

OK RT check

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 30250208 Date 7/9/12 Initials RAI Region (A B C D)  
 Site \_\_\_\_\_ Location 7.1 mi N of Vayland on 369 Ave  
 $Q_{100} =$  5250 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 5250 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 84 ft. Flow angle at bridge = 30 ° Abut. Skew = 0 ° Effective Skew = 30 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_

Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 72.75 ft\*  $q_2 = Q_2/W_2 =$  72.2 ft<sup>2</sup>/s

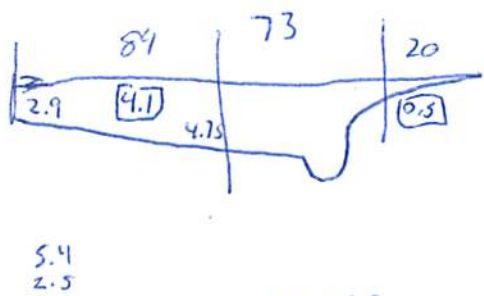
Bridge Vel,  $V_2 =$  6 ft/s Final  $y_2 = q_2/V_2 =$  12 ft  $\Delta h =$  0.7 ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  12.7 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(\theta) + a \cos(\theta)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

Water Surface Elev. = 304.1 ft  
 Low Steel Elev. = 14.2 ft 2.05  
1.75  
 $n$  (Channel) = 0.045  
 $n$  (LOB) = 0.035  
 $n$  (ROB) = 0.030  
 Pier Width = 1.75 ft  
 Pier Length = 1.75 ft  
 # Piers for 100 yr = 2 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  84 ft 4.75 → 2.9  
84 → 5.4  
7.25  
 Width of left overbank flow at approach,  $W_{lob} =$  84 ft Average left overbank flow depth,  $y_{lob} =$  4.1 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  20 ft Average right overbank flow depth,  $y_{rob} =$  0.5 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  3.72 From Figure 9  $W_2$  (effective) = 69.3 ft  $y_{cs} =$  4.3 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} >= 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} >= D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

PRGM: Contract

PRGM: CWCNEW

**PIER SCOUR CALCULATIONS**

$L/a$  ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.31 Using pier width  $a$  on Figure 11,  $\xi =$  7.2 Pier scour  $y_{ps} =$  6 ft

PRGM: Pier

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  4.1 ft right abutment,  $y_{aRT} =$  0.5 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  13.4 and  $\psi_{RT} =$  2.3  
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  13.4 ft Right abutment scour  $y_{bs} = \psi_{RT}(K_1/0.55) =$  2.3 ft

PRGM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 30250208 Date 7/9/12 Initials RaT Region (A B C D) C  
 Site \_\_\_\_\_ Location 7.1 mi. N of Vayland on 369 Ave  
 $Q_{500} =$  10600 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 7375 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

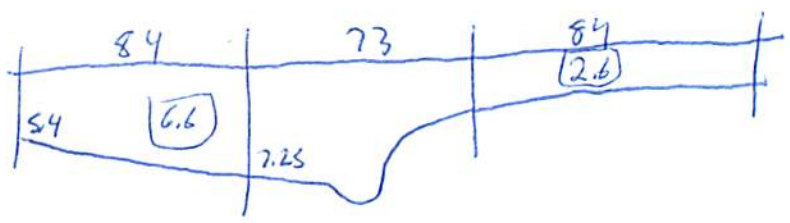
Bridge Width = 84 ft. Flow angle at bridge = 30 ° Abut. Skew = 0 ° Effective Skew = 30 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_

Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 72.75 ft\*  $q_2 = Q_2/W_2 =$  101.4 ft<sup>2</sup>/s

Bridge Vel,  $V_2 =$  7.1 ft/s Final  $y_2 = q_2/V_2 =$  14.2 ft  $\Delta h =$  1 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  15.2 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 3.0  
~~34~~ - 4.1 ft  
 Low Steel Elev. = 14.2 ft  
 $n$  (Channel) = 0.045  
 $n$  (LOB) = 0.035  
 $n$  (ROB) = 0.030  
 Pier Width = 1.75 ft  
 Pier Length = 1.75 ft  
 # Piers for 500 yr = 2 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  73 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  784 ft Average left overbank flow depth,  $y_{lob} =$  6.6 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  84 ft Average right overbank flow depth,  $y_{rob} =$  2.5 2.6 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  8.18 From Figure 9  $W_2$  (effective) = 69.3 ft  $y_{cs} =$  9 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.33 Using pier width  $a$  on Figure 11,  $\xi =$  7.2 Pier scour  $y_{ps} =$  6.1 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  6.6 ft right abutment,  $y_{aRT} =$  2.6 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  17.9 and  $\psi_{RT} =$  10.6  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1/0.55) =$  17.9 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1/0.55) =$  10.6 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Pie

PRGM: Abutment



98.8075  
44.59527

98° 48' 27"  
44° 35' 42.972"

Route 369 Ave Stream Turtle Ck MRM \_\_\_\_\_ Date 7/9/12 Initials RLT

Bridge Structure No. 30250208 Location 7.1 mi. N of Vayland on 369 Ave

GPS coordinates: N 440 351 399.9" taken from: USL abutment  centerline of  $\uparrow$  MRM end \_\_\_\_\_  
W 990 481 26.511 Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 137.95 sq. mi.

The average bottom of the main channel was 18.0 ft below top of guardrail at a point 43 ft from left abutment.

Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio  regional regression equations.

6/20  
8/24

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = <u>5250</u>			Q <sub>500</sub> = <u>10800</u>		
Estimated flow passing through bridge	<u>5250</u>			<u>7375</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>3425</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Chance of Pressure flow		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

2	125
5	545
10	1120
25	2310
50	3590
100	5250
500	10800

Riprap at abutments?  Yes \_\_\_ No \_\_\_ Marginal  
 Evidence of past Scour?  Yes \_\_\_ No \_\_\_ Don't know  
 Debris Potential? \_\_\_ High \_\_\_ Med  Low  
*Mostly on left, vast majority on left.  
 noticeable pier & contraction. Very heavy scour on left abutment. Hard to tell through pictures but riprap/concrete has been placed in the spot.*

Does scour countermeasure(s) appear to have been designed?  
 Riprap  Yes \_\_\_ No \_\_\_ Don't know \_\_\_ NA  
 Spur Dike \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Other \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
*rose quartz on left abutment. also appears to have additional concrete where previous scour occurred*

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material	Silt/Clay <input checked="" type="checkbox"/>	Sand ___	Gravel ___	Cobbles ___	Boulders ___
Size range, in mm	<0.062	0.062-2.00	2.00-64	64-250	>250

Comments, Diagrams & orientation of digital photos

- 1). left OB
- 2). main channel
- 3). right OB
- 4). left abutment
- 5). pier
- 6). pier
- 7). right abutment
- 8). left abutment
- 9). left abutment scou-
- 10). main channel

Summary of Results

	Q100	Q500
Bridge flow evaluated	<u>5250</u>	<u>7375</u>
Flow depth at left abutment (yaLT), in feet	<u>4.1</u>	<u>6.6</u>
Flow depth at right abutment (yaRT), in feet	<u>0.5</u>	<u>2.6</u>
Contraction scour depth (yca), in feet	<u>4.3</u>	<u>9</u>
Pier scour depth (yca), in feet	<u>6</u>	<u>6.1</u>
Left abutment scour depth (yca), in feet	<u>13.4</u>	<u>17.9</u>
Right abutment scour depth (yca), in feet	<u>2.3</u>	<u>10.6</u>
Flow angle of attack	<u>30</u>	<u>30</u>

See Comments/Diagram for justification where required