

OK RT

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 25297040 Date 7/13/12 Initials Raf Region (A B C D)
Site Location 1 mi N, 1 mi W of Cresbard
Q100 = Q10 1680 by: drainage area ratio flood freq. anal. regional regression eq. X
Bridge discharge (Q2) = 1680 (should be Q100 unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

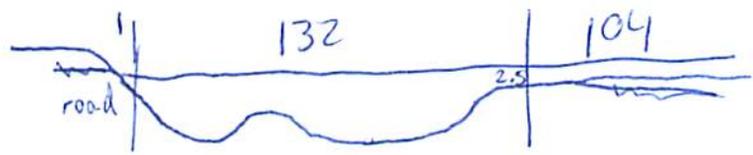
Bridge Width = 104 ft. Flow angle at bridge = 45 degrees Abut. Skew = 0 degrees Effective Skew = 45 degrees
Width (W2) iteration =

Avg. flow depth at bridge, y2 iteration =
Corrected channel width at bridge Section = W2 times cos of flow angle = 73.54 ft\* q2 = Q2/W2 = 22.9 ft^2/s

Bridge Vel, V2 = 2.4 ft/s Final y2 = q2/V2 = 9.5 ft Delta h = 0.1 ft
Average main channel depth at approach section, y1 = Delta h + y2 = 9.6 ft

\* NOTE: repeat above calculations until y2 changes by less than 0.2 Effective pier width = L sin(q) + a cos(q)
If y2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 2-4.1 ft 17.4
Low Steel Elev. = 13.5 ft
n (Channel) = 0.045
n (LOB) = 0.035
n (ROB) = 0.035
Pier Width = 1.7 ft
Pier Length = 1.65 ft
# Piers for 100 yr = 4



CONTRACTION SCOUR

Width of main channel at approach section W1 = 132 ft
Width of left overbank flow at approach, Wlob = 1 ft Average left overbank flow depth, ylob = 0.3 ft
Width of right overbank flow at approach, Wrob = 104 ft Average right overbank flow depth, yrob = 2.5 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)
x = 11.43 From Figure 9 W2 (effective) = 66.7 ft ycs = 12.5 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)
Estimated bed material D50 = ft Average approach velocity, V1 = Q100/(y1W1) = ft/s
Critical approach velocity, Vc = 11.17y1^(1/6)D50^(1/3) = ft/s
If V1 < Vc and D50 >= 0.2 ft, use clear water equation below, otherwise use live bed scour equation above.
Dc50 = 0.0006(q2/y1^(7/6))^3 = ft If D50 >= Dc50, zeta = 0.0
Otherwise, zeta = 0.122y1[q2/(D50^(1/3)y1^(7/6))]^(6/7) - y1 = ft From Figure 10, ycs = ft

PIER SCOUR CALCULATIONS

L/a ratio = 0.97 Correction factor for flow angle of attack (from Table 1), K2 = 1
Froude # at bridge = 0.14 Using pier width a on Figure 11, xi = 7 Pier scour yps = 5.2 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, yalT = 0.3 ft right abutment, yarT = 2.5 ft
Shape coefficient K1 = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
Using values for yalT and yarT on figure 12, psiLT = 1.4 and psiRT = 10.2
Left abutment scour, yas = psiLT(K1/0.55) = 1.4 ft Right abutment scour yas = psiRT(K1/0.55) = 10.2 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Pier

PRGM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 25291040 Date 7/13/12 Initials Lat Region (A B C D) D  
 Site \_\_\_\_\_ Location 1 mi N, 1 mi W of Cresbard  
 $Q_{500} =$  Q<sub>25</sub> 3610 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 3273 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

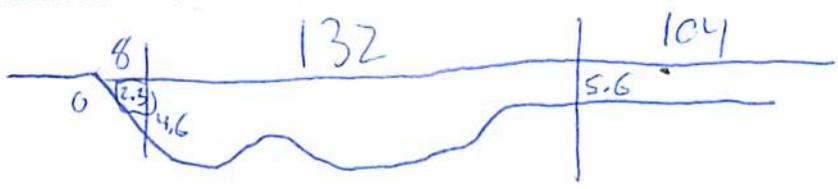
Bridge Width = 104 ft. Flow angle at bridge = 45 ° Abut. Skew = 0 ° Effective Skew = 45 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_

Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 73.54 ft\*  $q_2 = Q_2/W_2 =$  44.5 ft<sup>2</sup>/s

Bridge Vel,  $V_2 =$  3.3 ft/s Final  $y_2 = q_2/V_2 =$  13.5 ft  $\Delta h =$  0.2 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  13.7 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 24.0 ft  
 Low Steel Elev. = 13.4 ft  
 $n$  (Channel) = 0.045  
 $n$  (LOB) = 0.035  
 $n$  (ROB) = 0.035  
 Pier Width = 1.7 ft  
 Pier Length = 1.65 ft  
 # Piers for 500 yr = 4



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  132 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  8 ft Average left overbank flow depth,  $y_{lob} =$  2.3 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  104 ft Average right overbank flow depth,  $y_{rob} =$  5.6 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  19.68 From Figure 9  $W_2$  (effective) = 66.7 ft  $y_{cs} =$  17.5 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} >= 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2/y_1)^{7/6} =$  \_\_\_\_\_ ft If  $D_{50} >= D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

$L/a$  ratio = 0.97 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.16 Using pier width  $a$  on Figure 11,  $\xi =$  7 Pier scour  $y_{ps} =$  5.3 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  2.3 ft right abutment,  $y_{aRT} =$  5.6 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  9.4 and  $\psi_{RT} =$  16.1  
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  9.4 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  16.1 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCSNEW

PRGM: Pier

PRGM: Abutment

11 486'21, 11 056  
11 985, 15 086

11 2281'31  
11 9655

Route 152<sup>nd</sup> St Stream North Fork Snake Ck MRM \_\_\_\_\_ Date 7/13/17 Initials RAT

Bridge Structure No. 25297040 Location 1 mi N, 1 mi W of Cresbard

GPS coordinates: N 45° 11' 13.2" taken from: USL abutment  centerline of ↑ MRM end \_\_\_\_\_  
W 96° 57' 55.9" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 323.53 sq. mi.

The average bottom of the main channel was 17.4 ft below top of guardrail at a point 49 ft from left abutment.

Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio  regional regression equations.

**MISCELLANEOUS CONSIDERATIONS**

Flows	$Q_{100} = Q_{10}$ <u>1680</u>			$Q_{300} = Q_{25}$ <u>3610</u>		
Estimated flow passing through bridge	<u>1680</u>			<u>3273</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>337</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Chance of Pressure flow		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

712  
 2 | 165  
 5 | 290  
 10 | 1680  
 25 | 3610  
 50 | 5710  
 100 | 7470  
 500 | 17900

Riprap at abutments? \_\_\_ Yes \_\_\_ No  Marginal ~~adequate~~ only on left right abutment  
 Evidence of past Scour?  Yes \_\_\_ No \_\_\_ Don't know some contraction/pier and significant abutment  
 Debris Potential? \_\_\_ High \_\_\_ Med  Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_ Yes \_\_\_ No  Don't know \_\_\_ NA  
 Spur Dike \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Other \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA

**Bed Material Classification Based on Median Particle Size ( $D_{50}$ )**

Material Silt/Clay  Sand \_\_\_ Gravel \_\_\_ Cobbles \_\_\_ Boulders \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos  
 1) left ab  
 2) main channel  
 3) right ab  
 4) pier  
 5-8) right abutment  
 9-11) left abutment

**Summary of Results**

	$Q_{100} = Q_{10}$	$Q_{500} = Q_{25}$
Bridge flow evaluated	<u>1680</u>	<u>3273</u>
Flow depth at left abutment (yaLT), in feet	<u>0.3</u>	<u>2.3</u>
Flow depth at right abutment (yaRT), in feet	<u>2.5</u>	<u>5.6</u>
Contraction scour depth (yca), in feet	<u>12.5</u>	<u>17.5</u>
Pier scour depth (yp), in feet	<u>5.2</u>	<u>5.3</u>
Left abutment scour depth (yas), in feet	<u>1.4</u>	<u>9.4</u>
Right abutment scour depth (yas), in feet	<u>10.2</u>	<u>16.1</u>
Flow angle of attack	<u>45</u>	<u>45</u>

See Comments/Diagram for justification where required