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### SCOUR ANALYSIS AND REPORTING FORM

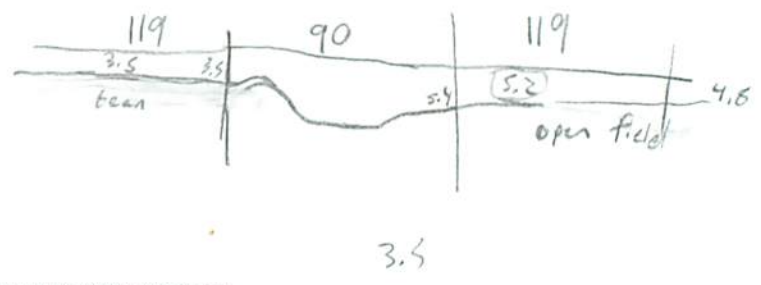
Bridge Structure No. 20030206 Date 7/30/12 Initials RAJ Region (A B C D) D  
 Site \_\_\_\_\_ Location 0.6 mi S of int of 469 Ave & 186 St.  
 $Q_{100} =$  4680 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 4680 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 119 ft. Flow angle at bridge = 10 ° Abut. Skew = 0 ° Effective Skew = 10 °  
 Width ( $W_2$ ) iteration = 119 86 90  
 Avg. flow depth at bridge,  $y_2$  iteration = 8.9 10.5 10.3  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 86.63 ft\*  $q_2 = Q_2/W_2 =$  52.8 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  5.2 ft/s Final  $y_2 = q_2/V_2 =$  10.3 ft  $\Delta h =$  0.5 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  10.8 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0-0.4 ft <sup>23.1</sup>/<sub>4.1</sub>  
 Low Steel Elev. = 19.0 ft see notes  
 $n$  (Channel) = 0.040  
 $n$  (LOB) = 0.030  
 $n$  (ROB) = 0.035  
 Pier Width = 2 ft  
 Pier Length = 2 ft  
 # Piers for 100 yr = 4 ft



#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 =$  90 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  119 ft Average left overbank flow depth,  $y_{lob} =$  5.2 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  119 ft Average right overbank flow depth,  $y_{rob} =$  3.5 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  10.33 From Figure 9  $W_2$  (effective) = 80.6 ft  $y_{cs} =$  11.3 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} >= 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} >= D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

#### PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.29 Using pier width  $a$  on Figure 11,  $\xi =$  8 Pier scour  $y_{ps} =$  24.63 ft 6.6

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} =$  5.2 ft right abutment,  $y_{aRT} =$  3.5 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  15.4 and  $\psi_{RT} =$  12.4  
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  15.4 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  12.4 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Pier

PRGM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 20030206 Date 7/30/12 Initials Ral Region (A B C D) D  
 Site \_\_\_\_\_ Location 0.6 mi S of int of 469 Av + 186 St  
 $Q_{500} =$  7510 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 7510 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 119 ft. Flow angle at bridge = 10 ° Abut. Skew = 0 ° Effective Skew = 10 °  
 Width ( $W_2$ ) iteration = 119 92 97 96  
 Avg. flow depth at bridge,  $y_2$  iteration = 11.3 12.9 12.5 12.6  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 94.91 ft\*  $q_2 = Q_2/W_2 =$  79.4 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  6.3 ft/s Final  $y_2 = q_2/V_2 =$  12.6 ft  $\Delta h =$  0.8 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  13.4 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0-0.4 ft  
 Low Steel Elev. = 19.0 ft  
 $r$  (Channel) = 0.040  
 $n$  (LOB) = 0.030  
 $n$  (ROB) = 0.035  
 Pier Width = 2 ft  
 Pier Length = 2 ft  
 # Piers for 500 yr = 4 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  96 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  119 ft Average left overbank flow depth,  $y_{lob} =$  7.8 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  119 ft Average right overbank flow depth,  $y_{rob} =$  6.1 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  17.11 From Figure 9  $W_2$  (effective) = 86.5 ft  $y_{cs} =$  16.1 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

$L/a$  ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.31 Using pier width  $a$  on Figure 11,  $\xi =$  8 Pier scour  $y_{ps} =$  6.7 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  7.8 ft right abutment,  $y_{aRT} =$  6.1 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  19.6 and  $\psi_{RT} =$  17.0  
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  19.6 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  17.0 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCSNEW

PGRM: Pic

PGRM: Abutment

1141E 1bh 09b  
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62089'11  
96.82539

1141E 1bh 09b  
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1141E 1bh 09b  
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Route 469 Ave Stream Hidewood Ck MRM \_\_\_\_\_ Date 7/30/12 Initials LAJ  
 Bridge Structure No. 20030206 Location 0.6 mi S of int of 469 Av + 186 St  
 GPS coordinates: N 44° 40' 48.2" taken from:  USL abutment  centerline of ↑ MRM end \_\_\_\_\_  
W 96° 49' 32.2" Datum of coordinates:  WGS84  NAD27 \_\_\_\_\_  
 Drainage area = 135.86 sq. mi.  
 The average bottom of the main channel was 23.1 ft below top of guardrail at a point 56 ft from left abutment.  
 Method used to determine flood flows:  Freq. Anal.  drainage area ratio  regional regression equations.

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8/23

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = <u>4680</u>			Q <sub>500</sub> = <u>7510</u>				
Estimated flow passing through bridge	<u>4680</u>			<u>7510</u>			2	384
Estimated road overflow & overtopping	<u>0</u>			<u>0</u>			5	1040
Consideration	Yes	No	Possibly	Yes	No	Possibly	10	1680
Chance of overtopping		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>		25	2710
Chance of Pressure flow		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>		50	3630-3640
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>		100	4680
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>		500	7500-7510

Riprap at abutments?  Yes  No  Marginal  
 Evidence of past Scour?  Yes  No  Don't know *some contractor, minor abutment*  
 Debris Potential?  High  Med  Low  
 Does scour countermeasure(s) appear to have been designed?  
 Riprap  Yes  No  Don't know  NA *- cobble-sized riprap held in place by netted wires.*  
 Spur Dike  Yes  No  Don't know  NA  
 Other  Yes  No  Don't know  NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay  Sand  Gravel  Cobbles  Boulders \_\_\_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos  
 1). left CB  
 2). main channel  
 3). right CB  
 4). pier  
 5-6). left abutment  
 7-8). right abutment  
 9). bed material  
 10). main channel

Note: bridge on hill slope! took lowest from bridge depth location. Lots of cobbles under bridge. Consider contraction scour.

Summary of Results

	Q100	Q500
Bridge flow evaluated	<u>4680</u>	<u>7510</u>
Flow depth at left abutment (yaLT), in feet	<u>5.2</u>	<u>7.9</u>
Flow depth at right abutment (yaRT), in feet	<u>3.5</u>	<u>6.1</u>
Contraction scour depth (y <sub>cs</sub> ), in feet	<u>11.3</u>	<u>16.1</u>
Pier scour depth (y <sub>ps</sub> ), in feet	<u>6.3</u> <u>6.6</u>	<u>6.7</u>
Left abutment scour depth (y <sub>as</sub> ), in feet	<u>15.4</u>	<u>19.6</u>
Right abutment scour depth (y <sub>as</sub> ), in feet	<u>12.4</u>	<u>17.0</u>
Flow angle of attack	<input checked="" type="checkbox"/> 10	<input checked="" type="checkbox"/> 10

See Comments/Diagram for justification where required