

OK RT

### SCOUR ANALYSIS AND REPORTING FORM

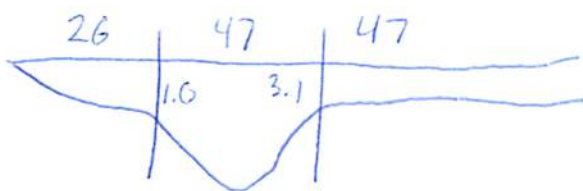
Bridge Structure No. 18092210 Date 6/6/12 Initials Ral Region (A B C D) C  
 Site \_\_\_\_\_ Location 8 mi W of Ethan on 265 St  
 $Q_{100} =$  1890 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 1890 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 47 ft. Flow angle at bridge = 5 ° Abut. Skew = 0 ° Effective Skew = 5 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_  
 Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 46.62 ft\*  $q_2 = Q_2/W_2 =$  40.4 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  4.5 ft/s Final  $y_2 = q_2/V_2 =$  9 ft  $\Delta h =$  0.4 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  9.4 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 1.2 ft  
 Low Steel Elev. = 11.2 ft  
 $n$  (Channel) = 0.035  
 $n$  (LOB) = 0.035  
 $n$  (ROB) = 0.035  
 Pier Width = 0 ft  
 Pier Length = 0 ft  
 # Piers for 100 yr = 0 ft



#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 =$  47 ft  $\frac{2}{3} \cdot 1.5$   
 Width of left overbank flow at approach,  $W_{lob} =$  26 ft Average left overbank flow depth,  $y_{lob} =$  1.0 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  47 ft Average right overbank flow depth,  $y_{rob} =$  3.1 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  1.65 From Figure 9  $W_2$  (effective) = 46.8 ft  $y_{cs} =$  2.2 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{2/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

#### PIER SCOUR CALCULATIONS

L/a ratio = \_\_\_\_\_ Correction factor for flow angle of attack (from Table 1),  $K_2 =$  \_\_\_\_\_  
 Froude # at bridge = \_\_\_\_\_ Using pier width a on Figure 11,  $\xi =$  \_\_\_\_\_ Pier scour  $y_{ps} =$  \_\_\_\_\_ ft

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} =$  1.0 ft right abutment,  $y_{aRT} =$  3.1 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  5.3 and  $\psi_{RT} =$  11.7  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) =$  6.4 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) =$  17.4 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pier

PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 18092210 Date 6/6/12 Initials Kal Region (A B C D) C  
 Site \_\_\_\_\_ Location 8 mi. W of Ethan on 265 St  
 $Q_{500} =$  3690 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 2951 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 47 ft. Flow angle at bridge = 5 ° Abut. Skew = 0 ° Effective Skew = 5 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_

Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 46.82 ft\*  $q_2 = Q_2/W_2 =$  63 ft<sup>2</sup>/s

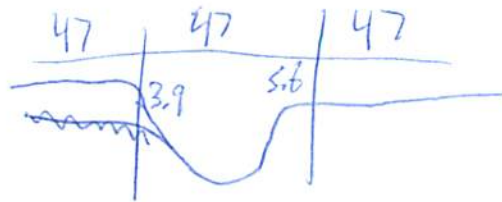
Bridge Vel,  $V_2 =$  5.6 ft/s Final  $y_2 = q_2/V_2 =$  11.2 ft  $\Delta h =$  0.6 ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  11.8 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 1.2 ft  
 Low Steel Elev. = 11.2 ft  
 $n$  (Channel) = 0.035  
 $n$  (LOB) = 0.035  
 $n$  (ROB) = 0.035  
 Pier Width = 0 ft  
 Pier Length = 0 ft  
 # Piers for 500 yr = 0 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  47 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  47 ft Average left overbank flow depth,  $y_{lob} =$  3.9 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  47 ft Average right overbank flow depth,  $y_{rob} =$  5.6 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  5.39 From Figure 9  $W_2$  (effective) = 46.8 ft  $y_{cs} =$  6 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} >= 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2 / y_1^{7/6})^{3/2} =$  \_\_\_\_\_ ft If  $D_{50} >= D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = \_\_\_\_\_ Correction factor for flow angle of attack (from Table 1),  $K_2 =$  \_\_\_\_\_  
 Froude # at bridge = \_\_\_\_\_ Using pier width  $a$  on Figure 11,  $\xi =$  \_\_\_\_\_ Pier scour  $y_{ps} =$  \_\_\_\_\_ ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  3.9 ft right abutment,  $y_{aRT} =$  5.6 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  13.1 and  $\psi_{RT} =$  16.1  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) =$  19.5 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) =$  24 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCSNEW

PRGM: Pier

PRGM: Abutment

43.51197  
98.14089

Route 265 St Stream N Branch 12 Mile Ck MRM \_\_\_\_\_ Date \_\_\_\_\_ Initials \_\_\_\_\_

Bridge Structure No. 18092210 Location 8 mi. W of Ethan on 265 St

GPS coordinates: N 45° 43' 31.2" taken from: USL abutment  centerline of  MRM end \_\_\_\_\_  
W 98° 0' 27.1" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 22.46 sq. mi.

The average bottom of the main channel was 16.4 ft below top of guardrail at a point 12 ft from left abutment.

Method used to determine flood flows: \_\_\_\_\_ Freq. Anal. \_\_\_\_\_ drainage area ratio  regional regression equations.

530  
8/23

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = <u>1890</u>			Q <sub>500</sub> = <u>3690</u>		
Estimated flow passing through bridge	<u>1890</u>			<u>2951</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>739</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Chance of Pressure flow		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

2 68.2683  
5 246 2929  
10 467  
25 898 898  
50 1340  
100 1890  
500 3690

Riprap at abutments? \_\_\_\_\_ Yes  No \_\_\_\_\_ Marginal  
 Evidence of past Scour?  Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know *abutment contraction*  
 Debris Potential? \_\_\_\_\_ High \_\_\_\_\_ Med  Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know \_\_\_\_\_ NA  
 Spur Dike \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know \_\_\_\_\_ NA  
 Other \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know \_\_\_\_\_ NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay  Sand \_\_\_\_\_ Gravel \_\_\_\_\_ Cobbles \_\_\_\_\_ Boulders \_\_\_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

1) main channel  
 2-3) right ab  
 4-5) left abd.  
 6) right OB  
 7) main channel  
 8) left OB

Summary of Results

	Q100	Q500
Bridge flow evaluated	<u>1890</u>	<u>2951</u>
Flow depth at left abutment (yaLT), in feet	<u>1.0</u>	<u>3.9</u>
Flow depth at right abutment (yaRT), in feet	<u>3.1</u>	<u>5.6</u>
Contraction scour depth (yca), in feet	<u>2.2</u>	<u>6</u>
Pier scour depth (ypp), in feet	<u>N/A</u>	<u>N/A</u>
Left abutment scour depth (yab), in feet	<u>6.4</u>	<u>7.3 + 19.5</u>
Right abutment scour depth (yab), in feet	<u>17.4</u>	<u>4.1 + 24</u>
IFlow angle of attack	<u>5</u>	<u>5</u>

See Comments/Diagram for justification where required