

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 27220326 Date 7/11/11 Initials CW Region (A B C D) B  
 Site 06453400 Location Approx. 4S St Charles on 354 Ave, Ponca Creek  
 $Q_{100} =$  6280 by: drainage area      flood frequency anal.  regional regression eq.       
 Bridge discharge ( $Q_2$ ) = 6280 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 157 ft. Flow angle at bridge = 15 ° Abut. Skew = 0 ° Effective Skew = 15 °  
 Width ( $W_2$ ) iteration = 157 121 132 131  
 Avg. flow depth at bridge,  $y_2$  iteration = 7.6 8.7 8.3 8.4  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 126.54 ft\*  $q_2 = Q_2/W_2 =$  49.6 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  5.9 ft/s Final  $y_2 = q_2/V_2 =$  8.4 ft  $\Delta h =$  0.7 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  9.1 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD,

Water Surface Elev. =      ft  
 Low Steel Elev. = 10.7 ft  
 n (Channel) = 0.040  
 n (LOB) = 0.055  
 n (ROB) = 0.055  
 Pier Width = 2.0 ft  
 Pier Length = 2.3 ft  
 # Piers for 100 yr = 2 ft



CONTRACTION SCOUR

Width of main channel at approach section  $W_1 =$  160 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  0 ft Average left overbank flow depth,  $y_{lob} =$  0 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  60 ft Average right overbank flow depth,  $y_{rob} =$  4.0 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  3.61 From Figure 9  $W_2$  (effective) = 122.5 ft  $y_{cs} =$  4.2 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$       ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$       ft/s  
 Critical approach velocity,  $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$       ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 =$       ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$       From Figure 10,  $y_{cs} =$       ft

PIER SCOUR CALCULATIONS

L/a ratio = 1.15 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1.0  
 Froude # at bridge = 0.36 Using pier width a on Figure 11,  $\xi =$  9 Pier scour  $y_{ps} =$  6.8 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} =$  0 ft right abutment,  $y_{aRT} =$  4.0 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  0 and  $\psi_{RT} =$  13.3  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1/0.55) =$  0 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1/0.55) =$  13.3 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pier

PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 27220326 Date 7/11/11 Initials Ch Region (A B C D) B  
 Site 06453400 Location Approx 4 S St. Charles on 354 Ave  
 $Q_{500} =$  10500 by: drainage area \_\_\_\_\_ flood frequency anal.  regional regression eq. \_\_\_\_\_  
 Bridge discharge ( $Q_2$ ) = 10500 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

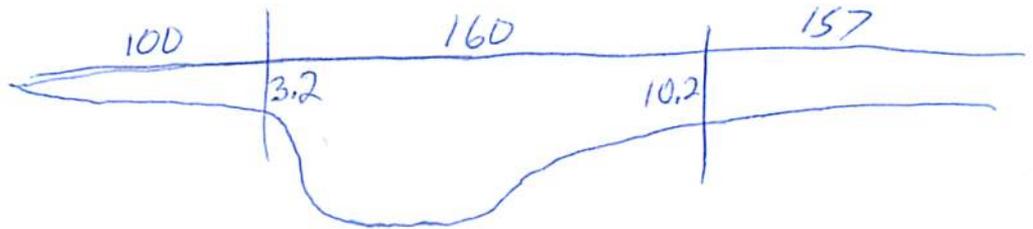
**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 157 ft. Flow angle at bridge = 15 ° Abut. Skew = 0 ° Effective Skew = 15 °  
 Width ( $W_2$ ) iteration = 157 145 150  
 Avg. flow depth at bridge,  $y_2$  iteration = 10.0 10.4 10.2  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 144.89 ft\*  $q_2 = Q_2/W_2 =$  72.5 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  7.1 ft/s Final  $y_2 = q_2/V_2 =$  10.2 ft  $\Delta h =$  1.0 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  11.2 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD,

Water Surface Elev. = \_\_\_\_\_ ft  
 Low Steel Elev. = 10.7 ft  
 n (Channel) = 0.040  
 n (LOB) = 0.055  
 n (ROB) = 0.055  
 Pier Width = 2.0 ft  
 Pier Length = 2.3 ft  
 # Piers for 500 yr = 2 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  160 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  100 ft Average left overbank flow depth,  $y_{lob} =$  1.6 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  157 ft Average right overbank flow depth,  $y_{rob} =$  6.1 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  5.04 From Figure 9  $W_2$  (effective) = 140.9 ft  $y_{cs} =$  5.7 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1)^{7/6} =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1.15 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1.0  
 Froude # at bridge = 0.39 Using pier width a on Figure 11,  $\xi =$  8 Pier scour  $y_{ps} =$  6.9 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  1.6 ft right abutment,  $y_{aRT} =$  6.1 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  6.6 and  $\psi_{RT} =$  17.0  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1/0.55) =$  6.6 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1/0.55) =$  17.0 ft

10.2  
6.1

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Pie

PRGM: Abutment

Route 354 Ave Stream Ponca Creek MRM \_\_\_\_\_ Date 7/11/11 Initials Car  
 Bridge Structure No. 2722 0326 Location approx 4 S St. Charles on 354 Ave  
 GPS coordinates: N 43° 01' 46.5" taken from: USL abutment  centerline of ↑ MRM end \_\_\_\_\_  
W 099° 05' 59.7" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 372.34 sq. mi.  
 The average bottom of the main channel was 15.8 ft below top of guardrail at a point 75 ft from left abutment.  
 Method used to determine flood flows:  Freq. Anal. \_\_\_\_\_ drainage area adjustment \_\_\_\_\_ regional regression equations.

**MISCELLANEOUS CONSIDERATIONS**

Flows	Q <sub>100</sub> = <u>6280</u>			Q <sub>500</sub> = <u>10500</u>		
Estimated flow passing through bridge	<u>6280</u>			<u>10500</u>		
Estimated road overflow & overtopping						
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Chance of Pressure flow		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel			<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>

Riprap at abutments?  Yes  No \_\_\_\_\_ Marginal  
 Evidence of past Scour?  Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know  
 Debris Potential?  High \_\_\_\_\_ Med \_\_\_\_\_ Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know  NA  
 Spur Dike \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know  NA  
 Other \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know  NA

**Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)**

Material	Silt/Clay <input checked="" type="checkbox"/>	Sand _____	Gravel _____	Cobbles _____	Boulders _____
Size range, in mm	<0.062	0.062-2.00	2.00-64	64-250	>250

Comments, Diagrams & orientation of digital photos  
1745-1D 51-LB US  
46-US  
47-US RB  
46-US LB  
49-US Face Bridge  
50-US RB

**Summary of Results**

	Q100	Q500
Bridge flow evaluated	<u>6280</u>	<u>10500</u>
Flow depth at left abutment (yaLT), in feet	<u>0.0</u>	<u>1.6</u>
Flow depth at right abutment (yaRT), in feet	<u>4.0</u>	<u>6.1</u>
Contraction scour depth (yca), in feet	<u>4.2</u>	<u>5.7</u>
Pier scour depth (ypp), in feet	<u>6.9</u>	<u>6.9</u>
Left abutment scour depth (yaa), in feet	<u>0.0</u>	<u>6.6</u>
Right abutment scour depth (yars), in feet	<u>13.3</u>	<u>17.0</u>
Flow angle of attack	<u>15</u>	<u>15</u>

See Comments/Diagram for justification where required