

OK RT

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 18160084 Date 7/7/11 Initials CW Region (A B C D)
Site Location NE edge Mitchell, Firesteel Creek, 410th Ave
Q100 = 12500\* by: drainage area ratio [checked] flood freq. anal. regional regression eq.

Bridge discharge (Q2) = 43996 (should be Q100 unless there is a relief bridge, road overflow, or bridge overtopping)

\* See note p.3 -> 12312 cfs from most contracted XS thru bridge 146'

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 166 ft. Flow angle at bridge = 52 degrees Abut. Skew = 0 degrees Effective Skew = 52 degrees

Width (W2) iteration = 166 146 Avg. flow depth at bridge, y2 iteration = 15.6 16.6 RD Overflow 102.2

Corrected channel width at bridge Section = W2 times cos of flow angle = 102.2 ft \* 0.6259 q2 = Q2/W2 = 136.9 ft^2/s

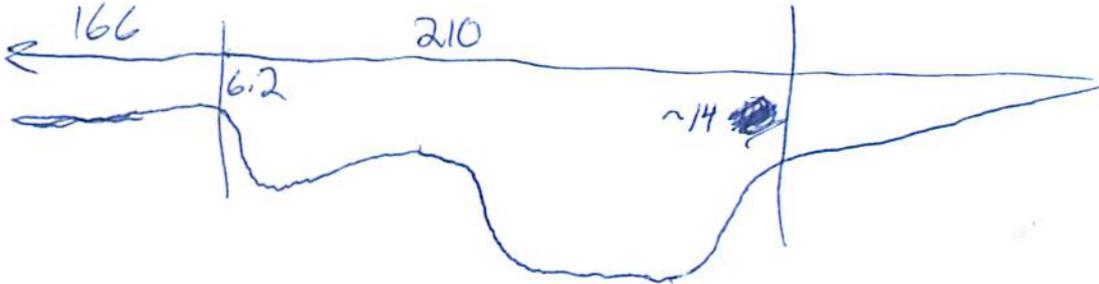
Bridge Vel, V2 = 4.3 ft/s Final y2 = q2/V2 = 16.5 ft Delta h = 1.4 ft

Average main channel depth at approach section, y1 = Delta h + y2 = 17.9 ft

\* NOTE: repeat above calculations until y2 changes by less than 0.2 Effective pier width = L sin(q) + a cos(q)

If y2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = Low Steel Elev. = 16.5 n (Channel) = 0.040 n (LOB) = 0.100 n (ROB) = 0.100 Pier Width = 2.3 ft Pier Length = 2.3 ft # Piers for 100 yr = 2



CONTRACTION SCOUR

Width of main channel at approach section W1 = 210 ft

Width of left overbank flow at approach, Wlob = 166 ft Average left overbank flow depth, ylob = 6.2 ft

Width of right overbank flow at approach, Wrob = 60 ft Average right overbank flow depth, yrob = 7.0 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

x = 23.62 / 29.61 From Figure 9 W2 (effective) = 97.5 / 85.3 ft ycs = 11.6 / 22.9 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material D50 = Average approach velocity, V1 = Q100/(y1W1) = ft/s

Critical approach velocity, Vc = 11.52y1^(1/6)D50^(1/3) = ft/s

If V1 < Vc and D50 >= 0.2 ft, use clear water equation below, otherwise use live bed scour equation above.

Dc50 = 0.0006(q2/y1^(7/6))^3 = ft If D50 >= Dc50, chi = 0.0

Otherwise, chi = 0.122y1[q2/(D50^(1/3)y1^(7/6))]^(6/7) - y1 = From Figure 10, ycs = ft

PIER SCOUR CALCULATIONS

L/a ratio = 1.0 Correction factor for flow angle of attack (from Table 1), K2 = 1.0
Froude # at bridge = 0.36 Using pier width a on Figure 11, xi = 8.9 Pier scour yps = 7.6 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, yaLT = 6.2 ft right abutment, yaRT = 7.0 ft
Shape coefficient K1 = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
Using values for yaLT and yaRT on figure 12, psiLT = 17.2 and psiRT = 18.6
Left abutment scour, yas = psiLT(K1/0.55) = 17.2 ft Right abutment scour yas = psiRT(K1/0.55) = 18.6 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pier

PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 18160084 Date 7/7/11 Initials LM Region (A B C D) C

Site \_\_\_\_\_ Location NE edge Mitchell

$Q_{500} = 18,800$  \* by: drainage area ratio  flood freq. anal. \_\_\_\_\_ regional regression eq. \_\_\_\_\_

Bridge discharge ( $Q_2$ ) = 13976 \* (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

\* see note p. 3 see p. 1 12312 cfs

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 166 ft. Flow angle at bridge = 52 ° Abut. Skew = 0 ° Effective Skew = 52 °

Width ( $W_2$ ) iteration = RD Overflow 146' is most contracted

Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_

Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 102.2 ft\*  $q_2 = Q_2/W_2 = 13976/146 = 95.72$  ft<sup>2</sup>/s

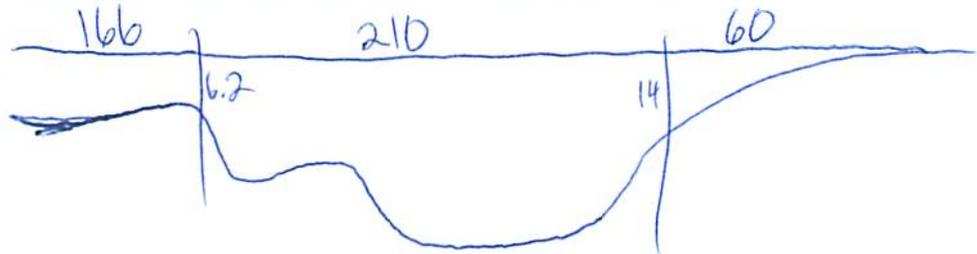
Bridge Vel,  $V_2 = 8.3$  ft/s Final  $y_2 = q_2/V_2 = 16.5$  ft  $\Delta h = 1.4$  ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = 17.9$  ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = \_\_\_\_\_ ft  
 Low Steel Elev. = 16.5 ft  
 $n$  (Channel) = 0.040  
 $n$  (LOB) = 0.100  
 $n$  (ROB) = 0.100  
 Pier Width = 2.3 ft  
 Pier Length = 2.3 ft  
 # Piers for 500 yr = 2



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 = 210$  ft

Width of left overbank flow at approach,  $W_{lob} = 166$  ft

Average left overbank flow depth,  $y_{lob} = 6.2$  ft

Width of right overbank flow at approach,  $W_{rob} = 60$  ft

Average right overbank flow depth,  $y_{rob} = 7.0$  ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x = \frac{23.62}{29.61}$  From Figure 9  $W_2$  (effective) =  $\frac{97.6}{85.3}$  ft  $y_{cs} = \frac{19.6}{22.9}$  ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1.0

Correction factor for flow angle of attack (from Table 1),  $K_2 = 1.0$

Froude # at bridge = 0.36

Using pier width  $a$  on Figure 11,  $\xi = 6.9$  Pier scour  $y_{ps} = 7.6$  ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} = 6.2$  ft right abutment,  $y_{aRT} = 7.0$  ft

Shape coefficient  $K_1 = 1.00$  for vertical-wall,  $0.82$  for vertical-wall with wingwalls,  $0.55$  for spill-through

Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = 17.2$  and  $\psi_{RT} = 18.6$

Left abutment scour,  $y_{as} = \psi_{LT} (K_1/0.55) = 17.2$  ft Right abutment scour  $y_{as} = \psi_{RT} (K_1/0.55) = 18.6$  ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pie

PGRM: Abutment

Route 410 Ave Stream Firesteel Creek MRM \_\_\_\_\_ Date 7/7/11 Initials CW

Bridge Structure No. 18160084 Location NE edge Mitchell

GPS coordinates: N 43° 43' 31.4" taken from: USL abutment  centerline of  $\uparrow$  MRM end \_\_\_\_\_  
W 78° 00' 27.7" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 647.96 sq. mi.

The average bottom of the main channel was 21.8 ft below top of guardrail at a point 38 ft from left abutment.

Method used to determine flood flows: \_\_\_\_\_ Freq. Anal.  drainage area ratio \_\_\_\_\_ regional regression equations.

**MISCELLANEOUS CONSIDERATIONS**

Flows	Q <sub>100</sub> = <u>12500*</u>			Q <sub>500</sub> = <u>18800*</u>		
Estimated flow passing through bridge	<del>13996</del> <u>12312</u>			<del>13996</del> <u>12312</u>		
Estimated road overflow & overtopping	<u>188</u>			<del>6466</del> <u>4504</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping			<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>
Chance of Pressure flow	<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

\* peaks are probably overestimated - Lk will probably attenuate peak flows

Riprap at abutments? \_\_\_\_\_ Yes \_\_\_\_\_ No  Marginal  
 Evidence of past Scour?  Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know  
 Debris Potential?  High \_\_\_\_\_ Med \_\_\_\_\_ Low

Does scour countermeasure(s) appear to have been designed?

Riprap  Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know \_\_\_\_\_ NA  
 Spur Dike \_\_\_\_\_ Yes \_\_\_\_\_ No  Don't know \_\_\_\_\_ NA  
 Other \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know  NA

**Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)**

Material Silt/Clay  Sand \_\_\_\_\_ Gravel \_\_\_\_\_ Cobbles \_\_\_\_\_ Boulders \_\_\_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

For 100 yr → geometry makes calcs funny 12500 cfs < 13996 cfs  
 7.8 146' → 12312 cfs  
 Photos  
 1714- ID  
 15- US  
 16- USRB  
 17- USLB  
 18- L Abut  
 19- R Abut  
 20- Looking at LB US App XS  
 21- RB US App XS

**Summary of Results**

	Q100	Q500
Bridge flow evaluated	<u>12312</u>	<u>12312</u>
Flow depth at left abutment (yaLT), in feet	<u>6.2</u>	<u>6.2</u>
Flow depth at right abutment (yaRT), in feet	<u>7.0</u>	<u>7.0</u>
Contraction scour depth (yca), in feet	<u>22.9</u>	<u>22.9</u>
Pier scour depth (ypp), in feet	<u>7.6</u>	<u>7.6</u>
Left abutment scour depth (yab), in feet	<u>17.2</u>	<u>17.2</u>
Right abutment scour depth (yab), in feet	<u>18.6</u>	<u>18.6</u>
Flow angle of attack	<u>52</u>	<u>52</u>

See Comments/Diagram for justification where required