

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 27010073 Date 8/16/11 Initials AW Region (A B C D) B
 Site _____ Location 10.7 mi N of Dallas on 333 Ave
 $Q_{500} =$ 6610 by: drainage area ratio _____ flood freq. anal. _____ regional regression eq.
 Bridge discharge (Q_2) = 6610 (should be Q_{500} unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 97 ft. Flow angle at bridge = 25 ° Abut. Skew = 27 ° Effective Skew = 2 °

Width (W_2) iteration = 97

Avg. flow depth at bridge, y_2 iteration = 9.9 vert wall

Corrected channel width at bridge Section = W_2 times cos of flow angle = 96.94 ft* $q_2 = Q_2/W_2 =$ 68.2 ft²/s

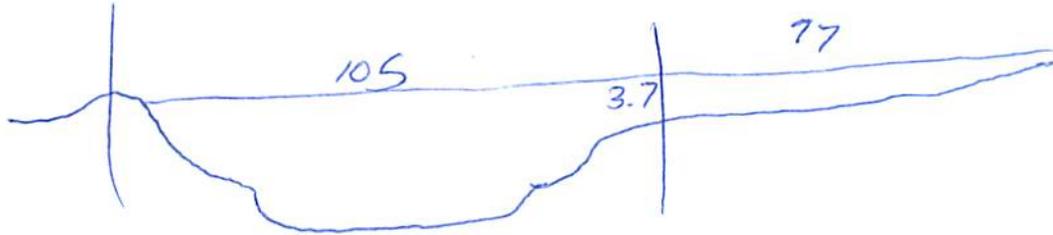
Bridge Vel, $V_2 =$ 6.9 ft/s Final $y_2 = q_2/V_2 =$ 9.9 ft $\Delta h =$ 1.0 ft

Average main channel depth at approach section, $y_1 = \Delta h + y_2 =$ 10.9 ft

* NOTE: repeat above calculations until y_2 changes by less than 0.2 Effective pier width = $L \sin(q) + a \cos(q)$

If y_2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = _____ ft
 Low Steel Elev. = 12.7 ft
 n (Channel) = 0.033
 n (LOB) = 0.040
 n (ROB) = 0.040
 Pier Width = 2.0 ft
 Pier Length = 2.0 ft
 # Piers for 500 yr = 2 ft



CONTRACTION SCOUR

Width of main channel at approach section $W_1 =$ 105 ft

Width of left overbank flow at approach, $W_{lob} =$ 0.0 ft

Width of right overbank flow at approach, $W_{rob} =$ 97 ft

Average left overbank flow depth, $y_{lob} =$ 0.0 ft

Average right overbank flow depth, $y_{rob} =$ 3.7 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$ 2.96 From Figure 9 W_2 (effective) = 92.9 ft $y_{cs} =$ 3.5 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material $D_{50} =$ _____ ft Average approach velocity, $V_1 = Q_{500}/(y_1 W_1) =$ _____ ft/s

Critical approach velocity, $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$ _____ ft/s

If $V_1 < V_c$ and $D_{50} \geq 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1)^{7/6} =$ _____ ft If $D_{50} \geq D_{c50}$, $\chi = 0.0$

Otherwise, $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$ _____ From Figure 10, $y_{cs} =$ _____ ft

PIER SCOUR CALCULATIONS

L/a ratio = 1.0
 Froude # at bridge = 0.39

Correction factor for flow angle of attack (from Table 1), $K_2 =$ 1.0
 Using pier width a on Figure 11, $\xi =$ 8.0 Pier scour $y_{ps} =$ 6.9 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, $y_{aLT} =$ 0.0 ft right abutment, $y_{aRT} =$ 3.7 ft
 Shape coefficient $K_1 =$ 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
 Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} =$ 0.0 and $\psi_{RT} =$ 12.7
 Left abutment scour, $y_{as} = \psi_{LT}(K_1/0.55) =$ 0.0 ft Right abutment scour $y_{as} = \psi_{RT}(K_1/0.55) =$ 12.7 ft

2.32 x 12.7 = 29.56

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Pier

PRGM: Abutment

Route 333 Arc Stream Bull CK MRM _____ Date 8/16/11 Initials CM
 Bridge Structure No. 27010073 Location 10.7 mi N of Dallas on 333 Arc
 GPS coordinates: N 43° 23' 45.0" taken from: USL abutment centerline of \uparrow MRM end _____
W 99° 30' 52.1" Datum of coordinates: WGS84 NAD27 _____

Drainage area = 62.4 sq. mi.
 The average bottom of the main channel was 16.6 ft below top of guardrail at a point 28 ft from left abutment.
 Method used to determine flood flows: ___ Freq. Anal. ___ drainage area ratio regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q ₁₀₀ = <u>3930</u>			Q ₅₀₀ = <u>6610</u>		
Estimated flow passing through bridge	<u>3930</u>			<u>6610</u>		
Estimated road overflow & overtopping						
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Chance of Pressure flow		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

Pks Calc'd 8/8
 2 | 263
 5 | 791
 10 | 1370
 25 | 2210
 50 | 3020
 100 | 3930
 500 | 6610

Riprap at abutments? ___ Yes No ___ Marginal
 Evidence of past Scour? Yes ___ No ___ Don't know *piles exposed under abut*
 Debris Potential? ___ High Med ___ Low

Does scour countermeasure(s) appear to have been designed?
 Riprap ___ Yes ___ No ___ Don't know NA
 Spur Dike ___ Yes ___ No Don't know ___ NA
 Other ___ Yes ___ No ___ Don't know NA

Bed Material Classification Based on Median Particle Size (D₅₀)
 Material Silt/Clay Sand ___ Gravel ___ Cobbles ___ Boulders ___
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos
Photos
 1932-10 37 - scout under L. Abut Too deep to set
 33- US 38 - R. Abut to piers → estim
 34- US RB 39 - spur dike on LB ~ 2.0'
 35- US LB 40 - US Face

Summary of Results

	Q100	Q500
Bridge flow evaluated	<u>3930</u>	<u>6610</u>
Flow depth at left abutment (yaLT), in feet	<u>0</u>	<u>0</u>
Flow depth at right abutment (yaRT), in feet	<u>0.5</u>	<u>3.7</u>
Contraction scour depth (yca), in feet	<u>1.5</u>	<u>3.5</u>
Pier scour depth (yps), in feet	<u>6.8</u>	<u>6.9</u>
Left abutment scour depth (yas), in feet	<u>0</u>	<u>0</u>
Right abutment scour depth (yas), in feet	<u>2.3</u>	<u>12.7</u>
Flow angle of attack	<u>2</u>	<u>2</u>

See Comments/Diagram for justification where required