

OK RJ

### SCOUR ANALYSIS AND REPORTING FORM

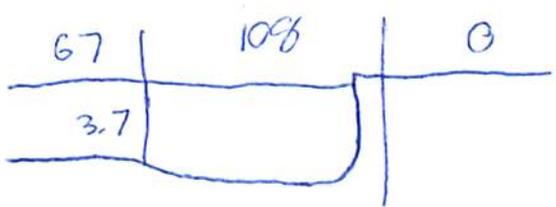
Bridge Structure No. 25300061 Date 7/13/12 Initials RJ Region ( A B C D ) D  
 Site \_\_\_\_\_ Location 0.7 mi S, 0.6 mi W of Crestard on 361 Ave  
 $Q_{100} = Q_c$  967 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 967 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 67 ft. Flow angle at bridge = 20 ° Abut. Skew = 0 ° Effective Skew = 20 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_  
 Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 62.96 ft\*  $q_2 = Q_2/W_2 = \frac{15.4}{62.96}$  ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 = \frac{Q_2}{W_2 y_2} = \frac{15.4}{62.96 \times 7.7} = 0.1$  ft/s Final  $y_2 = q_2/V_2 = 7.7$  ft  $\Delta h = 7.7 - 0.1 = 7.6$  ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = 7.6 + 0.1 = 7.7$  ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD,

Water Surface Elev. = 0-0.9 ft  
 Low Steel Elev. = 7.9 ft  
 n (Channel) = 0.040  
 n (LOB) = 0.035  
 n (ROB) = 0.025  
 Pier Width = 0 ft  
 Pier Length = 0 ft  
 # Piers for 100 yr = 0 ft



#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 = 108$  ft  
 Width of left overbank flow at approach,  $W_{lob} = 67$  ft Average left overbank flow depth,  $y_{lob} = 3.7$  ft  
 Width of right overbank flow at approach,  $W_{rob} = 0$  ft Average right overbank flow depth,  $y_{rob} = 0$  ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x = 8.32$  From Figure 9  $W_2$  (effective) = 63 ft  $y_{cs} = 9.2$  ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

#### PIER SCOUR CALCULATIONS

L/a ratio = \_\_\_\_\_ Correction factor for flow angle of attack (from Table 1),  $K_2 =$  \_\_\_\_\_  
 Froude # at bridge = \_\_\_\_\_ Using pier width a on Figure 11,  $\xi =$  \_\_\_\_\_ Pier scour  $y_{ps} =$  \_\_\_\_\_ ft

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} = 3.7$  ft right abutment,  $y_{aRT} = 0$  ft  
 Shape coefficient  $K_1 = 1.00$  for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = 12.7$  and  $\psi_{RT} = 0$   
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1/0.55) = 19$  ft Right abutment scour  $y_{as} = \psi_{RT} (K_1/0.55) = 0$  ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNSWE

PRGM: Pier

PRGM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 25300061 Date 7/13/12 Initials Rout Region (A B C D) D  
 Site \_\_\_\_\_ Location 0.7 mi S, 0.6 mi W of Cresbard on 361 Ave  
 $Q_{500} = Q_c$  2090 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 1020 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 67 ft. Flow angle at bridge = 20 ° Abut. Skew = 0 ° Effective Skew = 20 °

Width ( $W_2$ ) iteration = \_\_\_\_\_

Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_

Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 62.96 ft\*  $q_2 = Q_2/W_2 = 16.2$  ft<sup>2</sup>/s

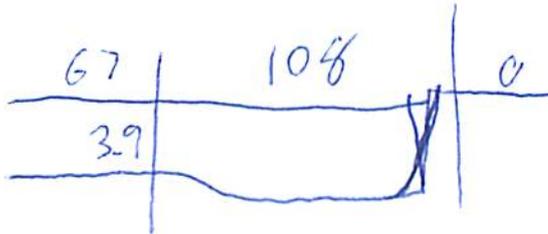
Bridge Vel,  $V_2 = 2.1$  ft/s Final  $y_2 = q_2/V_2 = 7.9$  ft  $\Delta h = 0.1$  ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = 8$  ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD,

Water Surface Elev. = 0-0.9 ft  
 Low Steel Elev. = 7.9 ft  
 $n$  (Channel) = 0.040  
 $n$  (LOB) = 0.035  
 $n$  (ROB) = 0.035  
 Pier Width = 0 ft  
 Pier Length = 0 ft  
 # Piers for 500 yr = 0 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 = 108$  ft  
 Width of left overbank flow at approach,  $W_{lob} = 67$  ft Average left overbank flow depth,  $y_{lob} = 3.9$  ft  
 Width of right overbank flow at approach,  $W_{rob} = 0$  ft Average right overbank flow depth,  $y_{rob} = 0$  ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x = 8.60$  From Figure 9  $W_2$  (effective) = 63 ft  $y_{cs} = 9.5$  ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

$L/a$  ratio = \_\_\_\_\_ Correction factor for flow angle of attack (from Table 1),  $K_2 =$  \_\_\_\_\_  
 Froude # at bridge = \_\_\_\_\_ Using pier width  $a$  on Figure 11,  $\xi =$  \_\_\_\_\_ Pier scour  $y_{ps} =$  \_\_\_\_\_ ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} = 3.9$  ft right abutment,  $y_{aRT} = 0$  ft  
 Shape coefficient  $K_1 = 1.00$  for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = 13.1$  and  $\psi_{RT} = 0$   
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1/0.55) = 19.5$  ft Right abutment scour  $y_{as} = \psi_{RT} (K_1/0.55) = 0$  ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCSNEW

PGRM: Pie

PGRM: Abutment

450 91 2197  
980 57 37  
11951's 1,  
9896078

1000000

11/11/11

1000000

Route 361 Ave Stream North Fork Snake Cr MRM \_\_\_\_\_ Date 7/13/12 Initials RAT  
 Bridge Structure No. 25300061 Location 0.7 mi S, 0.6 mi W of Cresbard on 361 Ave  
 PS coordinates: N 45° 9' 21.61" taken from: USL abutment centerline of ↑ MRM end \_\_\_\_\_  
W 98° 57' 37.81" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 481.54 sq. mi.  
 The average bottom of the main channel was 13.1 ft below top of guardrail at a point 28 ft from left abutment.  
 Method used to determine flood flows: \_\_\_\_\_ Freq. Anal. \_\_\_\_\_ drainage area ratio  regional regression equations.

**MISCELLANEOUS CONSIDERATIONS**

Flows	Q <sub>100</sub> = <u>Q<sub>s</sub> 967</u>			Q <sub>500</sub> = <u>Q<sub>ya</sub> 2090</u>		
	Yes	No	Possibly	Yes	No	Possibly
Estimated flow passing through bridge						
Estimated road overflow & overtopping						
Consideration						
Chance of overtopping		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Chance of Pressure flow		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

712  
 2 195  
 5 967  
 10 2090  
 25 4550  
 50 7260  
 100 10900  
 500 23300

Riprap at abutments? \_\_\_\_\_ Yes \_\_\_\_\_ No  Marginal  
 Evidence of past Scour?  Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know *minor contraction*  
 Debris Potential? \_\_\_\_\_ High \_\_\_\_\_ Med  Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know \_\_\_\_\_ NA  
 Spur Dike \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know \_\_\_\_\_ NA  
 Other \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know \_\_\_\_\_ NA

**Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)**

Material Silt/Clay  Sand \_\_\_\_\_ Gravel \_\_\_\_\_ Cobbles \_\_\_\_\_ Boulders \_\_\_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

- 1) left ab
- 2) main channel
- 3) right ab
- 4-5) right abutment
- 6-7) left abutment
- 8) debris

9) main channel

**Summary of Results**

	Q <sub>100</sub> Q <sub>s</sub>	Q <sub>500</sub> Q <sub>10</sub>
Bridge flow evaluated	967	1020
Flow depth at left abutment (yaLT), in feet	3.7	3.9
Flow depth at right abutment (yaRT), in feet	0	0
Contraction scour depth (y <sub>cs</sub> ), in feet	9.2	9.5
Pier scour depth (y <sub>ps</sub> ), in feet	N/A	N/A
Left abutment scour depth (y <sub>as</sub> ), in feet	19	19.5
Right abutment scour depth (y <sub>as</sub> ), in feet	0	0
Flow angle of attack	20	20

See Comments/Diagram for justification where required