

ok-Rat

### SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 20156220 Date 10-11-12 Initials RFT Region (A B C D)

Site \_\_\_\_\_ Location 2.6 mi E Brndt on 188 St

$Q_{100} = 2460$  by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X

Bridge discharge ( $Q_2$ ) = 2460 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method *low flow channel has larger angle, but the low flow channel is very shallow*

Bridge Width = 94 ft. Flow angle at bridge = 18 ° Abut. Skew = 0 ° Effective Skew = 18 °

Width ( $W_2$ ) iteration = 94

Avg. flow depth at bridge,  $y_2$  iteration = 7.4

Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 89.4 ft\*  $q_2 = Q_2/W_2 = 27.5$  ft<sup>2</sup>/s

Bridge Vel,  $V_2 = 3.7$  ft/s Final  $y_2 = q_2/V_2 = 7.4$  ft  $\Delta h = 0.3$  ft

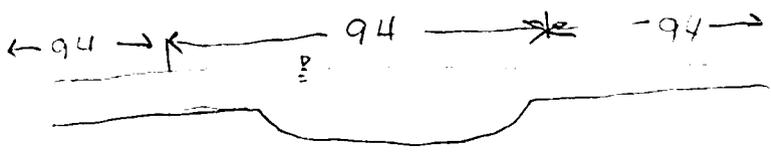
Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = 7.7$  ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 11.2 ft  
Low Steel Elev. = 8.0 ft  
n (Channel) = 0.35  
n (LOB) = 0.35  
n (ROB) = 0.35  
Pier Width = 1.1 ft  
Pier Length = 1.1 ft  
# Piers for 100 yr = 2 ft

ungrazed pasture



### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 = 94$  ft

Width of left overbank flow at approach,  $W_{lob} = 94$  ft

Average left overbank flow depth,  $y_{lob} = 6.0$  ft

Width of right overbank flow at approach,  $W_{rob} = 94$  ft

Average right overbank flow depth,  $y_{rob} = 5.6$  ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x = 10.96$  From Figure 9  $W_2$  (effective) = 87.2 ft  $y_{cs} = 12$  ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1)^{7/6} =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

### PIER SCOUR CALCULATIONS

L/a ratio = 1

Correction factor for flow angle of attack (from Table 1),  $K_2 = 1$

Froude # at bridge = 0.24

Using pier width a on Figure 11,  $\xi = 5.2$  Pier scour  $y_{ps} = 4.2$  ft

### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} = 6.0$  ft right abutment,  $y_{aRT} = 5.6$  ft

Shape coefficient  $K_1 = 1.00$  for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through

Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = 16.8$  and  $\psi_{RT} = 16.1$

Left abutment scour,  $y_{as} = \psi_{LT} (K_1/0.55) = 25.1$  ft Right abutment scour  $y_{as} = \psi_{RT} (K_1/0.55) = 24$  ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCSNEW

PRGM: Pier

PRGM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 20156220 Date \_\_\_\_\_ Initials \_\_\_\_\_ Region (A B C D) \_\_\_\_\_

Site \_\_\_\_\_ Location \_\_\_\_\_

$Q_{500} = 3850$  by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq.

Bridge discharge ( $Q_2$ ) = 3850 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 94 ft. Flow angle at bridge = 18 ° Abut. Skew = 0 ° Effective Skew = 18 °

Width ( $W_2$ ) iteration = 94

Avg. flow depth at bridge,  $y_2$  iteration = 9.3

Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 89.4 ft\*  $q_2 = Q_2/W_2 = 43.1$  ft<sup>2</sup>/s

Bridge Vel,  $V_2 = 4.7$  ft/s Final  $y_2 = q_2/V_2 = 9.3$  ft  $\Delta h = 0.4$  ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = 9.7$  ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

road overflow will begin at  $y_2 \approx 9.5$  ft

Water Surface Elev. = dry ft

Low Steel Elev. = 8.0 ft

n (Channel) = .035

n (LOB) = .035

n (ROB) = .035

Pier Width = 1.1 ft

Pier Length = 1.1 ft

# Piers for 500 yr = 2 ft

**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 = 94$  ft

Width of left overbank flow at approach,  $W_{lob} = 94$  ft

Average left overbank flow depth,  $y_{lob} = 8.0$  ft

Width of right overbank flow at approach,  $W_{rob} = 94$  ft

Average right overbank flow depth,  $y_{rob} = 7.6$  ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x = 15.3$  From Figure 9  $W_2$  (effective) = 87.2 ft  $y_{cs} = 15.2$  ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006(q_2/y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 = 1$

Froude # at bridge = 0.27 Using pier width a on Figure 11,  $\xi = 5.2$  Pier scour  $y_{ps} = 4.3$  ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} = 8.0$  ft right abutment,  $y_{aRT} = 7.6$  ft

Shape coefficient  $K_1 = 1.00$  for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through

Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = 19.8$  and  $\psi_{RT} = 19.5$

Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) = 29.5$  ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) = 29$  ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Pie

PRGM: Abutment

Route 188 St Stream Cobb Creek MRM \_\_\_\_\_ Date \_\_\_\_\_ Initials \_\_\_\_\_  
 Bridge Structure No. 20156220 Location 2.6 mi E Bandt on 188 St  
 GPS coordinates: N 44° 39.585' taken from:  USL abutment  centerline of  $\uparrow$  MRM end \_\_\_\_\_  
W 96° 34.151' Datum of coordinates:  WGS84  NAD27 \_\_\_\_\_

Drainage area = 28.53 sq. mi.

The average bottom of the main channel was 11.7 ft below top of guardrail at a point 30 ft from left abutment.  
 Method used to determine flood flows:  Freq. Anal.  drainage area ratio  regional regression equations.

8-23-12  
Pk | Q

**MISCELLANEOUS CONSIDERATIONS**

Flows	Q <sub>100</sub> = <u>2460</u>			Q <sub>500</sub> = <u>3850</u>		
Estimated flow passing through bridge	<u>2460</u>			<u>3850</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>0</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>				<input checked="" type="checkbox"/>
Chance of Pressure flow		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

2	219
5	581
10	922
25	1460
50	1940
100	2460
500	3850

Riprap at abutments?  Yes  No  Marginal  
 Evidence of past Scour?  Yes  No  Don't know *possibly minor contraction scour*  
 Debris Potential?  High  Med  Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap  Yes  No  Don't know  NA  
 Spur Dike  Yes  No  Don't know  NA  
 Other  Yes  No  Don't know  NA

**Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)**

Material Silt/Clay X Sand \_\_\_\_\_ Gravel \_\_\_\_\_ Cobbles \_\_\_\_\_ Boulders \_\_\_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

**Comments, Diagrams & orientation of digital photos**

str. no.  
 approach from bridge left abut. under bridge  
 LOB from bridge rt. abut. under bridge  
 ROB from bridge  
 bridge from approach

**Summary of Results**

	Q100	Q500
Bridge flow evaluated	<u>2460</u>	<u>3850</u>
Flow depth at left abutment (yaLT), in feet	<u>6.0</u>	<u>8.0</u>
Flow depth at right abutment (yaRT), in feet	<u>5.6</u>	<u>7.6</u>
Contraction scour depth (y <sub>cs</sub> ), in feet	<u>12.0</u>	<u>15.2</u>
Pier scour depth (y <sub>ps</sub> ), in feet	<u>4.2</u>	<u>4.3</u>
Left abutment scour depth (y <sub>as</sub> ), in feet	<u>25.1</u>	<u>29.5</u>
Right abutment scour depth (y <sub>as</sub> ), in feet	<u>24</u>	<u>29.0</u>
Flow angle of attack	<u>* 18°</u>	<u>* 18°</u>

\* low flow channel approaches bridge at a larger angle, but may have little effect at high flows  
 See Comments/Diagram for justification where required