

Dup Ok-Rat

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 29256060 Date 10-11-12 Initials RFT Region (A B C D) (C)  
 Site \_\_\_\_\_ Location 2.5 mi E Castlewood on 184th St  
 $Q_{100} =$  10400 by: drainage area ratio  flood freq. anal. \_\_\_\_\_ regional regression eq. \_\_\_\_\_  
 Bridge discharge ( $Q_2$ ) = 10400 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

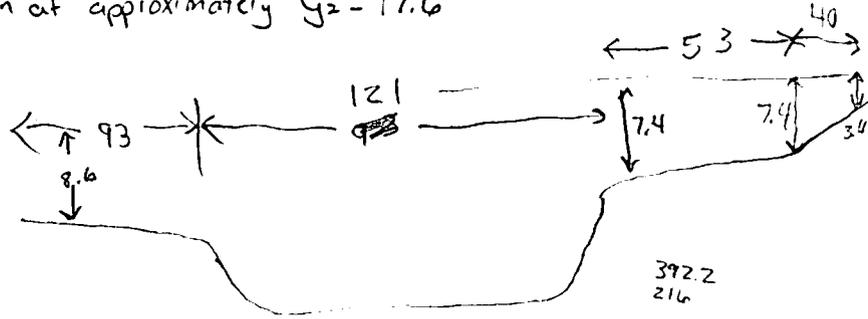
**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 93 ft. Flow angle at bridge = 24 ° Abut. Skew = 0 ° Effective Skew = 24 °  
 Width ( $W_2$ ) iteration = 93  
 Avg. flow depth at bridge,  $y_2$  iteration = 15.6  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 84.96 ft\*  $q_2 = Q_2/W_2 =$  122.4 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  7.8 ft/s Final  $y_2 = q_2/V_2 =$  15.6 ft  $\Delta h =$  1.3 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  16.9 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.  
 road overflow will begin at approximately  $y_2 = 17.6$

Water Surface Elev. = 3.9 ft  
 Low Steel Elev. = 11.8 ft  
 $n$  (Channel) = .035  
 $n$  (LOB) = .035  
 $n$  (ROB) = .035  
 Pier Width = NA ft  
 Pier Length = NA ft  
 # Piers for 100 yr = 0 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  121 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  93 ft Average left overbank flow depth,  $y_{lob} =$  6.5 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  93 ft Average right overbank flow depth,  $y_{rob} =$  8.6 ft

**Live Bed Contraction Scour** (use if bed material is small cobbles or finer)

$x =$  16.93 From Figure 9  $W_2$  (effective) = 85 ft  $y_{cs} =$  16.0 ft

**Clear Water Contraction Scour** (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} >= 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} >= D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = \_\_\_\_\_ Correction factor for flow angle of attack (from Table 1),  $K_2 =$  \_\_\_\_\_  
 Froude # at bridge = \_\_\_\_\_ Using pier width  $a$  on Figure 11,  $\xi =$  \_\_\_\_\_ Pier scour  $y_{ps} =$  \_\_\_\_\_ ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  6.5 ft right abutment,  $y_{aRT} =$  8.6 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  17.7 and  $\psi_{RT} =$  20.2  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) =$  17.7 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) =$  20.2 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pier

PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 29256060 Date \_\_\_\_\_ Initials \_\_\_\_\_ Region (A B C D)  
 Site \_\_\_\_\_ Location \_\_\_\_\_

$Q_{500} = 18400$  by: drainage area ratio  flood freq. anal. \_\_\_\_\_ regional regression eq. \_\_\_\_\_  
 Bridge discharge ( $Q_2$ ) = 13240 (should be  $Q_{300}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 93 ft. Flow angle at bridge = 2.11 ° Abut. Skew = 0 ° Effective Skew = 24 °  
 Width ( $W_2$ ) iteration = 93

Avg. flow depth at bridge,  $y_2$  iteration = 17.6

Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 84.96 ft\*  $q_2 = Q_2/W_2 = 155.8$  ft<sup>2</sup>/s

Bridge Vel,  $V_2 = 8.9$  ft/s Final  $y_2 = q_2/V_2 = 17.6$  ft  $\Delta h = 1.6$  ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = 19.2$  ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.  
*road overflow will occur at  $y_2 = 17.6$  assume this is also  $Q_{max}$  scour*

Water Surface Elev. = 3.9 ft  
 Low Steel Elev. = 11.8 ft  
 n (Channel) = .035  
 n (LOB) = .035  
 n (ROB) = .035  
 Pier Width = NA ft  
 Pier Length = NA ft  
 # Piers for 500 yr = 0



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 = 121$  ft

Width of left overbank flow at approach,  $W_{lob} = 93$  ft

Average left overbank flow depth,  $y_{lob} = 8.8$  ft

Width of right overbank flow at approach,  $W_{rob} = 93$  ft

Average right overbank flow depth,  $y_{rob} = 10.9$  ft

**Live Bed Contraction Scour** (use if bed material is small cobbles or finer)

$x = 22.05$  From Figure 9  $W_2$  (effective) = 85 ft  $y_{cs} = 18.8$  ft

**Clear Water Contraction Scour** (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006(q_2/y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = \_\_\_\_\_ Correction factor for flow angle of attack (from Table 1),  $K_2 =$  \_\_\_\_\_  
 Froude # at bridge = \_\_\_\_\_ Using pier width  $a$  on Figure 11,  $\xi =$  \_\_\_\_\_ Pier scour  $y_{ps} =$  \_\_\_\_\_ ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} = 8.8$  ft right abutment,  $y_{aRT} = 10.9$  ft

Shape coefficient  $K_1 = 1.00$  for vertical-wall,  $0.82$  for vertical-wall with wingwalls, 0.55 for spill-through

Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = 20.4$  and  $\psi_{RT} = 22.1$

Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) = 20.4$  ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) = 22.1$  ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCSNEW

PRGM: Pie

PRGM: Abutment

Route 184 St Stream Stray Horse Ck MRM \_\_\_\_\_ Date \_\_\_\_\_ Initials \_\_\_\_\_

Bridge Structure No. 29256060 Location \_\_\_\_\_

GPS coordinates: N 44° 43.055' taken from: USL abutment  centerline of  $\uparrow$  MRM end \_\_\_\_\_  
W 96° 58.390' Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 79.69 sq. mi.

The average bottom of the main channel was 19.8 ft below top of guardrail at a point 29 ft from left abutment.

Method used to determine flood flows: \_\_\_\_\_ Freq. Anal.  drainage area ratio \_\_\_\_\_ regional regression equations.

**MISCELLANEOUS CONSIDERATIONS**

Flows	Q <sub>100</sub> = <u>10400</u>			Q <sub>500</sub> = <u>18400</u>		
Estimated flow passing through bridge	<u>10400</u>			<u>13240</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>5160</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Chance of Pressure flow	<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

Riprap at abutments?  Yes \_\_\_\_\_ No \_\_\_\_\_ Marginal \_\_\_\_\_  
 Evidence of past Scour?  Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know scour pool under/at bridge  
 Debris Potential? \_\_\_\_\_ High \_\_\_\_\_ Med  Low

Does scour countermeasure(s) appear to have been designed?

Riprap \_\_\_\_\_ Yes \_\_\_\_\_ No  Don't know \_\_\_\_\_ NA some quartzite and some field stone. Fabric is also present, although not covered with rock  
 Spur Dike \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know  NA  
 Other \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know  NA

**Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)**

Material Silt/Clay  Sand \_\_\_\_\_ Gravel \_\_\_\_\_ Cobbles \_\_\_\_\_ Boulders \_\_\_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

Str. NO. bridge from approach  
 approach from bridge left abut.  
 LOB from bridge rt. abut.  
 ROB from bridge erosion fabric on left abut.

**Summary of Results**

	Q <sub>100</sub>	Q <sub>500</sub> max scour
Bridge flow evaluated	<u>10400</u>	<u>13240</u>
Flow depth at left abutment (yaLT), in feet	<u>6.5</u>	<u>8.8</u>
Flow depth at right abutment (yaRT), in feet	<u>8.6</u>	<u>10.9</u>
Contraction scour depth (yca), in feet	<u>16.0</u>	<u>18.8</u>
Pier scour depth (yps), in feet	<u>NA</u>	<u>NA</u>
Left abutment scour depth (yas), in feet	<u>17.7</u>	<u>20.4</u>
Right abutment scour depth (yas), in feet	<u>20.2</u>	<u>22.1</u>
If flow angle of attack	<u>24°</u>	<u>24°</u>

See Comments/Diagram for justification where required