

OK RT

### SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 26230091 Date 8/4/12 Initials Raf Region (A B C D)  
 Site \_\_\_\_\_ Location 1 mi S, 1 mi E of Twin Brooks on 472 Ave  
 $Q_{100} =$  604 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 804 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 27 ft. Flow angle at bridge = 5 ° Abut. Skew = 0 ° Effective Skew = 5 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_

Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_

Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 26.9 ft\*  $q_2 = Q_2/W_2 =$  29.9 ft<sup>2</sup>/s

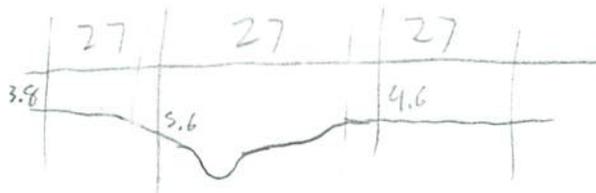
Bridge Vel,  $V_2 =$  3.9 ft/s Final  $y_2 = q_2/V_2 =$  7.7 ft  $\Delta h =$  0.3 ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  8 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = dry ft  
 Low Steel Elev. = 7.9 ft  
 $n$  (Channel) = 0.040  
 $n$  (LOB) = 0.035  
 $n$  (ROB) = 0.035  
 Pier Width = 0 ft  
 Pier Length = 0 ft  
 # Piers for 100 yr = 0 ft



56 38  
 1.26  
 46

#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 =$  27 ft

Width of left overbank flow at approach,  $W_{lob} =$  27 ft

Average left overbank flow depth,  $y_{lob} =$  5.0 ft

Width of right overbank flow at approach,  $W_{rob} =$  27 ft

Average right overbank flow depth,  $y_{rob} =$  4.6 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  2.87 From Figure 9  $W_2$  (effective) = 26.9 ft  $y_{cs} =$  7.7 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

#### PIER SCOUR CALCULATIONS

L/a ratio = \_\_\_\_\_

Correction factor for flow angle of attack (from Table 1),  $K_2 =$  \_\_\_\_\_

Froude # at bridge = \_\_\_\_\_

Using pier width  $a$  on Figure 11,  $\xi =$  \_\_\_\_\_ Pier scour  $y_{ps} =$  \_\_\_\_\_ ft

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} =$  5.0 ft right abutment,  $y_{aRT} =$  4.6 ft

Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through

Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  15 and  $\psi_{RT} =$  14.3

Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) =$  27.3 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) =$  26.0 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pier

PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 26230091 Date 8/4/12 Initials Pat Region (A B C D)  
 Site \_\_\_\_\_ Location 1 mi S, 1 mi E of Twin Brooks on 472 Ave  
 $Q_{500} =$  1260 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 821 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 27 ft. Flow angle at bridge = 5 ° Abut. Skew = 0 ° Effective Skew = 5 °

Width ( $W_2$ ) iteration = \_\_\_\_\_

Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_

Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 26.9 ft\*  $q_2 = Q_2/W_2 =$  30.5 ft<sup>2</sup>/s

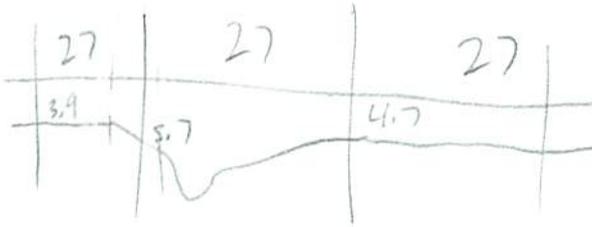
Bridge Vel,  $V_2 =$  3.9 ft/s Final  $y_2 = q_2/V_2 =$  7.8 ft  $\Delta h =$  0.3 ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  8.1 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0.14 ft  
 Low Steel Elev. = 7.9 ft  
 n (Channel) = 0.040  
 n (LOB) = 0.035  
 n (ROB) = 0.035  
 Pier Width = 0 ft  
 Pier Length = 0 ft  
 # Piers for 500 yr = 0 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  27 ft

Width of left overbank flow at approach,  $W_{lob} =$  27 ft

Average left overbank flow depth,  $y_{lob} =$  5.1 ft

Width of right overbank flow at approach,  $W_{rob} =$  27 ft

Average right overbank flow depth,  $y_{rob} =$  4.7 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  8.08 From Figure 9  $W_2$  (effective) = 26.9 ft  $y_{cs} =$  8.9 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = \_\_\_\_\_

Correction factor for flow angle of attack (from Table 1),  $K_2 =$  \_\_\_\_\_

Froude # at bridge = \_\_\_\_\_

Using pier width a on Figure 11,  $\xi =$  \_\_\_\_\_ Pier scour  $y_{ps} =$  \_\_\_\_\_ ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  5.1 ft right abutment,  $y_{aRT} =$  4.7 ft

Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through

Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  15.2 and  $\psi_{RT} =$  14.5

Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) =$  27.6 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) =$  26.3 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCSNEW

PRGM: Pier

PRGM: Abutment

96.76185  
45.19165

450 11' 29" 94  
96 45' 42" 95

Route 472 Ave Stream \_\_\_\_\_ MRM \_\_\_\_\_ Date 8/4/12 Initials RAT  
 Bridge Structure No. 26230091 Location 1 mi S, 1 mi E of Twin Brooks on 472 Ave  
 GPS coordinates: N 45° 11' 30.31" taken from: USL abutment  centerline of ↑ MRM end \_\_\_\_\_  
W 96° 45' 43.71" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 6.57 sq. mi.  
 The average bottom of the main channel was 11.8 ft below top of guardrail at a point 21 ft from left abutment.  
 Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio  regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = <u>804</u>			Q <sub>500</sub> = <u>1260</u>			2	63.2
Estimated flow passing through bridge	<u>804</u>			<u>821</u>			5	178
Estimated road overflow & overtopping	<u>0</u>			<u>439</u>			10	290
Consideration	Yes	No	Possibly	Yes	No	Possibly	25	471
Chance of overtopping		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>			50	629
Chance of Pressure flow	<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>			100	804
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>		500	1260
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>			

Riprap at abutments? \_\_\_ Yes \_\_\_ No  Marginal *see pictures*  
 Evidence of past Scour?  Yes \_\_\_ No \_\_\_ Don't know *mine, contraction*  
 Debris Potential? \_\_\_ High \_\_\_ Med  Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Spur Dike \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Other \_\_\_\_\_ \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay  Sand \_\_\_ Gravel \_\_\_ Cobbles \_\_\_ Boulders \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

- 1). left ab.
- 2). main channel
- 3). right ab.
- 4-5). right abutment
- 6-7). left abutment
- 8). main channel

Summary of Results

	Q100	Q500
Bridge flow evaluated	<u>804</u>	<u>821</u>
Flow depth at left abutment (yaLT), in feet	<u>5.0</u>	<u>5.1</u>
Flow depth at right abutment (yaRT), in feet	<u>4.6</u>	<u>4.7</u>
Contraction scour depth (yca), in feet	<u>8.7</u>	<u>8.9</u>
Pier scour depth (yps), in feet	<u>N/A</u>	<u>N/A</u>
Left abutment scour depth (yas), in feet	<u>27.3</u>	<u>27.6</u>
Right abutment scour depth (yas), in feet	<u>26.0</u>	<u>26.3</u>
IFlow angle of attack	<u>5</u>	<u>5</u>

See Comments/Diagram for justification where required