

OK RT

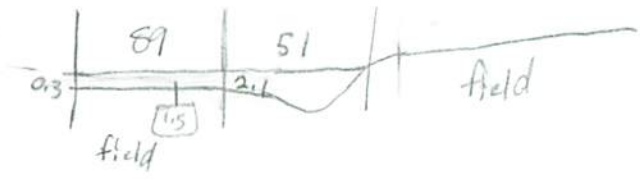
### SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 20050 273 Date 7/30/12 Initials Rat Region (A B C D) C  
 Site \_\_\_\_\_ Location 5.4 mi E of Estelline + 0.7 mi N on 471 Av  
 $Q_{100} =$  1210 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 120 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 89 ft. Flow angle at bridge = 25 ° Abut. Skew = 0 ° Effective Skew = 25 °  
 Width ( $W_2$ ) iteration = 89 50 53  
 Avg. flow depth at bridge,  $y_2$  iteration = 5.5 7.3 7.1  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 98.03 ft\*  $q_2 = Q_2/W_2 =$  25.2 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  3.6 ft/s Final  $y_2 = q_2/V_2 =$  7.1 ft  $\Delta h =$  0.3 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  7.3 ft  
 \*NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0-3.2 ft  
 Low Steel Elev. = 16.6 ft  
 $n$  (Channel) = 0.040  
 $n$  (LOB) = 0.030  
 $n$  (ROB) = 0.035  
 Pier Width = 1.7 ft  
 Pier Length = 1.7 ft  
 # Piers for 100 yr = 2 ft



#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 =$  51 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  89 ft Average left overbank flow depth,  $y_{lob} =$  1.5 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  0 ft Average right overbank flow depth,  $y_{rob} =$  0 ft  
 Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  2.43 From Figure 9  $W_2$  (effective) = 49.6 ft  $y_{cs} =$  3 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} >= 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} >= D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

#### PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.24 Using pier width  $a$  on Figure 11,  $\xi =$  7 Pier scour  $y_{ps} =$  5.7 ft

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} =$  1.5 ft right abutment,  $y_{aRT} =$  0 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  63 and  $\psi_{RT} =$  0  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1/0.55) =$  6.3 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1/0.55) =$  0 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWC/SNEW

PRGM: Pier

PRGM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

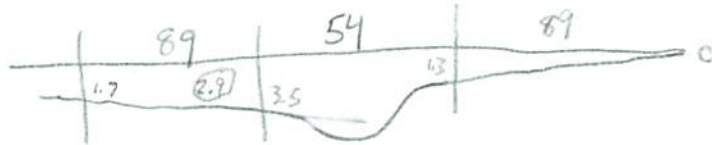
Bridge Structure No. 20050223 Date 7/30/12 Initials RA Region (A B C D) C  
 Site \_\_\_\_\_ Location 5.4 mi E + 0.7 mi N of Estelline on 471 Av  
 $Q_{500} =$  1870 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 1970 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 89 ft. Flow angle at bridge = 25 ° Abut. Skew = 0 ° Effective Skew = 25 °  
 Width ( $W_2$ ) iteration = 89 52 61 59  
 Avg. flow depth at bridge,  $y_2$  iteration = 6.8 8.9 8.2 8.6  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 53.47 ft\*  $q_2 = Q_2/W_2 =$  35 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  4.2 ft/s Final  $y_2 = q_2/V_2 =$  8.3 ft  $\Delta h =$  0.4 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  8.7 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0-3.2 ft  
 Low Steel Elev. = 16.6 ft  
 $n$  (Channel) = 0.040  
 $n$  (LOB) = 0.030  
 $n$  (ROB) = 0.035  
 Pier Width = 1.7 ft  
 Pier Length = 1.7 ft  
 # Piers for 500 yr = 2 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  54 ft  $1.3 = \frac{2}{3}$   
 Width of left overbank flow at approach,  $W_{lob} =$  89 ft Average left overbank flow depth,  $y_{lob} =$  0.9 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  89 ft Average right overbank flow depth,  $y_{rob} =$  2.9 ft  $3.5 \rightarrow 1.7$   
 $M = \frac{3.5}{40FF}$   
Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  4.67 From Figure 9  $W_2$  (effective) = 50.1 ft  $y_{cs} =$  4.6 ft  
3.99

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} >= 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} >= D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6.7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

$L/a$  ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.26 Using pier width  $a$  on Figure 11,  $\xi =$  7 Pier scour  $y_{ps} =$  5.7 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  6.9 ft right abutment,  $y_{aRT} =$  2.9 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  3.9 and  $\psi_{RT} =$  11.3  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1/0.55) =$  3.9 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1/0.55) =$  11.3 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"  
PRGM: Contract  
PRGM: CWCSNEW  
PRGM: Pie  
PRGM: Abutment

LH357h  
LLh3L7b

"2L15, Lh 2b  
4p 25, @492"



Route 471 Av Stream Peg Munky Run Cr MRM \_\_\_\_\_ Date 7/30/12 Initials Pat  
 Bridge Structure No. 20050273 Location 5.4 mi E + 0.7 mi N of Estelline on 471 Av  
 GPS coordinates: N 44° 31' 59.7" taken from: USL abutment  centerline of ↑ MRM end \_\_\_\_\_  
W 96° 47' 5.0" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 8.50 sq. mi.  
 The average bottom of the main channel was 20.4 ft below top of guardrail at a point 59 ft from left abutment.  
 Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio  regional regression equations.

713  
 8/23  
 2 | 105  
 5 | 283  
 10 | 452  
 25 | 719  
 50 | 951  
 100 | 1210  
 500 | 1870

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = <u>1210</u>			Q <sub>500</sub> = <u>1870</u>		
Estimated flow passing through bridge	<u>1210</u>			<u>1870</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>0</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Chance of Pressure flow		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

Riprap at abutments? \_\_\_ Yes \_\_\_ No  Marginal  
 Evidence of past Scour?  Yes \_\_\_ No \_\_\_ Don't know *some pic/contractor and left abutment*  
 Debris Potential? \_\_\_ High \_\_\_ Med  Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Spur Dike \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Other \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay  Sand \_\_\_ Gravel \_\_\_ Cobbles \_\_\_ Boulders \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos  
 1) left ab.  
 2) main channel  
 3) right ab.  
 4) pic  
 5-6) left abutment  
 7) main channel.  
 5-7) right abutment.

Summary of Results

	Q100	Q500
Bridge flow evaluated	<u>1210</u>	<u>1870</u>
Flow depth at left abutment (yaLT), in feet	<u>1.5</u>	<u>0.9</u>
Flow depth at right abutment (yaRT), in feet	<u>0</u>	<u>2.9</u>
Contraction scour depth (yca), in feet	<u>3</u>	<u>5.6 - 4.6</u>
Pier scour depth (yps), in feet	<u>5.7</u>	<u>5.7</u>
Left abutment scour depth (yas), in feet	<u>6.3</u>	<u>3.9</u>
Right abutment scour depth (yas), in feet	<u>0</u>	<u>11.3</u>
Flow angle of attack	<u>25</u>	<u>25</u>

See Comments/Diagram for justification where required