

ok RT

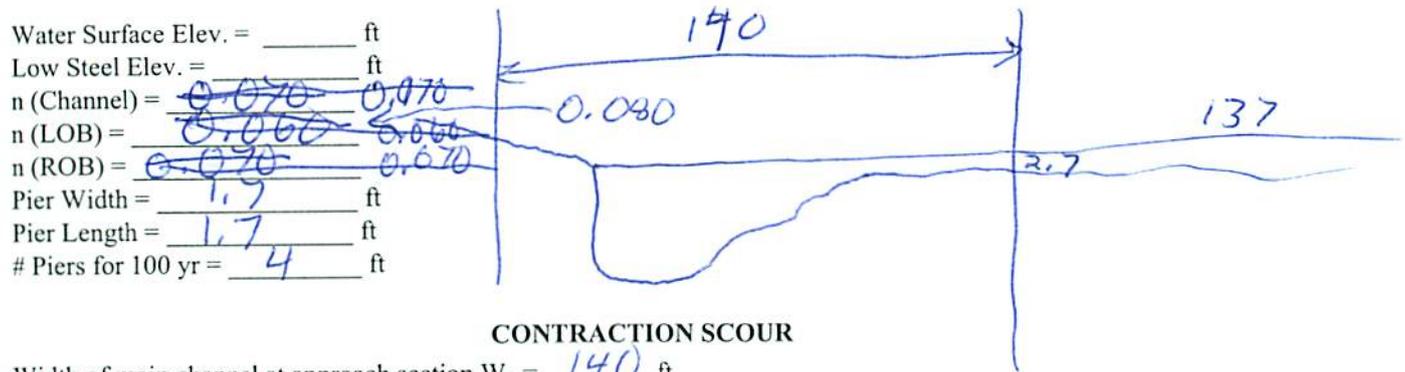
### SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 27089250 Date 8/16/14 Initials CR Region (A B C D) (C)  
 Site \_\_\_\_\_ Location 3 mi S + 3 mi W of Burke on 294 St  
 $Q_{100} =$  7210 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq.   
 Bridge discharge ( $Q_2$ ) = 7210 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 137 ft. Flow angle at bridge = 5 ° Abut. Skew = 0 ° Effective Skew = 5 °  
 Width ( $W_2$ ) iteration = 137 109 126 120 121  
 Avg. flow depth at bridge,  $y_2$  iteration = 8.6 9.4 9.0 9.3 9.2  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 120.54 ft\*  $q_2 = Q_2/W_2 =$  59.8 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  6.5 ft/s Final  $y_2 = q_2/V_2 =$  9.2 ft  $\Delta h =$  0.9 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  10.1 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.



Water Surface Elev. = \_\_\_\_\_ ft  
 Low Steel Elev. = \_\_\_\_\_ ft  
 $n$  (Channel) = ~~0.070~~ 0.070  
 $n$  (LOB) = ~~0.060~~ 0.060  
 $n$  (ROB) = ~~0.070~~ 0.070  
 Pier Width = 1.7 ft  
 Pier Length = 1.7 ft  
 # Piers for 100 yr = 4

#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 =$  140 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  0 ft Average left overbank flow depth,  $y_{lob} =$  0.0 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  137 ft Average right overbank flow depth,  $y_{rob} =$  2.7 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  3.64 From Figure 9  $W_2$  (effective) = 113.7 ft  $y_{cs} =$  4.3 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

#### PIER SCOUR CALCULATIONS

L/a ratio = 1.0 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1.0  
 Froude # at bridge = 0.34 Using pier width  $a$  on Figure 11,  $\xi =$  7.0 Pier scour  $y_{ps} =$  6.1 ft

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} =$  0.8 ft right abutment,  $y_{aRT} =$  2.7 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  0.0 and  $\psi_{RT} =$  11.0  
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  0.10 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  11.0 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

0.100  
0.100

PGRM: Contract

PGRM: CWCSNEW

PGRM: Pier

PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

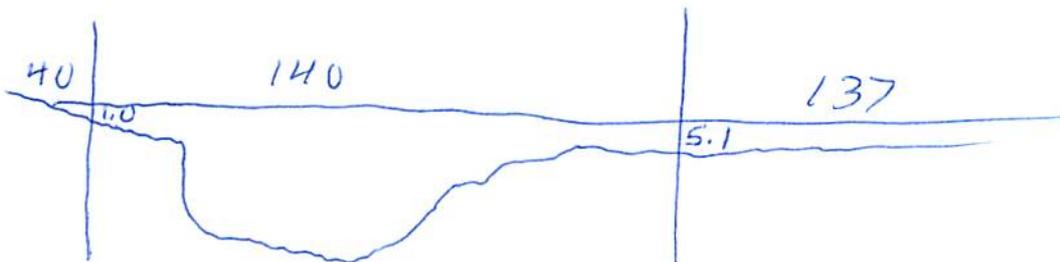
Bridge Structure No. 27089250 Date 8/16/11 Initials CU Region (A B C D) B  
 Site \_\_\_\_\_ Location 3 mi S or 3 mi W of Burke on 294 St  
 $Q_{500} =$  12000 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq.   
 Bridge discharge ( $Q_2$ ) = 12000 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 137 ft. Flow angle at bridge = 5 ° Abut. Skew = 0 ° Effective Skew = 5 °  
 Width ( $W_2$ ) iteration = 137  
 Avg. flow depth at bridge,  $y_2$  iteration = 11.3 Vert Wall  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 136.48 ft\*  $q_2 = Q_2/W_2 =$  87.9 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  7.8 ft/s Final  $y_2 = q_2/V_2 =$  11.3 ft  $\Delta h =$  1.2 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  12.5 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = \_\_\_\_\_ ft  
 Low Steel Elev. = \_\_\_\_\_ ft  
 $n$  (Channel) = 0.070  
 $n$  (LOB) = 0.060  
 $n$  (ROB) = 0.070  
 Pier Width = 1.7 ft  
 Pier Length = 1.7 ft  
 # Piers for 500 yr = 4



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  140 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  40 ft Average left overbank flow depth,  $y_{lob} =$  0.5 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  137 ft Average right overbank flow depth,  $y_{rob} =$  5.1 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  3.98 From Figure 9  $W_2$  (effective) = 129.7 ft  $y_{cs} =$  4.6 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1.0 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1.0  
 Froude # at bridge = 0.41 Using pier width  $a$  on Figure 11,  $\xi =$  7.0 Pier scour  $y_{ps} =$  6.2 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  0.5 ft right abutment,  $y_{aRT} =$  5.1 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  2.3 and  $\psi_{RT} =$  15.2  
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  2.3 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  15.2 ft

5.7  
2.4  
2.7

107  
28  
135

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pie

PGRM: Abutment

0.100  
0.080  
0.100

Route 294 St Stream Ponca CK MRM \_\_\_\_\_ Date 8/16/11 Initials AW  
 Bridge Structure No. 27089256 Location 3 mi S + 3 mi W of Burke on 294 St  
 GPS coordinates: N 43° 08' 25.0" taken from: USL abutment  centerline of ↑ MRM end \_\_\_\_\_  
W 99° 21' 17.8" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 215.4 sq. mi.  
 The average bottom of the main channel was 18.5 ft below top of guardrail at a point 58 ft from left abutment.  
 Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio  regional regression equations.

PK calc'd 8/18

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = <u>7210</u>			Q <sub>500</sub> = <u>12000</u>		
Estimated flow passing through bridge	<u>7210</u>			<u>12000</u>		
Estimated road overflow & overtopping						
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Chance of Pressure flow		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel	<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>		

PK2	Flow
5	495
10	1480
25	2550
50	4090
100	5550
500	7210
	12000

Riprap at abutments?  Yes \_\_\_ No \_\_\_ Marginal  
 Evidence of past Scour?  Yes \_\_\_ No \_\_\_ Don't know  
 Debris Potential?  High \_\_\_ Med \_\_\_ Low

Rip rap added in last couple years b/c channel was eroding banks

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Spur Dike \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Other \_\_\_ Yes \_\_\_ No \_\_\_ Don't know  NA

Dike is remains of old bridge

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay  Sand \_\_\_ Gravel \_\_\_ Cobbles \_\_\_ Boulders \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

- 1971 - ID
- 72 - US
- 73 - US RB
- 74 - US LB
- 75 - L. Abut
- 76 - L. Abut
- 77 - R. Abut
- 78 - US Face
- 79 - R. Abut Rip Rap
- 80 - LB Rip Rap

Spoke w/ Rancher Dave  
 81 - Old bridge abut / Dike Stellen?

Summary of Results

	Q100	Q500
Bridge flow evaluated	7210	12000
Flow depth at left abutment (yaLT), in feet	0	6.5
Flow depth at right abutment (yaRT), in feet	2.7	5.1
Contraction scour depth (yca), in feet	4.3	4.6
Pier scour depth (yp), in feet	6.1	6.2
Left abutment scour depth (yas), in feet	0	2.3
Right abutment scour depth (yas), in feet	11.0	15.2
Flow angle of attack	5	5

See Comments/Diagram for justification where required