	SCOUR ANALYSIS AND REPORTING FORM
	Bridge Structure No. 254/02/9 Date 7/16/17 Initials Region (ABCD)
	Site Location 2 m; Not Zell on 372 nd Av
	Que = G16 776 by: drainage area ratio flood freq. anal. regional regression eq. X
	Bridge discharge $(Q_2) = 776$ (should be $Q_{100}$ unless there is a relief bridge, road overflow, or bridge overtopping)
	Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method
	Bridge Width = $\frac{6}{16}$ ft. Flow angle at bridge = $\frac{15}{16}$ Abut. Skew = $\frac{15}{16}$ ° Effective Skew = $\frac{15}{16}$ °
	Width (W <sub>2</sub> ) iteration =
"Qui	Avg. flow depth at bridge, $y_2$ iteration =
or "RegionD"	Avg. flow depth at bridge, $y_2$ iteration =
or "	Bridge Vel, $V_2 = \underline{\hspace{1cm}}$ ft/s Final $y_2 = q_2/V_2 = \underline{\hspace{1cm}}$ ft $\Delta h = \underline{\hspace{1cm}}$ ft
nC"	Average main channel depth at approach section, $y_1 = \Delta h + y_2 = 6$ ft
RegionC",	* NOTE: repeat above calculations until y 1 changes by less than 0.2 Effective pier width = L sin(q) + a cos(q)  Why is above LS then account for Road Overflow using PRGM: RDOVREGA RDOVREGA RDOVREGA OVERFORD.
	If y 2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD,
	Water Surface Elev. = $0.976$ , ft
	Low Steel Elev. = 6.6 ft n (Channel) = 0.040
	$n \text{ (LOB)} = \frac{0.03c}{0.03c}$
	$n(ROB) = \underline{G.030}$
	Pier Width =ft Pier Length =ft
	Pier Length =
	CONTRACTION SCOUR
	Width of main channel at approach section $W_1 = \frac{46}{46}$ ft  Width of left overbank flow at approach $W_{th} = \frac{46}{46}$ ft  Average left overbank flow depth, $v_{th} = \frac{2.6}{46}$ ft
2	Width of left evertains new at appreach, who
3	Width of right overbank flow at approach, $W_{rob} = \frac{46}{100}$ ft Average right overbank flow depth, $y_{rob} = \frac{3}{100}$ ft
	Live Bed Contraction Scour (use if bed material is small cobbles or finer)
-	$x = 5.17$ From Figure 9 $W_2$ (effective) = $\frac{99.9}{100}$ ft $y_{cs} = \frac{5.8}{100}$ ft
1	Clear Water Contraction Scour (use if bed material is larger than small cobbles)
3	Estimated bed material $D_{50} = \frac{\text{ft}}{\sqrt{16} \text{ps}}$ Average approach velocity, $V_1 = Q_{100}/(y_1 W_1) = \frac{\text{ft/s}}{\sqrt{16} \text{ps}}$
5	Critical approach velocity, $Vc = 11.17y_1^{1/6}D_{50}^{1/3} = $ ft/s If $V_1 < V_c$ and $D_{50} >= 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above.
N N	$D_{c50} = 0.0006(q_2/y_1^{7/6})^3 = $ ft If $D_{50} >= D_{c50}$ , $\chi = 0.0$
	Otherwise, $\chi = 0.122y_1[q_2/(D_{50}^{1/3}y_1^{7/6})]^{6/7} - y_1 =$ From Figure 10, $y_{cs} =$ ft
	Otherwise, $\chi = 0.122 y_1 [q_2/(D_{50} - y_1)] - y_1 - y_2$
101	PIER SCOUR CALCULATIONS
OKM. Pier	L/a ratio = Correction factor for flow angle of attack (from Table 1), K2 =
5	Froude # at bridge =ft  Using pier width a on Figure 11, $\xi$ =ft
	ABUTMENT SCOUR CALCULATIONS
nent	Average flow depth blocked by: left abutment, $y_{al.T} = 2.6$ ft right abutment, $y_{aRT} = 3.7$ ft
GKM. Abument	Shape coefficient $K_1$ = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls. Using values for $y_{aLT}$ and $y_{aRT}$ on figure 12, $\psi_{LT}$ = 1.00 for vertical-wall with wingwalls. 0.55 for spill-through
KM	Using values for $y_{aLT}$ and $y_{aRT}$ on figure 12, $\psi_{LT} = 10^{-6}$ and $\psi_{RT} = 10^{-6}$
7	Left abutment scour, $y_{as} = \psi_{LT}(K_1/0.55) = 15.8$ ft Right abutment scour $y_{as} = \psi_{RT}(K_1/0.55) = 17.7$ ft

hb9267hh

43678,550hh

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100	46	17.7	 All In
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Route 372 Ave Stream Dove CK		MRM	Dat	e 7/16/17	Init	ials Rat		
Bridge Structure No. 264/62/9 Loc	ation 角 🗸	n: 1/ f	7-11 0	3/2	-c An			
GPS coordinates: N 440 551 37.0(1)	taken from:	USL abutmen	t ×	centerline o	of ↑ MRM €	end		
N 960 44' B.8'	Datum of co	ordinates: Wo	GS84 ×	NAD27				
Drainage area = 7254 sq. mi.								
The average bottom of the main channel was	4 ft below	top of guardr	ail at a noin	. 17	ft from le	ft abutment		
Method used to determine flood flows:Freq.	Anal	drainage area t	ratio V	regional reg	ression equ	ations	71	5
Method used to determine flood flows1 req.	Allai	aramage area i	atto	regional reg	ression equ	ations.	21	<u></u>
MIS	SCELLANE	OUS CONSII	DERATION	NS			610	25
Flows	Q400 = Qx 776			Q500=G21570			25	1 92.5
Estimated flow passing through bridge	776			776 971			5	386
Estimated road overflow & overtopping	0			649 599			10	776
Consideration	Yes	No	Possibly	Yes	No	Possibly	25	1570
Chance of overtopping		X		X			50	2400
Chance of Pressure flow		×		>			100	3460
Armored appearance to channel		~			>			6960
Lateral instability of channel		7			X		500	10100
	NI.	N4		1 . 4	den			
Riprap at abutments?	No _	Marginal	minor	OCCUM LOCA	101	(I		
Evidence of past Scour?Yes	No	Don't know	1'kel ab	stront Lun	de i water)			
Riprap at abutments? Yes Yes Evidence of past Scour? Yes High	Med	<_Low						
Does scour countermeasure(s) appear to have been	designed?							
RiprapY	es $\chi$ N	oDor	n't know	NA				
Spur DikeY	es V N	o Do	n't know	NA				
Other V	oc X N	oDor	n't know	NΑ				
OtherY	C5		i t know					
Bed Material	Classificatio	n Based on Mo	edian Partic	le Size (D <sub>50</sub>	)			
				Cobbles		Boulders		
	Gravel .00 2.00-64							
Size range, in mm <0.062 0.062-2.	00	2.00-64		64-250		>250		
Comments, Diagrams & orientation of digital phot	os							
D. Left CB								
2). main chance! 3). night CMS 4). left & abudnest 5) right abudnest								
2) o'ut on								
10 1 51 0 1 1 7								
4), left so abushes								
Stright shutmost								
6) main Changel								
The state of the s								
Summary of Results		Olar (	10		Q500	3	٦	
Duides flow analysted		776 776	10		\$ 9	719	-	
Bridge flow evaluated Flow depth at left abutment (yaLT), in feet	2.6		3.4			-		
Flow depth at right abutment (yaL1), in feet	3.2		3.9			-		
Contraction scour depth (yes), in feet	5.8			7.7			1	
Pier scour depth (yps), in feet		NIA			N/A		1	
Left abutment scour depth (yas), in feet		15.6			18.2			
Right abutment scour depth (yas), in feet		17.7			19.5			
1Flow angle of attack		15			15			