

OK RT

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 31001085 Date 6/5/12 Initials Rat Region (A B C D) D
 Site 25250 Old Mill Road, James River
 $Q_{100} = \frac{28700}{4130}$ by: drainage area ratio flood freq. anal. regional regression eq.
 Bridge discharge (Q_2) = 41300 (should be Q_{100} unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 333 ft. Flow angle at bridge = 40 ° Abut. Skew = 0 ° Effective Skew = 40 °
 Width (W_2) iteration = _____

Avg. flow depth at bridge, y_2 iteration = _____

Corrected channel width at bridge Section = W_2 times cos of flow angle = 255.09 ft* $q_2 = Q_2/W_2 = \frac{41300}{333} = 123.7$ ft²/s

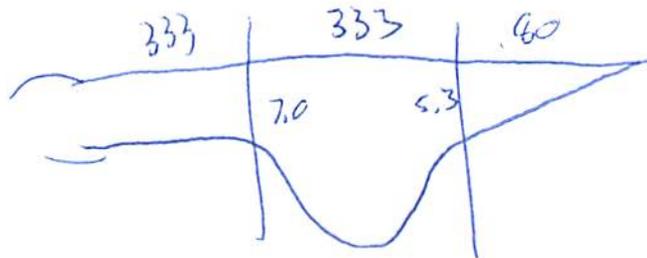
Bridge Vel, $V_2 = 9$ ft/s Final $y_2 = q_2/V_2 = 13.7$ ft $\Delta h = 1.7$ ft

Average main channel depth at approach section, $y_1 = \Delta h + y_2 = 19.7$ ft

* NOTE: repeat above calculations until y_2 changes by less than 0.2 Effective pier width = $L \sin(q) + a \cos(q)$

If y_2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 5.6 ft
 Low Steel Elev. = 16.1 ft 25.5
 n (Channel) = 0.033 $= 7.4$
 n (LOB) = 0.040 18.1
 n (ROB) = 0.050
 Pier Width = 2.5 ft $5/8$
 Pier Length = 2.5 ft
 # Piers for 100 yr = 3 ft



CONTRACTION SCOUR

Width of main channel at approach section $W_1 = 333$ ft

Width of left overbank flow at approach, $W_{lob} = 333$ ft

Average left overbank flow depth, $y_{lob} = 7.0$ ft

Width of right overbank flow at approach, $W_{rob} = 60$ ft

Average right overbank flow depth, $y_{rob} = 5.3$ ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x = 11.16$ From Figure 9 W_2 (effective) = 247.6 ft $y_{cs} = 12.2$ ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material $D_{50} =$ _____ ft Average approach velocity, $V_1 = Q_{100}/(y_1 W_1) =$ _____ ft/s

Critical approach velocity, $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$ _____ ft/s

If $V_1 < V_c$ and $D_{50} \geq 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$ _____ ft If $D_{50} \geq D_{c50}$, $\chi = 0.0$

Otherwise, $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$ _____ From Figure 10, $y_{cs} =$ _____ ft

PIER SCOUR CALCULATIONS

L/a ratio = 1

Correction factor for flow angle of attack (from Table 1), $K_2 = 1$

Froude # at bridge = 0.37

Using pier width a on Figure 11, $\xi = 9.5$ Pier scour $y_{ps} = 9.2$ ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, $y_{aLT} = 7$ ft right abutment, $y_{aRT} = 5.3$ ft

Shape coefficient $K_1 = 1.00$ for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through

Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} = 18.6$ and $\psi_{RT} = 15.6$

Left abutment scour, $y_{as} = \psi_{LT} (K_1 / 0.55) = 18.6$ ft Right abutment scour $y_{as} = \psi_{RT} (K_1 / 0.55) = 15.6$ ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCSNEW

PRGM: Pier

PRGM: Abutment

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 31001085 Date 4/5/12 Initials RAT Region (A B C D) C

Site 25250 Old Mill Road Location 25250 Old Mill Road

$Q_{500} = \frac{56000 \times 109.00}{1000}$ by: drainage area ratio W flood freq. anal. regional regression eq. X

Bridge discharge (Q_2) = 47049 (should be Q_{500} unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 333 ft. Flow angle at bridge = 40 ° Abut. Skew = 0 ° Effective Skew = 40 °

Width (W_2) iteration =

Avg. flow depth at bridge, y_2 iteration =

Corrected channel width at bridge Section = W_2 times cos of flow angle = 255.09 ft* $q_2 = Q_2/W_2 = \frac{47049}{333} = \underline{164.8}$ ft²/s

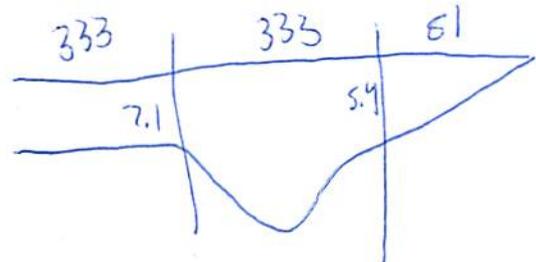
Bridge Vel, $V_2 = \frac{9.1}{1.483} = \underline{6.1}$ ft/s Final $y_2 = q_2/V_2 = \frac{164.8}{6.1} = \underline{18.1}$ ft $\Delta h = \underline{1.7}$ ft

Average main channel depth at approach section, $y_1 = \Delta h + y_2 = \underline{19.8}$ ft

* NOTE: repeat above calculations until y_2 changes by less than 0.2 Effective pier width = $L \sin(q) + a \cos(q)$

If y_2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 56 ft
 Low Steel Elev. = 16.1 ft
 n (Channel) = 0.033
 n (LOB) = 0.040
 n (ROB) = 0.050
 Pier Width = 2.5 ft
 Pier Length = 2.5 ft
 # Piers for 500 yr = 3



CONTRACTION SCOUR

Width of main channel at approach section $W_1 = \underline{333}$ ft

Width of left overbank flow at approach, $W_{lob} = \underline{333}$ ft Average left overbank flow depth, $y_{lob} = \underline{7.1}$ ft

Width of right overbank flow at approach, $W_{rob} = \underline{81}$ ft Average right overbank flow depth, $y_{rob} = \underline{5.4}$ ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x = \underline{16.3}$ From Figure 9 W_2 (effective) = 247.6 ft $y_{cs} = \underline{12.3}$ ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material $D_{50} = \underline{\quad}$ ft Average approach velocity, $V_1 = Q_{500}/(y_1 W_1) = \underline{\quad}$ ft/s

Critical approach velocity, $V_c = 1.52 y_1^{1/6} D_{50}^{1/3} = \underline{\quad}$ ft/s

If $V_1 < V_c$ and $D_{50} \geq 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1)^{7/6} = \underline{\quad}$ ft If $D_{50} \geq D_{c50}$, $\chi = 0.0$

Otherwise, $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 = \underline{\quad}$ From Figure 10, $y_{cs} = \underline{\quad}$ ft

PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1), $K_2 = \underline{1}$

Froude # at bridge = 0.38 Using pier width a on Figure 11, $\xi = \underline{9.5}$ Pier scour $y_{ps} = \underline{8.2}$ ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, $y_{aLT} = \underline{7.1}$ ft right abutment, $y_{aRT} = \underline{5.4}$ ft

Shape coefficient $K_1 = 1.00$ for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through

Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} = \underline{19.8}$ and $\psi_{RT} = \underline{15.7}$

Left abutment scour, $y_{as} = \psi_{LT}(K_1/0.55) = \underline{19.8}$ ft Right abutment scour $y_{as} = \psi_{RT}(K_1/0.55) = \underline{15.7}$ ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pier

PGRM: Abutment

97.96384
43.7255

Route old Mill Rd stream James River MRM Date 6/5/12 Initials Lat
 Bridge Structure No. 31001085 Location 25250 old Mill Road
 GPS coordinates: N 43° 43' 30.71" taken from: USL abutment centerline of MRM end
W 99° 57' 50.01" Datum of coordinates: WGS84 NAD27

Drainage area = 16323.76 sq. mi. 16333.9
 The average bottom of the main channel was 25.5 ft below top of guardrail at a point 194 ft from left abutment.
 Method used to determine flood flows: Freq. Anal. drainage area ratio regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q ₁₀₀ = <u>28700</u> Q₂₅ <u>41500</u>			Q ₅₀₀ = <u>56200</u> Q₅₀ <u>70800</u>		
Estimated flow passing through bridge	<u>41500</u>			<u>42048</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>25752</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping			<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>		
Chance of Pressure flow	<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

Q₅₀
S/30
 2 | 1350
 5 | 7370
 10 | 17300
 25 | 41500
 50 | 70800
 100 | 113000
 500 | 276000

Riprap at abutments? Yes No Marginal ^{star}
 Evidence of past Scour? Yes No Don't know ^{star}
 Debris Potential? High Med Low ^{see picture}

Does scour countermeasure(s) appear to have been designed?
 Riprap Yes No Don't know NA ^{raise granite along left abutment}
 Spur Dike Yes No Don't know NA
 Other Yes No Don't know NA

Bed Material Classification Based on Median Particle Size (D₅₀)

Material Silt/Clay Sand Gravel Cobbles Boulders
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos
 1) main channel
 2) piers
 3) right abutment
 4) left abutment
 5) right OB
 6) main channel
 7-8) left OB
 9) left abutment
 10) debris
 11) right abutment

Summary of Results

	Q ₁₀₀ Q₂₅	Q ₅₀₀ Q₅₀
Bridge flow evaluated	<u>41500</u>	<u>42048</u>
Flow depth at left abutment (yaLT), in feet	<u>7.0</u>	<u>7.1</u>
Flow depth at right abutment (yaRT), in feet	<u>5.3</u>	<u>5.4</u>
Contraction scour depth (y _{cs}), in feet	<u>12.2</u>	<u>12.3</u>
Pier scour depth (y _{ps}), in feet	<u>8.2</u>	<u>8.2</u>
Left abutment scour depth (y _{as}), in feet	<u>15.6</u>	<u>15.6</u>
Right abutment scour depth (y _{rs}), in feet	<u>15.6</u>	<u>15.7</u>
Flow angle of attack	<u>40</u>	<u>40</u>

See Comments/Diagram for justification where required