

OK RT

### SCOUR ANALYSIS AND REPORTING FORM

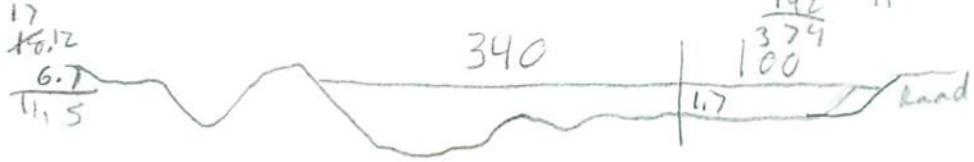
Bridge Structure No. 15196190 Date 7/31/12 Initials RAJ Region (A B C D) C  
 Site \_\_\_\_\_ Location Big Sioux River on 20<sup>th</sup> Ave S in Watertown  
 $Q_{100} =$  6220 6810 by: drainage area  flood frequency anal. \_\_\_\_\_ regional regression eq.   
 Bridge discharge ( $Q_2$ ) = 6810 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 374 ft. Flow angle at bridge = 55 ° Abut. Skew = 45 ° Effective Skew = 10 °  
 Width ( $W_2$ ) iteration = 374 327 331 \_\_\_\_\_  
 Avg. flow depth at bridge,  $y_2$  iteration = 6.1 6.5 6.5 \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 325.97 ft\*  $q_2 = Q_2/W_2 =$  20.9 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  3.2 ft/s Final  $y_2 = q_2/V_2 =$  6.5 ft  $\Delta h =$  0.2 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  6.7 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(a) + a \cos(a)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 07 ft 17  
 Low Steel Elev. = 11.5 ft 6.7  
 $n$  (Channel) = 0.045  
 $n$  (LOB) = 0.030  
 $n$  (ROB) = 0.030  
 Pier Width = 2.2 ft  
 Pier Length = 2.2 ft  
 # Piers for 100 yr = 3 ft



#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 =$  340 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  0 ft Average left overbank flow depth,  $y_{lob} =$  0 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  100 ft Average right overbank flow depth,  $y_{rob} =$  1.7 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  0.75 From Figure 9  $W_2$  (effective) = 319.4 ft  $y_{cs} =$  1.2 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

#### PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.22 Using pier width a on Figure 11,  $\xi =$  8.6 Pier scour  $y_{ps} =$  6.9 ft

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} =$  0 ft right abutment,  $y_{aRT} =$  1.7 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  0 and  $\psi_{RT} =$  7  
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  0 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  7 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pier

PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

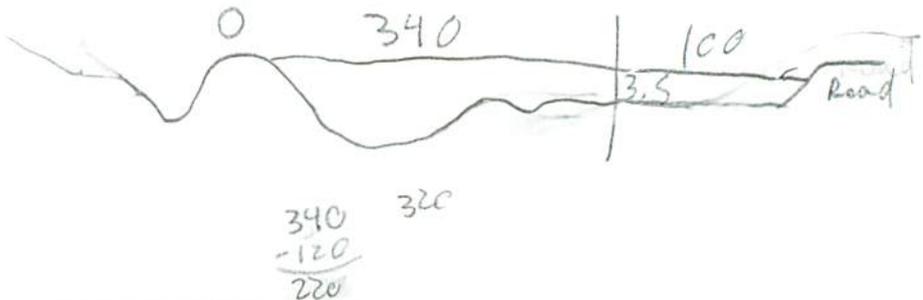
Bridge Structure No. 15196190 Date 7/31/12 Initials RAJ Region (A B C D) C  
 Site 11200 Location Big Sioux River on 20th Ave S in Watertown  
 $Q_{500} =$  9130 / 10180 by: drainage area X flood frequency anal.      regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 11200 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 374 ft. Flow angle at bridge = 55 ° Abut. Skew = 45 ° Effective Skew = 10 °  
 Width ( $W_2$ ) iteration = 374 336 340  
 Avg. flow depth at bridge,  $y_2$  iteration = 7.8 8.2 8.2  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 334.63 ft\*  $q_2 = Q_2/W_2 =$  33.4 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  4.1 ft/s Final  $y_2 = q_2/V_2 =$  8.2 ft  $\Delta h =$  0.3 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  8.5 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0-1 ft  
 Low Steel Elev. = 11.5 ft  
 $n$  (Channel) = 0.045  
 $n$  (LOB) = 0.030  
 $n$  (ROB) = 0.030  
 Pier Width = 2.2 ft  
 Pier Length = 22 ft  
 # Piers for 500 yr = 3 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  340 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  0 ft Average left overbank flow depth,  $y_{lob} =$  0 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  100 ft Average right overbank flow depth,  $y_{rob} =$  3.5 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  1.19 From Figure 9  $W_2$  (effective) = 328.3 ft  $y_{cs} =$  1.7 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$       ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$       ft/s

Critical approach velocity,  $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$       ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 =$       ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$       From Figure 10,  $y_{cs} =$       ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.25 Using pier width  $a$  on Figure 11,  $\xi =$  8.0 Pier scour  $y_{ps} =$  7 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  0 ft right abutment,  $y_{aRT} =$  3.5 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  0 and  $\psi_{RT} =$  12.4  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1/0.55) =$  0 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1/0.55) =$  12.4 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pie

PGRM: Abutment

7923'11  
7926'02

470 5' 51.6"  
440 52' 35.6"

Route 20<sup>th</sup> Ave S Stream Big Sioux River MRM \_\_\_\_\_ Date 7/3/12 Initials Lat

Bridge Structure No. 15196190 Location Watertown

GPS coordinates: N 44° 52' 35.7" taken from: USL abutment  centerline of  $\uparrow$  MRM end \_\_\_\_\_  
W 97° 5' 51.1" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 396.125 sq. mi.

The average bottom of the main channel was 19.2 ft below top of guardrail at a point 226 ft from left abutment.

Method used to determine flood flows: \_\_\_ Freq. Anal.  drainage area adjustment  regional regression equations.

MISCELLANEOUS CONSIDERATIONS

11200

713

Flows	Q <sub>100</sub> = <u>6220</u> <del>6010</del> <u>6010</u>			Q <sub>500</sub> = <u>9130</u> <del>10180</del>		
Estimated flow passing through bridge	<u>6010</u>			<u>11200</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>0</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Chance of Pressure flow		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

2 | 517  
 5 | 1440  
 10 | 2350  
 25 | 3860  
 50 | 5240  
 100 | 6810  
 500 | 11200

Riprap at abutments?  Yes \_\_\_ No \_\_\_ Marginal  
 Evidence of past Scour?  Yes \_\_\_ No \_\_\_ Don't know *minor pier/contraction*  
 Debris Potential? \_\_\_ High \_\_\_ Med  Low

Does scour countermeasure(s) appear to have been designed?

Riprap  Yes \_\_\_ No \_\_\_ Don't know \_\_\_ NA  
 Spur Dike \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Other \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay  Sand \_\_\_ Gravel \_\_\_ Cobbles \_\_\_ Boulders \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

- 1). left ab
- 2). main channel
- 3). right ab
- 4). pier
- 5). pier scour
- 6-7). left abutment
- 8-9). right abutment
- 10). main channel

Note: Profile taken w 325ft from right abutment

Summary of Results

	Q100	Q500
Bridge flow evaluated	<u>6810</u>	<u>11200</u>
Flow depth at left abutment (yaLT), in feet	<u>0</u>	<u>0</u>
Flow depth at right abutment (yaRT), in feet	<u>1.7</u>	<u>3.5</u>
Contraction scour depth (yca), in feet	<u>1.2</u>	<u>1.7</u>
Pier scour depth (yps), in feet	<u>6.9</u>	<u>7</u>
Left abutment scour depth (yas), in feet	<u>0</u>	<u>0</u>
Right abutment scour depth (yas), in feet	<u>7</u>	<u>12.4</u>
Flow angle of attack	<u>10</u>	<u>10</u>

See Comments/Diagram for justification where required