

OK RT

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 15184181 Date 8/16/10 Initials CW Region (A B C D)
Site Location Big Sixes River on South Broadway in Watertown
Q100 = 6170 by: drainage area flood frequency anal. regional regression eq.
Bridge discharge (Q2) = 3992 (should be Q100 unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 96 ft. Flow angle at bridge = 0 degrees Abut. Skew = 0 degrees Effective Skew = 0 degrees
Width (W2) iteration = 96

Avg. flow depth at bridge, y2 iteration = 11.3

Corrected channel width at bridge Section = W2 times cos of flow angle = 96 ft* q2 = Q2/W2 = 41.6 ft^2/s

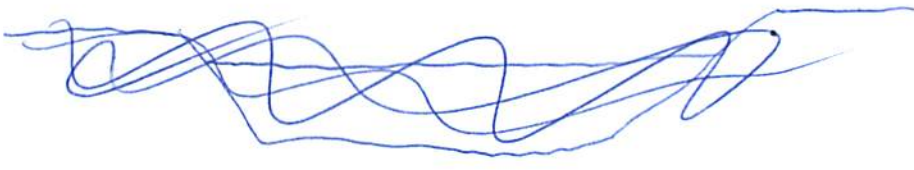
Bridge Vel, V2 = 4.6 ft/s Final y2 = q2/V2 = 9.1 ft Dh = 0.4 ft

Average main channel depth at approach section, y1 = Dh + y2 = 9.5 ft

* NOTE: repeat above calculations until y2 changes by less than 0.2 Effective pier width = L sin(q) + a cos(q)
If y2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD,

Water Surface Elev. =
Low Steel Elev. = 9.1 ft
n (Channel) = 0.033
n (LOB) = 0.050
n (ROB) = 0.030
Pier Width = 1.2 ft
Pier Length = 1.2 ft
Piers for 100 yr = 2

Road over flow ymax = 9.1 ft
Q = 3992



CONTRACTION SCOUR

Width of main channel at approach section W1 = 118 ft Average left overbank flow depth, ylob = 0.5 ft
Width of left overbank flow at approach, Wlob = 60 ft Average right overbank flow depth, yrob = 4.5 ft
Width of right overbank flow at approach, Wrob = 96 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)
x = 5.59 From Figure 9 W2 (effective) = 93.6 ft ycs = 6.3 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)
Estimated bed material D50 = Average approach velocity, V1 = Q100/(y1 W1) =
Critical approach velocity, Vc = 11.52 y1^1/6 D50^1/3 =
If V1 < Vc and D50 >= 0.2 ft, use clear water equation below, otherwise use live bed scour equation above.
Dc50 = 0.0006 (q2/y1^7/6)^3 = If D50 >= Dc50, chi = 0.0
Otherwise, chi = 0.122 y1 [q2 / (D50^1/3 y1^7/6)]^6/7 - y1 = From Figure 10, ycs =

PIER SCOUR CALCULATIONS

L/a ratio = 1.0 Correction factor for flow angle of attack (from Table 1), K2 = 1.0
Froude # at bridge = 0.27 Using pier width a on Figure 11, xi = 5.5 Pier scour yps = 4.5 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, yalT = 0.5 ft right abutment, yarT = 4.5 ft
Shape coefficient K1 = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
Using values for yalT and yarT on figure 12, psiLT = 2.3 and psiRT = 14.1
Left abutment scour, yas = psiLT (K1/0.55) = 4.2 ft Right abutment scour yas = psiRT (K1/0.55) = 25.7 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCSNEW

PGRM: Pier

PGRM: Abutment

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 15184181 Date 8/16/10 Initials CW Region (A B C D) C
 Site _____ Location Big Sioux River on South Broadway in Watertown
 $Q_{500} = \underline{4200}$ 10100 by: drainage area flood frequency anal. _____ regional regression eq. _____
 Bridge discharge (Q_2) = 3992 (should be Q_{500} unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 96 ft. Flow angle at bridge = 0° Abut. Skew = 0° Effective Skew = 0°
 Width (W_2) iteration = 96
 Avg. flow depth at bridge, y_2 iteration = 9.1

Corrected channel width at bridge Section = W_2 times cos of flow angle = 96 ft* $q_2 = Q_2/W_2 = \underline{41.6}$ ft²/s
 Bridge Vel, $V_2 = \underline{9.6}$ ft/s Final $y_2 = q_2/V_2 = \underline{9.1}$ ft $\Delta h = \underline{0.4}$ ft
 Average main channel depth at approach section, $y_1 = \Delta h + y_2 = \underline{9.5}$ ft

* NOTE: repeat above calculations until y_2 changes by less than 0.2 Effective pier width = $L \sin(q) + a \cos(q)$
 If y_2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Road over flow $y_{max} = 9.1' \rightarrow Q = 3992$

Water Surface Elev. = _____ ft
 Low Steel Elev. = 9.1 ft
 n (Channel) = 0.033
 n (LOB) = 0.050
 n (ROB) = 0.030
 Pier Width = 1.2 ft
 Pier Length = 1.2 ft
 # Piers for 500 yr = 2



CONTRACTION SCOUR

Width of main channel at approach section $W_1 = \underline{118}$ ft
 Width of left overbank flow at approach, $W_{lob} = \underline{60}$ ft Average left overbank flow depth, $y_{lob} = \underline{0.5}$ ft
 Width of right overbank flow at approach, $W_{rob} = \underline{96}$ ft Average right overbank flow depth, $y_{rob} = \underline{4.5}$ ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x = \underline{5.59}$ From Figure 9 W_2 (effective) = 93.6 ft $y_{cs} = \underline{6.3}$ ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material $D_{50} =$ _____ ft Average approach velocity, $V_1 = Q_{500}/(y_1 W_1) =$ _____ ft/s

Critical approach velocity, $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$ _____ ft/s

If $V_1 < V_c$ and $D_{50} \geq 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1)^{7/6} =$ _____ ft If $D_{50} \geq D_{c50}$, $\chi = 0.0$

Otherwise, $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$ _____ From Figure 10, $y_{cs} =$ _____ ft

PIER SCOUR CALCULATIONS

L/a ratio = 1.0 Correction factor for flow angle of attack (from Table 1), $K_2 = \underline{1.0}$
 Froude # at bridge = 0.27 Using pier width a on Figure 11, $\xi = \underline{5.5}$ Pier scour $y_{ps} = \underline{4.5}$ ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, $y_{aLT} = \underline{0.5}$ ft right abutment, $y_{aRT} = \underline{4.5}$ ft
 Shape coefficient $K_1 = \underline{1.00}$ for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
 Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} = \underline{2.3}$ and $\psi_{RT} = \underline{14.1}$
 Left abutment scour, $y_{as} = \psi_{LT} (K_1/0.55) = \underline{4.2}$ ft Right abutment scour $y_{as} = \psi_{RT} (K_1/0.55) = \underline{25.7}$ ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pie

PGRM: Abutment

Route S. Broadway Stream Big Sioux River MRM _____ Date 8/16/10 Initials AW
 Bridge Structure No. 15184181 Location in Watertown
 GPS coordinates: N 44°53'21.7" taken from: USL abutment X centerline of ↑ MRM end _____
W 97°07'08.5" Datum of coordinates: WGS84 X NAD27 _____
 Drainage area = 390.21 sq. mi.
 The average bottom of the main channel was 14.0 ft below top of guardrail at a point 31 ft from left abutment.
 Method used to determine flood flows: _____ Freq. Anal. ✓ drainage area adjustment _____ regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q ₁₀₀ = <u>6170</u>			Q ₅₀₀ = <u>9200 10100</u>		
Estimated flow passing through bridge	<u>3992</u>			<u>3992</u>		
Estimated road overflow & overtopping	<u>2178</u>			<u>6108</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping	<u>X</u>			<u>X</u>		
Chance of Pressure flow	<u>X</u>			<u>X</u>		
Armored appearance to channel			<u>X</u>			<u>X</u>
Lateral instability of channel		<u>X</u>			<u>X</u>	

Riprap at abutments? X Yes _____ No _____ Marginal
 Evidence of past Scour? X Yes _____ No _____ Don't know Appears cobbles have washed away
 Debris Potential? X High _____ Med _____ Low Sloping abut., washed away

Does scour countermeasure(s) appear to have been designed?

Riprap X Yes _____ No _____ Don't know _____ NA
 Spur Dike X Yes _____ No _____ Don't know _____ NA
 Other _____ Yes _____ No _____ Don't know X NA

Bed Material Classification Based on Median Particle Size (D₅₀)

Material Silt/Clay _____ Sand _____ Gravel X Cobbles _____ Boulders _____
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

1084 - Upstream 1048 - Bridge ID
1085 - US RB Both 100+ 500 year floods top
1086 - US LB bridge + spur dike
1047 - Bridge from
Approach XS

Summary of Results

	Q100	Q500
Bridge flow evaluated	<u>3992</u>	<u>3992</u>
Flow depth at left abutment (yaLT), in feet	<u>0.5</u>	<u>0.5</u>
Flow depth at right abutment (yaRT), in feet	<u>4.5</u>	<u>4.5</u>
Contraction scour depth (yca), in feet	<u>6.3</u>	<u>6.3</u>
Pier scour depth (yps), in feet	<u>4.5</u>	<u>4.5</u>
Left abutment scour depth (yas), in feet	<u>4.2</u>	<u>4.2</u>
Right abutment scour depth (yas), in feet	<u>25.7</u>	<u>25.7</u>
Flow angle of attack	<u>0</u>	<u>0</u>

See Comments/Diagram for justification where required