

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 22211160 Date 10/10/11 Initials CW Region (A B C D)

Site \_\_\_\_\_ Location 5.9 mi W of Delmont on 294 St

$Q_{100} =$  4700 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. \_\_\_\_\_

Bridge discharge ( $Q_2$ ) = 3298 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 120 ft. Flow angle at bridge = 0° Abut. Skew = 0° Effective Skew = 0°

Width ( $W_2$ ) iteration = 120

Avg. flow depth at bridge,  $y_2$  iteration = 8.8 > 7.4 → RD overflow

Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 120 ft\*  $q_2 = Q_2/W_2 =$  27.5 ft<sup>2</sup>/s

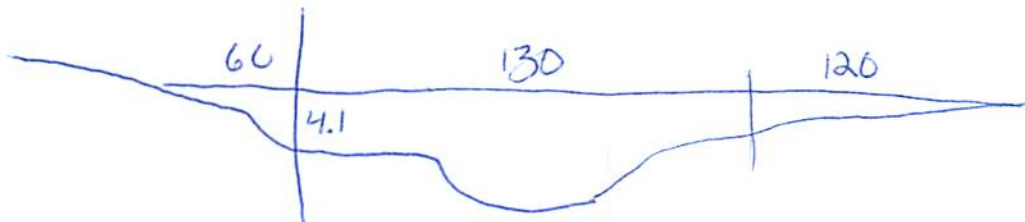
Bridge Vel,  $V_2 =$  3.7 ft/s Final  $y_2 = q_2/V_2 =$  7.4 ft  $\Delta h =$  0.3 ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  7.7 ft

\*NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

- Water Surface Elev. = \_\_\_\_\_ ft
- Low Steel Elev. = 7.4 ft
- n (Channel) = 0.040
- n (LOB) = 0.035
- n (ROB) = 0.033
- Pier Width = 1.65 ft
- Pier Length = 3.6/22 ft
- # Piers for 100 yr = 3 ft



CONTRACTION SCOUR

Width of main channel at approach section  $W_1 =$  130 ft

Width of left overbank flow at approach,  $W_{lob} =$  60 ft Average left overbank flow depth,  $y_{lob} =$  2.05 ft 2.1

Width of right overbank flow at approach,  $W_{rob} =$  120 ft Average right overbank flow depth,  $y_{rob} =$  1.0 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  1.45 From Figure 9  $W_2$  (effective) = 115.1 ft  $y_{cs} =$  2.4 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} >= 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1)^{7/6} =$  \_\_\_\_\_ ft If  $D_{50} >= D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

PIER SCOUR CALCULATIONS

L/a ratio = 2.14 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1.0  
 Froude # at bridge = 0.24 Using pier width a on Figure 11,  $\xi =$  6.9 Pier scour  $y_{ps} =$  5.6 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} =$  2.1 ft right abutment,  $y_{aRT} =$  1.0 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  8.6 and  $\psi_{RT} =$  4.3  
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  4.6 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  4.3 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCSNEW

PRGM: Pier

PRGM: Abutment



**SCOUR ANALYSIS AND REPORTING FORM**

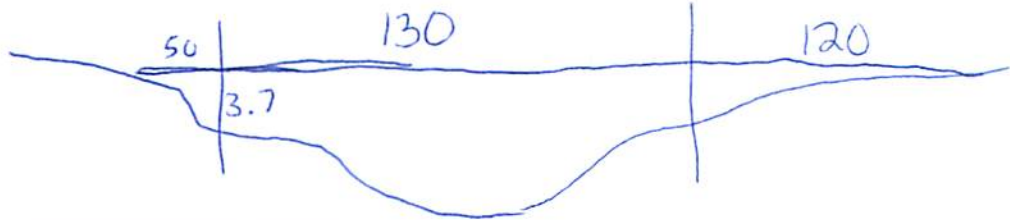
Bridge Structure No. 22211160 Date 10/10/11 Initials CL Region (A B C D) 0  
 Site \_\_\_\_\_ Location 5.9 mi W of Delmont on 284 St  
 Q<sub>500</sub> = 3010 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. \_\_\_\_\_  
 Bridge discharge (Q<sub>2</sub>) = 3010 (should be Q<sub>500</sub> unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 120 ft. Flow angle at bridge = 0 ° Abut. Skew = 0 ° Effective Skew = 0 °  
 Width (W<sub>2</sub>) iteration = 120  
 Avg. flow depth at bridge, y<sub>2</sub> iteration = 7.1 → Vert Wall  
 Corrected channel width at bridge Section = W<sub>2</sub> times cos of flow angle = 120 ft\* q<sub>2</sub> = Q<sub>2</sub>/W<sub>2</sub> = 25.1 ft<sup>2</sup>/s  
 Bridge Vel, V<sub>2</sub> = 3.5 ft/s Final y<sub>2</sub> = q<sub>2</sub>/V<sub>2</sub> = 7.1 ft Δh = 0.2 ft  
 Average main channel depth at approach section, y<sub>1</sub> = Δh + y<sub>2</sub> = 7.3 ft

\* NOTE: repeat above calculations until y<sub>2</sub> changes by less than 0.2 Effective pier width = L sin(q) + a cos(q)  
 If y<sub>2</sub> is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = \_\_\_\_\_ ft  
 Low Steel Elev. = 7.4 ft  
 n (Channel) = 0.040  
 n (LOB) = 0.035  
 n (ROB) = 0.033  
 Pier Width = 1.65 ft  
 Pier Length = 3.6/22 ft  
 # Piers for 500 yr = 3 ft



**CONTRACTION SCOUR**

Width of main channel at approach section W<sub>1</sub> = 130 ft  
 Width of left overbank flow at approach, W<sub>lob</sub> = 50 ft Average left overbank flow depth, y<sub>lob</sub> = 1.9 ft  
 Width of right overbank flow at approach, W<sub>rob</sub> = 120 ft Average right overbank flow depth, y<sub>rob</sub> = 0.6 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 x = 1.48 From Figure 9 W<sub>2</sub> (effective) = 115.1 ft y<sub>cs</sub> = 2.0 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material D<sub>50</sub> = \_\_\_\_\_ ft Average approach velocity, V<sub>1</sub> = Q<sub>500</sub>/(y<sub>1</sub>W<sub>1</sub>) = \_\_\_\_\_ ft/s  
 Critical approach velocity, V<sub>c</sub> = 11.17y<sub>1</sub><sup>1/6</sup>D<sub>50</sub><sup>1/3</sup> = \_\_\_\_\_ ft/s  
 If V<sub>1</sub> < V<sub>c</sub> and D<sub>50</sub> >= 0.2 ft, use clear water equation below, otherwise use live bed scour equation above.  
 D<sub>c50</sub> = 0.0006(q<sub>2</sub>/y<sub>1</sub><sup>7/6</sup>)<sup>3</sup> = \_\_\_\_\_ ft If D<sub>50</sub> >= D<sub>c50</sub>, χ = 0.0  
 Otherwise, χ = 0.122y<sub>1</sub>[q<sub>2</sub>/(D<sub>50</sub><sup>1/3</sup>y<sub>1</sub><sup>7/6</sup>)<sup>6/7</sup>] - y<sub>1</sub> = \_\_\_\_\_ From Figure 10, y<sub>cs</sub> = \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 2.14 Correction factor for flow angle of attack (from Table 1), K<sub>2</sub> = 1.0  
 Froude # at bridge = 0.23 Using pier width a on Figure 11, ξ = 6.9 Pier scour y<sub>ps</sub> = 5.5 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment, y<sub>aLT</sub> = 1.9 ft right abutment, y<sub>aRT</sub> = 0.6 ft  
 Shape coefficient K<sub>1</sub> = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for y<sub>aLT</sub> and y<sub>aRT</sub> on figure 12, ψ<sub>LT</sub> = 7.4 and ψ<sub>RT</sub> = 2.7  
 Left abutment scour, y<sub>as</sub> = ψ<sub>LT</sub>(K<sub>1</sub>/0.55) = 7.4 ft Right abutment scour y<sub>as</sub> = ψ<sub>RT</sub>(K<sub>1</sub>/0.55) = 2.7 ft

1.9  
2.7  
2.7  
1.6

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pie

PGRM: Abutment

Route 284 St Stream Choteau Ck MRM \_\_\_\_\_ Date 10/10/11 Initials Ch

Bridge Structure No. 22211160 Location 5.9 mi W of Delmont on 284 St

GPS coordinates: N 43° 16' 05.9" W 098° 16' 58.2" taken from: USL abutment  centerline of ↑ MRM end \_\_\_\_\_ Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 178.64 sq. mi.

The average bottom of the main channel was 12.3 ft below top of guardrail at a point 55 ft from left abutment.

Method used to determine flood flows: \_\_\_\_\_ Freq. Anal. \_\_\_\_\_ drainage area ratio \_\_\_\_\_ regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	<u>Q<sub>100</sub> = Q<sub>50</sub> = 4700</u>			<u>Q<sub>500</sub> = Q<sub>25</sub> = 3010</u>		
Estimated flow passing through bridge	<u>3298</u>			<u>3010</u>		
Estimated road overflow & overtopping	<u>1402</u>			<u>        </u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping	<input checked="" type="checkbox"/>				<input checked="" type="checkbox"/>	
Chance of Pressure flow	<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

8/23  
 2 | 165  
 5 | 706  
 10 | 1450  
 25 | 3010  
 50 | 4700  
 100 | 6920  
 500 | 14500

Riprap at abutments? \_\_\_\_\_ Yes \_\_\_\_\_ No  Marginal *Looks like most has washed away*  
 Evidence of past Scour?  Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know *Abutment*  
 Debris Potential? \_\_\_\_\_ High \_\_\_\_\_ Med  Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know \_\_\_\_\_ NA  
 Spur Dike \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know  NA  
 Other \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know  NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay  Sand \_\_\_\_\_ Gravel \_\_\_\_\_ Cobbles \_\_\_\_\_ Boulders \_\_\_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

Photos  
 2082 - ID  
 83 - US  
 84 - US RB  
 85 - US LB  
 86 - L. Abut  
 87 - Pier config  
 88 - L. Abut  
 89 - US Face  
 90 - R. Abut  
 91 - R. Abut  
 \*cattle in stream → bank erosion

Summary of Results

	<u>Q<sub>100</sub> = 50</u>	<u>Q<sub>500</sub> = 25</u>
Bridge flow evaluated	<u>3298</u>	<u>3010</u>
Flow depth at left abutment (yaLT), in feet	<u>2.1</u>	<u>1.9</u>
Flow depth at right abutment (yaRT), in feet	<u>1.0</u>	<u>0.6</u>
Contraction scour depth (y <sub>cs</sub> ), in feet	<u>2.4</u>	<u>2.0</u>
Pier scour depth (y <sub>ps</sub> ), in feet	<u>5.6</u>	<u>5.5</u>
Left abutment scour depth (y <sub>as</sub> ), in feet	<u>8.6</u>	<u>7.8</u>
Right abutment scour depth (y <sub>as</sub> ), in feet	<u>4.3</u>	<u>2.7</u>
Flow angle of attack	<u>0°</u>	<u>0°</u>

See Comments/Diagram for justification where required