

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 26330038 Date 10-11-11 Initials RT Region (A B C D) (C)
 Site _____ Location From Millbank, 3E, 3.2N
 $Q_{100} =$ 7130 by: drainage area ratio _____ flood freq. anal. _____ regional regression eq.
 Bridge discharge (Q_2) = _____ (should be Q_{100} unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 160 ft. Flow angle at bridge = 13 ° Abut. Skew = 0 ° Effective Skew = 13 °
 Width (W_2) iteration = 156 158
 Avg. flow depth at bridge, y_2 iteration = 9.7 9.6

Corrected channel width at bridge Section = W_2 times cos of flow angle = 154 ft* $q_2 = Q_2/W_2 =$ 46.3 ft²/s

Bridge Vel, $V_2 =$ 4.8 ft/s Final $y_2 = q_2/V_2 =$ 9.6 ft $\Delta h =$ 0.5 ft

Average main channel depth at approach section, $y_1 = \Delta h + y_2 =$ 10.1 ft

* NOTE: repeat above calculations until y_2 changes by less than 0.2 Effective pier width = $L \sin(q) + a \cos(q)$

If y_2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD,

Water Surface Elev. = 1.2 ft
 Low Steel Elev. = 12.4 ft
 n (Channel) = .027
 n (LOB) = .030
 n (ROB) = .029
 Pier Width = 0.9 ft
 Pier Length = 1.2 ft
 # Piers for 100 yr = 2 ft

assume ROB fence line acts as a guidebank @ Q_{100} and thus there is no right overbank width at Q_{100} .

CONTRACTION SCOUR

Width of main channel at approach section $W_1 =$ 160 ft *assume 1.5 bridge lengths*
 Width of left overbank flow at approach, $W_{lob} =$ 240 ft Average left overbank flow depth, $y_{lob} =$ 0.7 ft
 Width of right overbank flow at approach, $W_{rob} =$ 0 ft Average right overbank flow depth, $y_{rob} =$ 0 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$ 0.69 From Figure 9 W_2 (effective) = 152.2 ft $y_{cs} =$ 1.1 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material $D_{50} =$ _____ ft Average approach velocity, $V_1 = Q_{100}/(y_1 W_1) =$ _____ ft/s

Critical approach velocity, $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$ ~~_____~~ ft/s

If $V_1 < V_c$ and $D_{50} \geq 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006(q_2/y_1^{7/6})^3 =$ _____ ft If $D_{50} \geq D_{c50}$, $\chi = 0.0$

Otherwise, $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$ _____ From Figure 10, $y_{cs} =$ _____ ft

PIER SCOUR CALCULATIONS

L/a ratio = 1.33 Correction factor for flow angle of attack (from Table 1), $K_2 =$ 1
 Froude # at bridge = 0.27 Using pier width a on Figure 11, $\xi =$ 4.4 Pier scour $y_{ps} =$ 3.6 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, $y_{aLT} =$ 0.7 ft right abutment, $y_{aRT} =$ 0 ft
 Shape coefficient $K_1 =$ 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
 Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} =$ 3.1 and $\psi_{RT} =$ 0
 Left abutment scour, $y_{as} = \psi_{LT}(K_1/0.55) =$ 3.1 ft Right abutment scour $y_{as} = \psi_{RT}(K_1/0.55) =$ 0 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"
 PGRM: Contract
 PGRM: CWCSNEW
 PGRM: Pier
 PGRM: Abutment

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 26330038 Date _____ Initials _____ Region (A B **0** D)
 Site _____ Location _____
 $Q_{500} =$ 11,700 by: drainage area ratio _____ flood freq. anal. _____ regional regression eq.
 Bridge discharge (Q_2) = _____ (should be Q_{500} unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 160 ft. Flow angle at bridge = 13 ° Abut. Skew = 0 ° Effective Skew = 13 °
 Width (W_2) iteration = 160
 Avg. flow depth at bridge, y_2 iteration = 12.2
 Corrected channel width at bridge Section = W_2 times cos of flow angle = 156 ft* $q_2 = Q_2/W_2 =$ 75 ft²/s
 Bridge Vel, $V_2 =$ 6.1 ft/s Final $y_2 = q_2/V_2 =$ 12.2 ft $\Delta h =$ 0.8 ft
 Average main channel depth at approach section, $y_1 = \Delta h + y_2 =$ 13.0 ft

* NOTE: repeat above calculations until y_2 changes by less than 0.2 Effective pier width = $L \sin(q) + a \cos(q)$
 If y_2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD,

Water Surface Elev. = 1.2 ft
 Low Steel Elev. = 12.4 ft
 n (Channel) = 0.027
 n (LOB) = 0.030
 n (ROB) = 0.029
 Pier Width = 0.9 ft
 Pier Length = 1.2 ft
 # Piers for 500 yr = 2 ft

CONTRACTION SCOUR

Width of main channel at approach section $W_1 =$ 160 ft ← assume 1.5 bridge lengths
 Width of left overbank flow at approach, $W_{lob} =$ 240 ft ← Average left overbank flow depth, $y_{lob} =$ 3.6 ft
 Width of right overbank flow at approach, $W_{rob} =$ 320 ft ← Average right overbank flow depth, $y_{rob} =$ 1.8 ft
 ← assume 2 bridge lengths
Live Bed Contraction Scour (use if bed material is small cobbles or finer)
 $x =$ 3.56 From Figure 9 W_2 (effective) = 154.2 ft $y_{cs} =$ 4.2 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material $D_{50} =$ _____ ft Average approach velocity, $V_1 = Q_{500}/(y_1 W_1) =$ _____ ft/s
 Critical approach velocity, $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$ N/A ft/s
 If $V_1 < V_c$ and $D_{50} \geq 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above.
 $D_{c50} = 0.0006(q_2/y_1^{7/6})^3 =$ _____ ft If $D_{50} \geq D_{c50}$, $\chi = 0.0$
 Otherwise, $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$ _____ From Figure 10, $y_{cs} =$ _____ ft

PIER SCOUR CALCULATIONS

L/a ratio = 1.33 Correction factor for flow angle of attack (from Table 1), $K_2 =$ 1
 Froude # at bridge = 0.31 Using pier width a on Figure 11, $\xi =$ 4.4 Pier scour $y_{ps} =$ 3.7 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, $y_{aLT} =$ 3.6 ft right abutment, $y_{aRT} =$ 1.8 ft
 Shape coefficient $K_1 =$ 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
 Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} =$ 12.6 and $\psi_{RT} =$ 7.4
 Left abutment scour, $y_{as} = \psi_{LT}(K_1/0.55) =$ 12.6 ft Right abutment scour $y_{as} = \psi_{RT}(K_1/0.55) =$ 7.4 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Pie

PRGM: Abutment

Route 482nd Ave Stream N. Fk Whetstone MRM _____ Date _____ Initials _____

Bridge Structure No. 26330038 Location From Milbank, 3 E, 3.2 N

GPS coordinates: N 95° 16.327' taken from: USL abutment centerline of ↑ MRM end _____
W 96° 33.336' Datum of coordinates: WGS84 NAD27 _____

Drainage area = 396.45 (cont.) sq. mi.

The average bottom of the main channel was 17.9 ft below top of guardrail at a point 44 ft from left abutment.

Method used to determine flood flows: Freq. Anal. drainage area ratio regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q ₁₀₀ = <u>7130</u>			Q ₅₀₀ = <u>11,700</u>		
Estimated flow passing through bridge						
Estimated road overflow & overtopping						
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping						
Chance of Pressure flow						
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel			<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>	

Riprap at abutments? Yes No Marginal
 Evidence of past Scour? Yes No Don't know scour pool under bridge?
 Debris Potential? High Med Low right abutment scour under bridge

Does scour countermeasure(s) appear to have been designed?

Riprap Yes No Don't know NA
 Spur Dike Yes No Don't know NA
 Other Yes No Don't know NA

Bed Material Classification Based on Median Particle Size (D₅₀)

Material	Silt/Clay <input checked="" type="checkbox"/>	Sand <input type="checkbox"/>	Gravel <input type="checkbox"/>	Cobbles <input type="checkbox"/>	Boulders <input type="checkbox"/>
Size range, in mm	<0.062	0.062-2.00	2.00-64	64-250	>250

Comments, Diagrams & orientation of digital photos
a swale and high-flow side channel in the left overbank will help guide water to the bridge opening and may mitigate some of the left abutment scour.

structure photos
approach section from bridge
left overbank
right overbank
bridge from right approach ←
right abutment under bridge

Summary of Results

	Q100	Q500
Bridge flow evaluated	<u>7130</u>	<u>11,700</u>
Flow depth at left abutment (yaLT), in feet	<u>0.7</u>	<u>3.6</u>
Flow depth at right abutment (yaRT), in feet	<u>0</u>	<u>1.8</u>
Contraction scour depth (yca), in feet	<u>1.1</u>	<u>4.2</u>
Pier scour depth (yps), in feet	<u>3.6</u>	<u>3.7</u>
Left abutment scour depth (yas), in feet	<u>3.1</u>	<u>12.6</u>
Right abutment scour depth (yas), in feet	<u>0</u>	<u>7.4</u>
Flow angle of attack	<u>13°</u>	<u>13°</u>

See Comments/Diagram for justification where required

Basin Characteristics from
Provisional StreamStats 10-7-11

Cont. D.A. = 396.45 mi²

PII = 0.97

100% Subregion A

Manually Calculated Peaks

$Q_{100} = 7130 \text{ cfs}$

$Q_{500} = 11,700 \text{ cfs}$