

OK RT

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 29230115 Date 7/31/12 Initials Nat Region (A B C D) C
Site Location 3.6 mi W & 0.5 mi N of Dempster on 459 Ave
Q100 = 73750 by: drainage area ratio flood freq. anal. regional regression eq. x
Bridge discharge (Q2) = 3750 (should be Q100 unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 108 ft. Flow angle at bridge = 40 degrees Abut. Skew = 0 degrees Effective Skew = 40 degrees
Width (W2) iteration = 108
Avg. flow depth at bridge, y2 iteration = 9.5
Corrected channel width at bridge Section = W2 times cos of flow angle = 62.73 ft\* q2 = Q2/W2 = 45.3 ft^2/s
Bridge Vel, V2 = 4.9 ft/s Final y2 = q2/V2 = 9.5 ft Delta h = 0.5 ft
Average main channel depth at approach section, y1 = Delta h + y2 = 11.0 ft

\* NOTE: repeat above calculations until y2 changes by less than 0.2 Effective pier width = L sin(q) + a cos(q)
If y2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 06-4.0 ft
Low Steel Elev. = 9.5 ft
n (Channel) = 0.033
n (LOB) = 0.035
n (ROB) = 0.035
Pier Width = 1.85 ft
Pier Length = 1.85 ft
# Piers for 100 yr = 2



CONTRACTION SCOUR

Width of main channel at approach section W1 = 132 ft
Width of left overbank flow at approach, Wlob = 0 ft Average left overbank flow depth, ylob = 0 ft
Width of right overbank flow at approach, Wrob = 0 ft Average right overbank flow depth, yrob = 0 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

x = 6.7 From Figure 9 W2 (effective) = 79 ft ycs = 7.5 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material D50 = ft Average approach velocity, V1 = Q100/(y1 W1) = ft/s

Critical approach velocity, Vc = 11.17 y1^1/6 D50^1/3 = ft/s

If V1 < Vc and D50 >= 0.2 ft, use clear water equation below, otherwise use live bed scour equation above.

Dc50 = 0.0006 (q2/y1^7/6)^3 = ft If D50 >= Dc50, chi = 0.0

Otherwise, chi = 0.122 y1 [q2 / (D50^1/3 y1^7/6)]^6/7 - y1 = From Figure 10, ycs = ft

PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1), K2 = 1
Froude # at bridge = 0.27 Using pier width a on Figure 11, xi = 7.5 Pier scour yps = 6.2 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, yalT = 3.1 ft right abutment, yarT = 4.6 ft
Shape coefficient K1 = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
Using values for yalT and yarT on figure 12, psiLT = 11.7 and psiRT = 14.3
Left abutment scour, yas = psiLT (K1/0.55) = 21.3 ft Right abutment scour yas = psiRT (K1/0.55) = 26 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pier

PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 29230115 Date 7/31/12 Initials Lat Region (A B C D) D  
 Site \_\_\_\_\_ Location 3.6 mi W + 0.5 mi N of Dempster on 459 Ave  
 $Q_{500} =$  1500 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 1500 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 108 ft. Flow angle at bridge = 40 ° Abut. Skew = 0 ° Effective Skew = 40 °  
 Width ( $W_2$ ) iteration = 108

Avg. flow depth at bridge,  $y_2$  iteration = 6  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 62.73 ft\*  $q_2 = Q_2/W_2 =$  16.1 ft<sup>2</sup>/s

Bridge Vel,  $V_2 =$  3 ft/s Final  $y_2 = q_2/V_2 =$  6 ft  $\Delta h =$  0.2 ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  6.2 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 2.6  
0-4.0 ft  
 Low Steel Elev. = 9.5 ft  
 $n$  (Channel) = 0.033  
 $n$  (LOB) = 0.039  
 $n$  (ROB) = 0.035  
 Pier Width = 1.85 ft  
 Pier Length = 1.85 ft  
 # Piers for 500 yr = 2 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  108 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  0 ft Average left overbank flow depth,  $y_{lob} =$  0 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  0 ft Average right overbank flow depth,  $y_{rob} =$  0 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  2.27 From Figure 9  $W_2$  (effective) = 79 ft  $y_{cs} =$  2.9 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} >= 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006(q_2/y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} >= D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

$L/a$  ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.22 Using pier width  $a$  on Figure 11,  $\xi =$  2.5 Pier scour  $y_{ps} =$  6 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  0 ft right abutment,  $y_{aRT} =$  0.8 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure-12,  $\psi_{LT} =$  0 and  $\psi_{RT} =$  3.5  
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  0 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  6.3 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Pie

PRGM: Abutment

$y_2$   $y_{ps}$   
 $10 - 4.1 = 5.9$   $6.2 y_2$   
 $- 5.4$



Route 459 Ave Stream Boswell Diversion Ditch MRM \_\_\_\_\_ Date 7/3/12 Initials Rat  
 Bridge Structure No. 29230115 Location 3.6 mi W & 0.5 mi N of Dempster on 459 Ave  
 GPS coordinates: N 40° 13' 13.0" taken from: USL abutment  centerline of  MRM end \_\_\_\_\_  
W 97° 1' 37.4" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 7.09 sq. mi.  
 The average bottom of the main channel was 13.5 ft below top of guardrail at a point 58 ft from left abutment.  
 Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio  regional regression equations.

**MISCELLANEOUS CONSIDERATIONS**

Flows	Q <sub>100</sub> = Q <sub>max</sub> <u>3750</u>			Q <sub>500</sub> = <u>1500</u>				
Estimated flow passing through bridge	<u>3750</u>			<u>1500</u>				
Estimated road overflow & overtopping	<u>0</u>			<u>0</u>				
Consideration	Yes	No	Possibly	Yes	No	Possibly		
Chance of overtopping		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>			
Chance of Pressure flow	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>			
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>			
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>			

7/3  
 8/23  
 2 79.3  
 5 219  
 10 353  
 25 567  
 50 754  
 100 960  
 500 1500

Riprap at abutments? \_\_\_ Yes \_\_\_ No  Marginal - on outside, right abutment and left abutment  
 Evidence of past Scour?  Yes \_\_\_ No \_\_\_ Don't know under bridge only  
 Debris Potential? \_\_\_ High \_\_\_ Med  Low lots of pier/abutment/contractor.

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Spur Dike \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Other \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA

**Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)**

Material Silt/Clay  Sand \_\_\_ Gravel \_\_\_ Cobbles \_\_\_ Boulders \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

**Comments, Diagrams & orientation of digital photos**

- 1). left ab
- 2). main channel
- 3). right ab
- 4). pier
- 5). right abutment
- 6). left abutment
- 7). right abutment

Note: Assume flow east-west. There appears to be a decommissioned dam east of bridge on 460 Ave 189 ft, this may drastically reduce the flood flow levels.  
 Note: High water levels much > than flow levels. Calc. @ low steel

**Summary of Results**

	Q <sub>100</sub> - Q <sub>max</sub>	Q <sub>500</sub>
Bridge flow evaluated	<u>3750</u>	<u>1500</u>
Flow depth at left abutment (yaLT), in feet	<u>0</u>	<u>0</u>
Flow depth at right abutment (yaRT), in feet	<u>0</u>	<u>0</u>
Contraction scour depth (y <sub>cs</sub> ), in feet	<u>7.5</u>	<u>2.8</u>
Pier scour depth (y <sub>ps</sub> ), in feet	<u>6.2</u>	<u>6</u>
Left abutment scour depth (y <sub>as</sub> ), in feet	<u>21.3</u>	<u>0</u>
Right abutment scour depth (y <sub>as</sub> ), in feet	<u>26.0</u>	<u>6.3</u>
Flow angle of attack	<u>40</u>	<u>40</u>

See Comments/Diagram for justification where required