

SCOUR ANALYSIS AND REPORTING FORM

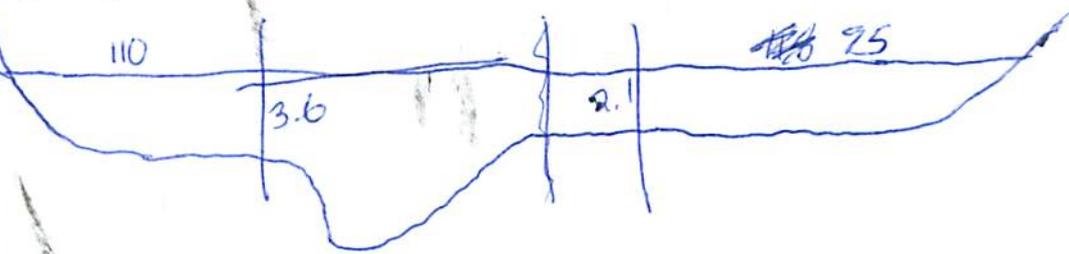
Bridge Structure No. 16582080 Date 8/9/11 Initials CLW Region (A B C D) C  
 Site \_\_\_\_\_ Location 1 mi N + 0.2 mi E of McLaughlin on IRR 108 St  
 $Q_{100} = 6390$  by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq.   
 Bridge discharge ( $Q_2$ ) = 6390 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 58 ft. Flow angle at bridge = 0 ° Abut. Skew = 0 ° Effective Skew = 0 °  
 Width ( $W_2$ ) iteration = 158 84 93 88 89  
 Avg. flow depth at bridge,  $y_2$  iteration = 7.5 10.5 9.9 10.2 10.2  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 89 ft\*  $q_2 = Q_2/W_2 = 71.8$  ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 = 7.1$  ft/s Final  $y_2 = q_2/V_2 = 10.2$  ft  $\Delta h = 1.0$  ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = 11.2$  ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = \_\_\_\_\_ ft  
 Low Steel Elev. = \_\_\_\_\_ ft  
 n (Channel) = 0.035  
 n (LOB) = 0.050  
 n (ROB) = 0.050  
 Pier Width = 3.0 ft  
 Pier Length = 3.0 ft  
 # Piers for 100 yr = 2 ft



CONTRACTION SCOUR

Width of main channel at approach section  $W_1 = 160$  ft  
 Width of left overbank flow at approach,  $W_{lob} = 110$  ft Average left overbank flow depth,  $y_{lob} = 2.7$  ft  
 Width of right overbank flow at approach,  $W_{rob} = 95$  ft Average right overbank flow depth,  $y_{rob} = 1.5$  ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x = 11.69$  From Figure 9  $W_2$  (effective) = 83 ft  $y_{cs} = 12.7$  ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

PIER SCOUR CALCULATIONS

L/a ratio = 1.0 Correction factor for flow angle of attack (from Table 1),  $K_2 = 1.0$   
 Froude #. at bridge = 0.31 Using pier width a on Figure 11,  $\xi = 10.7$  Pier scour  $y_{ps} = 7.3$  ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} = 2.9$  ft right abutment,  $y_{aRT} = 1.5$  ft  
 Shape coefficient  $K_1 = 1.00$  for vertical-wall,  $0.82$  for vertical-wall with wingwalls,  $0.55$  for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = 11.0$  and  $\psi_{RT} = 6.3$   
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) = 11.0$  ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) = 6.3$  ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pier

PGRM: Abutment

3.6  
5.4  
4.5  
18.1  
11.2  
5.4  
2.9  
45.1  
2.9  
3.2  
2.10  
2.25  
10.5  
5.9  
2.10  
6.0

3  
1.50  
0.75  
47.50  
6650  
7.1250  
2.10  
0.75  
250  
1470  
14950

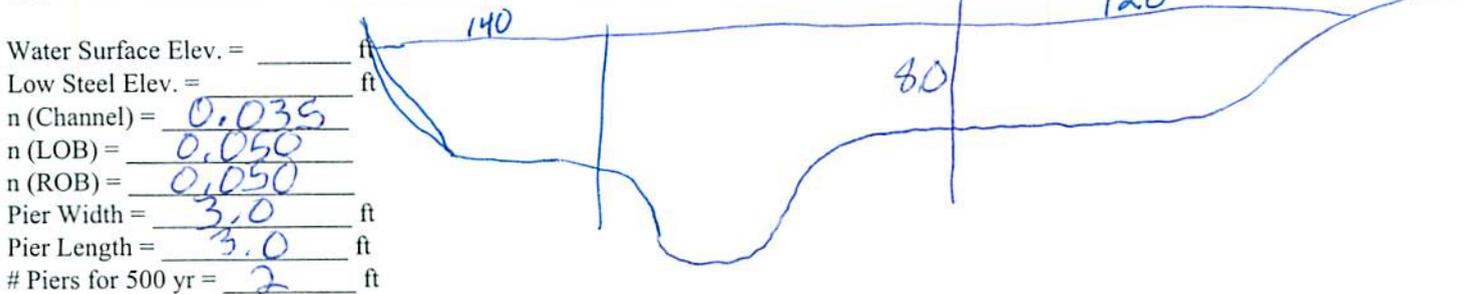
**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 16582080 Date 8/9/11 Initials CW Region (A B C D) B  
 Site \_\_\_\_\_ Location 1 mi. N + 0.2 E of McLaughlin on IRR 108 St  
 $Q_{500} =$  16600 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq.   
 Bridge discharge ( $Q_2$ ) = 16600 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 158 ft. Flow angle at bridge = 0° Abut. Skew = 0° Effective Skew = 0°  
 Width ( $W_2$ ) iteration = 158 100 118 110 110  
 Avg. flow depth at bridge,  $y_2$  iteration = 12.9 15.8 14.5 15.0 15.0  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 110 ft\*  $q_2 = Q_2/W_2 =$  150.9 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  10.1 ft/s Final  $y_2 = q_2/V_2 =$  15.0 ft  $\Delta h =$  2.1 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  17.1 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  160 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  140 ft Average left overbank flow depth,  $y_{lob} =$  7.1 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  120 ft Average right overbank flow depth,  $y_{rob} =$  6.0 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  15.34 From Figure 9  $W_2$  (effective) = 104 ft  $y_{cs} =$  15.2 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} >= 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1)^{7/6} =$  \_\_\_\_\_ ft If  $D_{50} >= D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1.0 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1.0  
 Froude # at bridge = 0.46 Using pier width a on Figure 11,  $\xi =$  10.7 Pier scour  $y_{ps} =$  9.5 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  7.1 ft right abutment,  $y_{aRT} =$  6.0 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  18.8 and  $\psi_{RT} =$  16.8  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1/0.55) =$  18.8 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1/0.55) =$  16.8 ft

8.00  
0.75  
40000  
40000  
40000

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Pie

PRGM: Abutment

Route RR 108 St Stream Oak Ck MRM \_\_\_\_\_ Date 8/9/11 Initials CEW  
 Bridge Structure No. 16582080 Location 1 mi. N + 0.2 mi E of McLaughlin on RR 108 St  
 GPS coordinates: N 45° 49' 53.9" taken from: USL abutment  centerline of MRM end \_\_\_\_\_  
W 100° 48' 26.4" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 146.70 sq. mi.  
 The average bottom of the main channel was 30 ft below top of guardrail at a point 44 ft from left abutment.  
 Method used to determine flood flows: \_\_\_\_\_ Freq. Anal. \_\_\_\_\_ drainage area ratio \_\_\_\_\_  regional regression equations.

**MISCELLANEOUS CONSIDERATIONS**

Flows	Q <sub>100</sub> = <u>6390</u>			Q <sub>500</sub> = <u>16600</u>		
Estimated flow passing through bridge	<u>6390</u>			<u>16600</u>		
Estimated road overflow & overtopping	<del>6390</del>			<del>16600</del>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Chance of Pressure flow		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

Peaks Calc'd on  
8/8

Pk 2	426
5	1300
10	2250
25	3610
50	4920
100	6390
500	16600

Riprap at abutments? \_\_\_\_\_ Yes \_\_\_\_\_ No  Marginal  
 Evidence of past Scour? \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know  
 Debris Potential? \_\_\_\_\_ High  Med \_\_\_\_\_ Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know \_\_\_\_\_ NA  
 Spur Dike \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know  NA  
 Other \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know  NA

**Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)**

Material Silt/Clay  Sand \_\_\_\_\_ Gravel \_\_\_\_\_ Cobbles \_\_\_\_\_ Boulders \_\_\_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos  
Very tall vegetation → lot's of estimating b/c poor visibility  
 1430-10 35- App XS LB  
 31-us 36- App XS RB  
 32-us RB 37- Bridge us  
 33-us LB 34-L Abut

**Summary of Results**

	Q100	Q500
Bridge flow evaluated	<u>6390</u>	<u>16600</u>
Flow depth at left abutment (yaLT), in feet	<u>2.7</u>	<u>7.1</u>
Flow depth at right abutment (yaRT), in feet	<u>1.5</u>	<u>6.0</u>
Contraction scour depth (yca), in feet	<u>12.7</u>	<u>15.2</u>
Pier scour depth (yp), in feet	<u>9.3</u>	<u>9.5</u>
Left abutment scour depth (yas), in feet	<u>11.0</u>	<u>18.8</u>
Right abutment scour depth (yas), in feet	<u>6.3</u>	<u>16.8</u>
Flow angle of attack	<u>0</u>	<u>0</u>

See Comments/Diagram for justification where required