	SCOUR ANALYSIS AND REPORTING FORM						
	Bridge Structure No. 27165307 Date 7/11/11 Initials Ch Region (ABCD)						
	Site Location Approx 4.1 SW Herrick on 349 Ave Ponca Creek?  Q <sub>100</sub> = 5860 by: drainage area v flood frequency anal. regional regression eq.						
	Q <sub>100</sub> = by: drainage area flood frequency anal regional regression eq						
	Bridge discharge $(Q_2) = 560$ (should be $Q_{100}$ unless there is a relief bridge, road overflow, or bridge overtopping)						
PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"	Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method  Bridge Width = $\frac{1}{100}$ ft. Flow angle at bridge = $\frac{3}{100}$ Abut. Skew = $\frac{3}{100}$ effective Skew = $\frac{3}{100}$ November 1000 8.8 9.2 19.4  Corrected channel width at bridge Section = $\frac{3}{100}$ ft. Since $\frac{3}{100}$ f						
	CONTRACTION SCOUP						
PGRM: Contract	Width of main channel at approach section $W_1 = \frac{162}{162}$ ft						
	Width of left overbank flow at approach, $W_{lob} = 25$ ft  Average left overbank flow depth, $y_{lob} = 1.5$ ft						
	Width of right overbank flow at approach, $W_{rob} = $ ft Average right overbank flow depth, $y_{rob} = $ ft						
PGR	Live Bed Contraction Scour (use if bed material is small cobbles or finer)						
	$x = 3.05$ From Figure 9 $W_2$ (effective) = 90.8 ft $y_{cs} = 9.9$ ft						
	Clear Water Contraction Secure (use if had material is larger than small cabbles)						
PGRM: CWCSNEW	Clear Water Contraction Scour (use if bed material is larger than small cobbles)  Estimated bed material $D_{50} = $ ft Average approach velocity, $V_1 = Q_{100}/(y_1W_1) = $ ft/s						
	Critical approach velocity, $Vc = 11.52y_1^{1/6}D_{50}^{1/3} =ft/s$						
Z.	If $V_1 < V_c$ and $D_{50} >= 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above.						
GR							
	$\begin{aligned} &D_{c50} = 0.0006(q_2/y_1^{7/6})^3 = \underline{\qquad \qquad \qquad } ft & If  D_{50} >= D_{c50},  \chi = 0.0 \\ &Otherwise,  \chi = 0.122y_1[q_2/(D_{50}^{1/3}y_1^{7/6})]^{6/7} - y_1 = \underline{\qquad \qquad } ft \end{aligned}$						
Pier	PIER SCOUR CALCULATIONS						
PGRM: Pier	Froude # at bridge = $0.34$ Correction factor for flow angle of attack (from Table 1), K2 = $1.6$ Using pier width a on Figure 11, $\xi = 6.6$ Pier scour $y_{ps} = 7.4$ ft						
PG	Froude # at bridge = $0.370$ Using pier width a on Figure 11, $\xi = 9.6$ Pier scour $y_{ps} = 7.7$ ft						
	ABUTMENT SCOUR CALCULATIONS						
PGRM: Abutment	Average flow depth blocked by: left abutment, $y_{aLT} = 0$ ft right abutment, $y_{aRT} = 0$ ft Shape coefficient $K_1 = 1.00$ for vertical-wall, 0.82 for vertical-wall with wingwalls, Using values for $y_{aLT}$ and $y_{aRT}$ on figure 12, $\psi_{LT} = 0$ ft Right abutment scour, $y_{as} = \psi_{LT}(K_1/0.55) = 0$ ft						
: Abı	Shape coefficient K <sub>1</sub> = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through						
JRM.	Using values for $y_{aLT}$ and $y_{aRT}$ on figure 12, $\psi_{LT} = 600$ and $\psi_{RT} = 0.00$						
PC	Left abutment scour, $y_{as} = \psi_{LT}(K_1/0.55) = $ ft Right abutment scour $y_{as} = \psi_{RT}(K_1/0.55) = $ ft						

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6.1

Route 349 Ave Stream Ponca Cree	10	MRM	Da	ate 7/11/	// Ini	itials Ch			
Deidae Structure No. 2711 5307 Los	ation Asse	SW HI S	Sial Ho	cold	3 11	G Aug	- 1		
Bridge Structure No. 2716 5307 Loc GPS coordinates: N 43°03' 28.9" Loc W 099° 12' 28.2"	taken from:	USL abutmen	t_X_	centerline o	f î MRM	end	_		
W099°12'28.2"	Datum of co	ordinates: W	GS84_X	NAD27_					
	16.8			56					
The average bottom of the main channel was		v top of guardi	ail at a poir	nt 47	ft from le	eft abutment.			
Method used to determine flood flows:Freq.	Anal i	drainage area	adjustment	region					
Method used to determine flood flowsfreq.	Allai.	dramage area	adjustificit	icgion	ai regressi	ion equations.			
	CELLANE	OUS CONSI	DERATIO						
Flows	$Q_{100} = 5860$			$Q_{500} = 9800$					
Estimated flow passing through bridge	5860			9475					
Estimated road overflow & overtopping	_				325	5			
Consideration	Yes	No	Possibly	Yes	No	Possibly			
Chance of overtopping		X				X			
Chance of Pressure flow		$\sim$				X			
Armored appearance to channel		X			X				
Lateral instability of channel									
Riprap at abutments?  Yes No Marginal Car on R. Abut  Evidence of past Scour?  Yes No Don't know  Debris Potential?  Yes No Don't know  Low									
7									
Does scour countermeasure(s) appear to have been	designed?								
		lo Do	n't know	NA					
OtherY	esN	loDo	n't know	NA					
Bed Material	Classificatio	on Based on M	edian Partic	ele Size (D <sub>50</sub> )					
Material Silt/Clay Sand		Gravel		Cobbles		Boulders			
The Control of the Co				64-250 >250					
Size range, in mm <0.062 0.062-2.	00	2.00-64		04-230		-230			
Comments, Diagrams & orientation of digital photos POOT Visibility to/c vegetation > forced to estim. Overbank width									
Photos 36-LAbut		41) - AV	n RR	3		X 11 1	2 / 1		
		40 - AF	/R	<u>*</u>	,	Tused Til	constricted of 125 than entr		
1732-10 37-R. Abut 33-45 83 38-Pier confid		42-45	Free	Bride		Width	04 125		
35-45LB 39-dragon F/	5	42-45 43: Sue 44-50	Der on	LB		rather	Than entr		
	V	44- 510	2 4 00	12		with			
Summary of Results			ar ch	60			1		
		Q100		-	Q500	7	į		
Bridge flow evaluated	59	360			947	5			
Flow depth at left abutment (yaLT), in feet	- 1	5			3.1				
Flow depth at right abutment (yaRT), in feet	4	0,0		-	70	í			
Contraction scour depth (ycs), in feet	4	7 4			43		2		
Pier scour depth (yps), in feet	- 1	3			113				
Left abutment scour depth (yas), in feet Right abutment scour depth (yas), in feet	6	0.0			().()				
1Flow angle of attack		250			25°				
		N. d.			-		I)		