road overflow, or bridge overtopping)

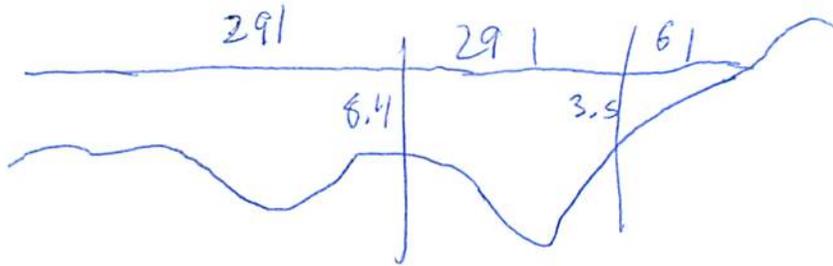
Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 291 ft. Flow angle at bridge = 20 ° Abut. Skew = 0 ° Effective Skew = 20 °
 Width (W_2) iteration = _____
 Avg. flow depth at bridge, y_2 iteration = _____

Corrected channel width at bridge Section = W_2 times cos of flow angle = 273.45 ft* $q_2 = Q_2/W_2 =$ 311.2 ft²/s
 Bridge Vel, $V_2 =$ 12.2 ft/s Final $y_2 = q_2/V_2 =$ 24.9 ft $\Delta h =$ 3.2 ft
 Average main channel depth at approach section, $y_1 = \Delta h + y_2 =$ 28.1 ft

* NOTE: repeat above calculations until y_2 changes by less than 0.2 Effective pier width = $L \sin(q) + a \cos(q)$
 If y_2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = - ft
 Low Steel Elev. = 25 ft
 n (Channel) = 0.060
 n (LOB) = 0.090
 n (ROB) = 0.075
 Pier Width = 2.5 ft
 Pier Length = 14.35 ft
 # Piers for 500 yr = 1 ft



CONTRACTION SCOUR

Width of main channel at approach section $W_1 =$ 291 ft
 Width of left overbank flow at approach, $W_{lob} =$ 291 ft Average left overbank flow depth, $y_{lob} =$ 8.4 ft
 Width of right overbank flow at approach, $W_{rob} =$ 61 ft Average right overbank flow depth, $y_{rob} =$ 3.5 ft
 $53 \frac{2}{3} = 10.6$

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$ 4.93 From Figure 9 W_2 (effective) = 271 ft $y_{cs} =$ 5.6 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material $D_{50} =$ _____ ft Average approach velocity, $V_1 = Q_{500}/(y_1 W_1) =$ _____ ft/s

Critical approach velocity, $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$ _____ ft/s

If $V_1 < V_c$ and $D_{50} \geq 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$ _____ ft If $D_{50} \geq D_{c50}$, $\chi = 0.0$

Otherwise, $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$ _____ From Figure 10, $y_{cs} =$ _____ ft

PIER SCOUR CALCULATIONS

L/a ratio = 5.24 Correction factor for flow angle of attack (from Table 1), $K_2 =$ 1.85
 Froude # at bridge = 0.43 Using pier width a on Figure 11, $\xi =$ 9.5 Pier scour $y_{ps} =$ 15.6 ^{15.5} ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, $y_{aLT} =$ 8.4 ft right abutment, $y_{aRT} =$ 3.5 ft

Shape coefficient $K_1 =$ 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through

Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} =$ 20.1 and $\psi_{RT} =$ 12.4

Left abutment scour, $y_{as} = \psi_{LT} (K_1 / 0.55) =$ 20.1 ft Right abutment scour $y_{as} = \psi_{RT} (K_1 / 0.55) =$ 12.4 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pie

PGRM: Abutment

Route S. Dak. Ave Stream Vermillion River MRM _____ Date 5/27/12 Initials Lat
 Bridge Structure No. 14117214 Location in Vermillion, 700 S. Dakota Ave
 GPS coordinates: N 42° 46' 24.0" taken from: USL abutment centerline of MRM end _____
W 16° 55' 51.0" Datum of coordinates: WGS84 NAD27 _____

Drainage area = 2115.53 sq. mi.
 The average bottom of the main channel was 33.9 ft below top of guardrail at a point 136 ft from left abutment.
 Method used to determine flood flows: _____ Freq. Anal. drainage area ratio regional regression equations.

MISCELLANEOUS CONSIDERATIONS

| | | | | | | |
|---------------------------------------|---------------------------------------|-------------------------------------|----------|---------------------------------------|-------------------------------------|-------------------------------------|
| Flows | Q ₁₀₀ = <u>20300 40700</u> | | | Q ₅₀₀ = <u>31800 85100</u> | | |
| Estimated flow passing through bridge | | | | <u>40700</u> | | |
| Estimated road overflow & overtopping | | | | <u>0</u> | | |
| Consideration | Yes | No | Possibly | Yes | No | Possibly |
| Chance of overtopping | | <input checked="" type="checkbox"/> | | <input checked="" type="checkbox"/> | | <input checked="" type="checkbox"/> |
| Chance of Pressure flow | | <input checked="" type="checkbox"/> | | <input checked="" type="checkbox"/> | | |
| Armored appearance to channel | | <input checked="" type="checkbox"/> | | | <input checked="" type="checkbox"/> | |
| Lateral instability of channel | | <input checked="" type="checkbox"/> | | | <input checked="" type="checkbox"/> | |

5/22
 2 | 1590
 5 | 5570
 10 | 9950
 25 | 18700
 50 | 25200
 100 | 40700
 500 | 85100

Riprap at abutments? Yes _____ No _____ Marginal riprap lines the right bank but is absent of the left side
 Evidence of past Scour? Yes _____ No _____ Don't know contraction
 Debris Potential? _____ High Med _____ Low

Does scour countermeasure(s) appear to have been designed?
 Riprap Yes _____ No _____ Don't know _____ NA rose quartz
 Spur Dike _____ Yes No _____ Don't know _____ NA riprap
 Other _____ Yes No _____ Don't know _____ NA riprap along right bank, flow on

Bed Material Classification Based on Median Particle Size (D₅₀) bank.
 Material Silt/Clay Sand _____ Gravel _____ Cobbles _____ Boulders _____
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos
 1) main channel
 2) right ab
 3) right ab
 4) pier
 5) pier
 6) left ab
 7) left ab
 8) left ab
 9) left ab
 10) main channel
 11) right ab
 12) right ab
 13) main channel

Note: the Q values used are from Stream Stats, and are higher than the Q₁₀₀ and Q₅₀₀ values produced by a drainage area ratio from a nearby gage.

Summary of Results

| | | |
|----------------------------------------------|--------------|------------------|
| | Q100 | Q500 |
| Bridge flow evaluated | <u>40700</u> | <u>85100</u> |
| Flow depth at left abutment (yaLT), in feet | <u>5.3</u> | <u>8.4</u> |
| Flow depth at right abutment (yaRT), in feet | <u>0</u> | <u>3.5</u> |
| Contraction scour depth (yca), in feet | <u>0</u> | <u>5.6</u> |
| Pier scour depth (yps), in feet | <u>15.2</u> | <u>15.6 15.5</u> |
| Left abutment scour depth (yas), in feet | <u>15.6</u> | <u>20.1</u> |
| Right abutment scour depth (yas), in feet | <u>0</u> | <u>12.4</u> |
| IFlow angle of attack | <u>20</u> | <u>20</u> |

See Comments/Diagram for justification where required