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**SCOUR ANALYSIS AND REPORTING FORM**

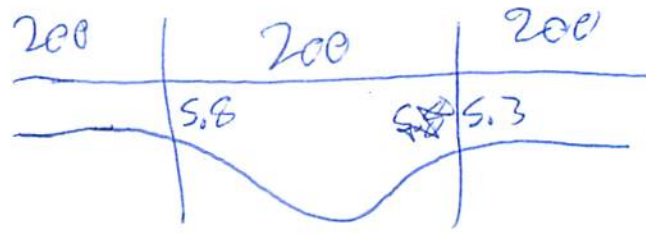
Bridge Structure No. 14120183 Date 5/27/12 Initials Lat Region (A B C D) C  
 Site 06479010 Location 31530 University Road, Vermillion River  
 $Q_{100} =$  1820036700 by: drainage area ratio      flood freq. anal.  regional regression eq.       
 Bridge discharge ( $Q_2$ ) =      (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 200 ft. Flow angle at bridge = 5 ° Abut. Skew = 0 ° Effective Skew = 5 °  
 Width ( $W_2$ ) iteration = 199.24 174.33 181.31 178.38  
 Avg. flow depth at bridge,  $y_2$  iteration = 19.1 20.5 20.1 20.2  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 199.24 ft\*  $q_2 = Q_2/W_2 =$  205.6 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  10.7 ft/s Final  $y_2 = q_2/V_2 =$  20.12 ft  $\Delta h =$  1.82 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  22.3 ft

\*NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = UNK ft 29.25  
 Low Steel Elev. = 24.9 ft 4.35  
 $n$  (Channel) = 0.070 27.90  
 $n$  (LOB) = 0.035  
 $n$  (ROB) = 0.035  
 Pier Width = 1.95 ft channel  
 Pier Length = 1.95 ft  
 # Piers for 100 yr = 4 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  200 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  200 ft Average left overbank flow depth,  $y_{lob} =$  5.8 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  200 ft Average right overbank flow depth,  $y_{rob} =$  5.3 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  14.17 From Figure 9  $W_2$  (effective) = 170.5 ft  $y_{cs} =$  14.5 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$       ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$       ft/s  
 Critical approach velocity,  $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$       ft/s  
 If  $V_1 < V_c$  and  $D_{50} >= 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2/y_1)^{7/6} =$       ft If  $D_{50} >= D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$       From Figure 10,  $y_{cs} =$       ft

**PIER SCOUR CALCULATIONS**

$L/a$  ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.4 Using pier width  $a$  on Figure 11,  $\xi =$  7.8 Pier scour  $y_{ps} =$  6.8 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  5.8 ft right abutment,  $y_{aRT} =$  5.3 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  16.5 and  $\psi_{RT} =$  15.6  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1/0.55) =$  16.5 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1/0.55) =$  15.6 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pier

PGRM: Abutment

### SCOUR ANALYSIS AND REPORTING FORM

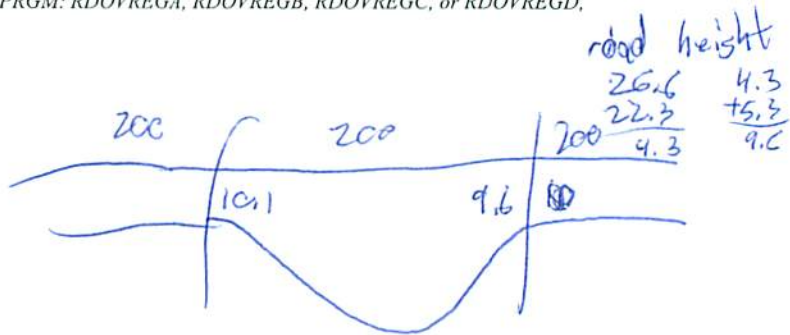
Bridge Structure No. 14120183 Date 5/27/12 Initials ReT Region (A B C D) \_\_\_\_\_  
 Site 06479010 Location 31530 University Road  
 $Q_{500} = \underline{33100}$  ~~74600~~ by: drainage area ratio \_\_\_\_\_ flood freq. anal.  regional regression eq.   
 Bridge discharge ( $Q_2$ ) = 62210 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 200 ft. Flow angle at bridge = 5 ° Abut. Skew = 0 ° Effective Skew = 5 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_  
 Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 199.24 ft\*  $q_2 = Q_2/W_2 = \underline{312.2}$  ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 = \underline{17.5}$  ft/s Final  $y_2 = q_2/V_2 = \underline{24.9}$  ft  $\Delta h = \underline{3.2}$  ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = \underline{28.1}$  ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(\alpha) + a \cos(\alpha)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = \_\_\_\_\_ ft  
 Low Steel Elev. = 24.9 ft  
 n (Channel) = 0.070  
 n (LOB) = 0.035  
 n (ROB) = 0.35  
 Pier Width = 1.95 ft  
 Pier Length = 1.95 ft  
 # Piers for 500 yr = 4



#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 = \underline{200}$  ft  
 Width of left overbank flow at approach,  $W_{lob} = \underline{200}$  ft Average left overbank flow depth,  $y_{lob} = \underline{10.1}$  ft  
 Width of right overbank flow at approach,  $W_{rob} = \underline{200}$  ft Average right overbank flow depth,  $y_{rob} = \underline{9.6}$  ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x = \underline{21.73}$  From Figure 9  $W_2$  (effective) = 191.4 ft  $y_{cs} = \underline{18.0}$  ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1)^{7/6} =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

#### PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 = \underline{1}$   
 Froude # at bridge = 0.44 Using pier width a on Figure 11,  $\xi = \underline{7.8}$  Pier scour  $y_{ps} = \underline{6.9}$  ft

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} = \underline{10.1}$  ft right abutment,  $y_{aRT} = \underline{9.2}$  ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = \underline{21.4}$  and  $\psi_{RT} = \underline{21}$   
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) = \underline{21.4}$  ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) = \underline{21}$  ft

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PGRM: Pie

PGRM: Abutment



Route University Rd Stream Vermillion River MRM Date 5/27/12 Initials RaT

Bridge Structure No. 14120183 Location 31530 University Road

GPS coordinates: N 42° 49' 14" taken from: USL abutment  centerline of  MRM end   
W: 96° 55' 27.2" Datum of coordinates: WGS84  NAD27

Drainage area = 1775.17 sq. mi.

The average bottom of the main channel was 29.25 ft below top of guardrail at a point 71 ft from left abutment.

Method used to determine flood flows:  Freq. Anal.  drainage area ratio  regional regression equations.

*from at-site frequency analysis*

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = <del>33100</del> <u>36700</u>	Q <sub>500</sub> = <del>33100</del> <u>74600</u>				
Estimated flow passing through bridge	<u>36700</u>	<u>62210</u>				
Estimated road overflow & overtopping	<del>36700</del> <u>0</u>	<u>12390</u>				
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Chance of Pressure flow		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

5/27

2	355
5	1670
10	3610
25	7900
50	12700
100	19200
500	42200

Notes: Flows from stream stats do not match previous values upstream are lower than upstream values. I will use up stream numbers also much less than downstream numbers. Form 1413046

2	1910
5	5410
10	9480
25	17400
50	23000
100	36700
500	74600

~2 miles upst. com

Riprap at abutments?  Yes  No  Marginal *yes, on left abutment and bank, no on right*  
 Evidence of past Scour?  Yes  No  Don't know *piers, contraction*  
 Debris Potential?  High  Med  Low

Does scour countermeasure(s) appear to have been designed?

Riprap  Yes  No  Don't know  NA  
 Spur Dike  Yes  No  Don't know  NA  
 Other  Yes  No  Don't know  NA *tees along both banks, riprap along right bank*

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay  Sand  Gravel  Cobbles  Boulders   
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

1) main channel 7) left OB  
 2) piers 8) main channel  
 3) pier scour 9) right OB  
 4) left ab 10) left OB  
 5) left ab 11) right OB  
 6) right ab 12) main channel

Note: Q values used in this analysis are based on Stream Stats results and are larger than the Q<sub>100</sub> and Q<sub>500</sub> values determined for the stream gage at this location.

Summary of Results

	Q100	Q500
Bridge flow evaluated	<u>36700</u>	<u>62210</u>
Flow depth at left abutment (yaLT), in feet	<u>5.8</u>	<u>10.1</u>
Flow depth at right abutment (yaRT), in feet	<u>5.3</u>	<u>9.6</u>
Contraction scour depth (yca), in feet	<u>14.5</u>	<u>18.6</u>
Pier scour depth (yps), in feet	<u>6.8</u>	<u>6.9</u>
Left abutment scour depth (yas), in feet	<u>16.3</u>	<u>21.4</u>
Right abutment scour depth (yas), in feet	<u>15.6</u>	<u>21</u>
IFlow angle of attack	<u>5</u>	<u>5</u>

See Comments/Diagram for justification where required