

# Grand River

## SCOUR ANALYSIS AND REPORTING FORM

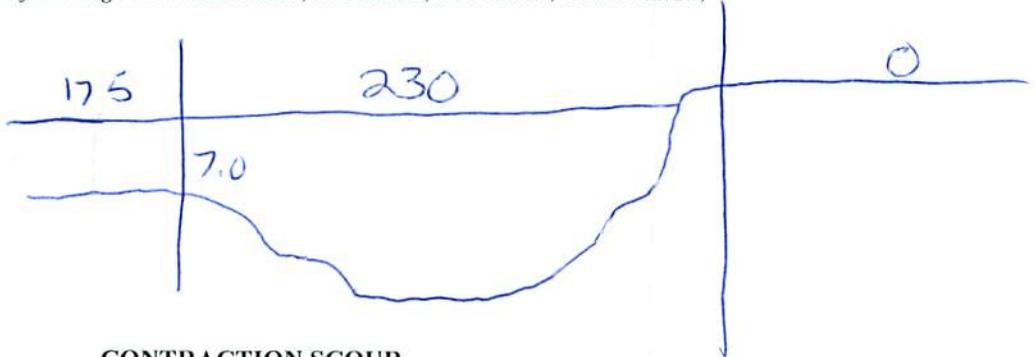
Bridge Structure No. 16149190 Date 10/29/11 Initials CE Region (A B C D) B  
 Site \_\_\_\_\_ Location On 222 Ave? S of Morristown  
 $Q_{100} =$  41,100 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq.   
 Bridge discharge ( $Q_2$ ) = 41100 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 175 ft. Flow angle at bridge = 3 ° Abut. Skew = 0 ° Effective Skew = 3 °  
 Width ( $W_2$ ) iteration = 175 172  
 Avg. flow depth at bridge,  $y_2$  iteration = 19.0 19.1  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 171.76 ft\*  $q_2 = Q_2/W_2 =$  239.3 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  12.5 ft/s Final  $y_2 = q_2/V_2 =$  19.1 ft  $\Delta h =$  3.2 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  22.4 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = \_\_\_\_\_ ft  
 Low Steel Elev. = 20.9 ft  
 $n$  (Channel) = 0.043  
 $n$  (LOB) = 0.050  
 $n$  (ROB) = 0.035  
 Pier Width = 2.4 ft  
 Pier Length = 23 ft  
 # Piers for 100 yr = 2 ft



### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 =$  230 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  175 ft Average left overbank flow depth,  $y_{lob} =$  7.0 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  0 ft Average right overbank flow depth,  $y_{rob} =$  0 ft

### Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  11.36 From Figure 9  $W_2$  (effective) = 167 ft  $y_{cs} =$  12.4 ft

### Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

### PIER SCOUR CALCULATIONS

L/a ratio = 9.58 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  ~1.4  
 Froude # at bridge = 0.5 Using pier width  $a$  on Figure 11,  $\xi =$  9.2 Pier scour  $y_{ps} =$  11.7 ft

### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} =$  7.0 ft right abutment,  $y_{aRT} =$  0 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  18.6 and  $\psi_{RT} =$  0  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) =$  18.6 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) =$  0 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pier

PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 16149190 Date 10/29/11 Initials CW Region (A B C D) B  
 Site \_\_\_\_\_ Location on 222 Ave? Sof Morristown  
 $Q_{500} = 66300$  by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq.   
 Bridge discharge ( $Q_2$ ) = 49470 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 175 ft. Flow angle at bridge = 3 ° Abut. Skew = 0 ° Effective Skew = 3 °  
 Width ( $W_2$ ) iteration = 175

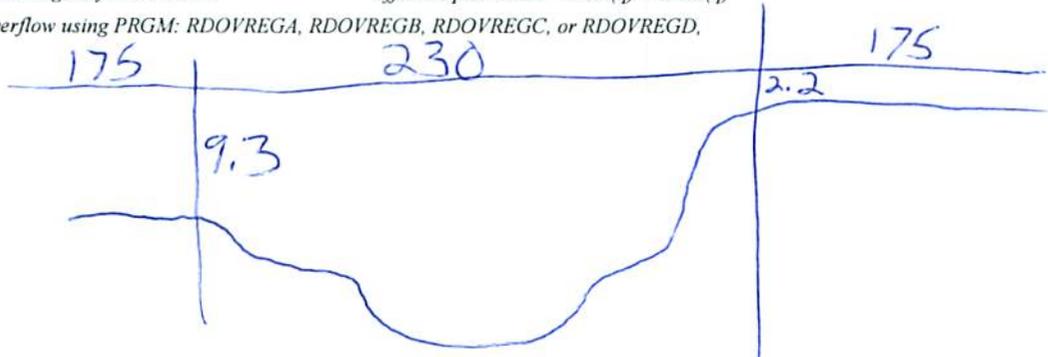
Avg. flow depth at bridge,  $y_2$  iteration = 24.4 → RD overflow  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 174.76 ft\*  $q_2 = Q_2/W_2 = 283.1$  ft<sup>2</sup>/s

Bridge Vel,  $V_2 = 13.5$  ft/s Final  $y_2 = q_2/V_2 = 20.9$  ft  $\Delta h = 3.5$  ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = 24.7$  ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = \_\_\_\_\_ ft  
 Low Steel Elev. = 20.9 ft  
 $n$  (Channel) = 0.043  
 $n$  (LOB) = 0.050  
 $n$  (ROB) = 0.045  
 Pier Width = 2.4 ft  
 Pier Length = 23 ft  
 # Piers for 500 yr = 2 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 = 230$  ft  
 Width of left overbank flow at approach,  $W_{lob} = 175$  ft Average left overbank flow depth,  $y_{lob} = 9.3$  ft  
 Width of right overbank flow at approach,  $W_{rob} = 175$  ft Average right overbank flow depth,  $y_{rob} = 2.2$  ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x = 13.45$  From Figure 9  $W_2$  (effective) = 170 ft  $y_{cs} = 14.2$  ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} >= 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} >= D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 9.58 Correction factor for flow angle of attack (from Table 1),  $K_2 = 1.4$   
 Froude # at bridge = 1.65 Using pier width  $a$  on Figure 11,  $\xi = 9.2$  Pier scour  $y_{ps} = 13.9$  ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{alT} = 9.3$  ft right abutment,  $y_{arT} = 2.2$  ft  
 Shape coefficient  $K_1 = 1.00$  for vertical-wall,  $0.82$  for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{alT}$  and  $y_{arT}$  on figure 12,  $\psi_{LT} = 20.8$  and  $\psi_{RT} = 9.0$   
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) = 20.8$  ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) = 9.0$  ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Pie

PRGM: Abutment

Route 222 Ave? Stream ~~Delaware~~ Grand River MRM \_\_\_\_\_ Date 10/29/11 Initials CW  
 Bridge Structure No. 16149190 Location On 222 Ave? S of Morristown  
 GPS coordinates: N45° 40' 32.5" taken from: USL abutment  centerline of  $\uparrow$  MRM end \_\_\_\_\_  
W101° 41' 50.7" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 3947.9 sq. mi.  
 The average bottom of the main channel was 25.6 ft below top of guardrail at a point 46 ft from left abutment.  
 Method used to determine flood flows: \_\_\_\_\_ Freq. Anal. \_\_\_\_\_ drainage area ratio  regional regression equations.

**MISCELLANEOUS CONSIDERATIONS**

Flows	Q <sub>100</sub> = <u>41100</u>			Q <sub>500</sub> = <u>66300</u>		
Estimated flow passing through bridge	<u>41100</u>			<u>49470</u>		
Estimated road overflow & overtopping				<u>16830</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Chance of Pressure flow			<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>
Armored appearance to channel	<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>		
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

Riprap at abutments?  Yes  No  Marginal Concrete lined channel / not riprap  
 Evidence of past Scour?  Yes  No  Don't know Banks up and downstream  
 Debris Potential?  High  Med  Low not @ bridge

Does scour countermeasure(s) appear to have been designed?  
 Riprap  Yes  No  Don't know  NA  
 Spur Dike  Yes  No  Don't know  NA  
 Other \_\_\_\_\_  Yes  No  Don't know  NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)  
 Material Silt/Clay  Sand  Gravel \_\_\_\_\_ Cobbles \_\_\_\_\_ Boulders \_\_\_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

10/4/11

2	2780
5	8690
10	15100
25	23800
50	32100
100	41100
500	66300

Photos  
2140-1D  
 81- US  
 82- USRB  
 83- USLB  
 84- L. Abut  
 85- R. Abut  
 86- US Face  
 87- LB App XS  
 88- RB App XS

**Summary of Results**

	Q100	Q500
Bridge flow evaluated	<u>41100</u>	<u>49470</u>
Flow depth at left abutment (yaLT), in feet	<u>7.0</u>	<u>9.3</u>
Flow depth at right abutment (yaRT), in feet	<u>0.0</u>	<u>2.2</u>
Contraction scour depth (yca), in feet	<u>12.4</u>	<u>14.2</u>
Pier scour depth (yp), in feet	<u>11.7</u>	<u>13.9</u>
Left abutment scour depth (yas), in feet	<u>14.6</u>	<u>20.8</u>
Right abutment scour depth (yas), in feet	<u>0.0</u>	<u>9.0</u>
Flow angle of attack	<u>3.</u>	<u>3</u>

See Comments/Diagram for justification where required