

OK RT

SCOUR ANALYSIS AND REPORTING FORM

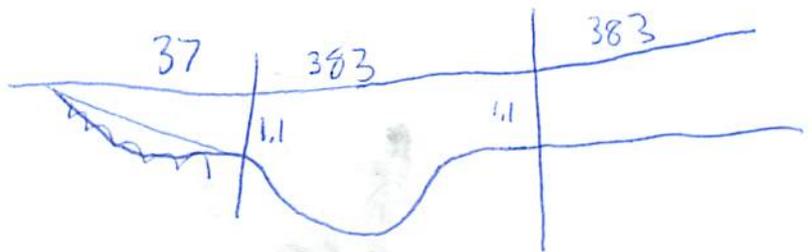
Bridge Structure No. 31040141 Date 6/5/12 Initials Dal Region (A B C D)
Site Location 25 810 416 Ave, James River
Q 25 = 29700 43300 by: drainage area ratio flood freq. anal. regional regression eq. X
Bridge discharge (Q2) = 43300 (should be Q100 unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 383 ft. Flow angle at bridge = 10 degrees Abut. Skew = 0 degrees Effective Skew = 10 degrees
Width (W2) iteration = 377.19 326.96 353.24 347.64 350 344.08
Avg. flow depth at bridge, y2 iteration = 15.1 16.2 15.7 15.8 W2 = 344.68
Corrected channel width at bridge Section = W2 times cos of flow angle = 377.19 ft* q2 = Q2/W2 = 125.6 ft^2/s
Bridge Vel, V2 = 7.9 ft/s Final y2 = q2/V2 = 15.8 ft Delta h = 1.3 ft
Average main channel depth at approach section, y1 = Delta h + y2 = 17.1 ft

* NOTE: repeat above calculations until y2 changes by less than 0.2 Effective pier width = L sin(q) + a cos(q)
If y2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 4.5 ft
Low Steel Elev. = 19.5 ft
n (Channel) = 0.030
n (LOB) = 0.035
n (ROB) = 0.045
Pier Width = 2.4 ft
Pier Length = 2.4 ft
Piers for 100 yr = 4 ft



CONTRACTION SCOUR

Width of main channel at approach section W1 = 383 ft
Width of left overbank flow at approach, Wlob = 35 ft Average left overbank flow depth, ylob = 1.1 ft
Width of right overbank flow at approach, Wrob = 383 ft Average right overbank flow depth, yrob = 1.1 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)
x = 2.6 From Figure 9 W2 (effective) = 335.1 ft ycs = 3.2 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)
Estimated bed material D50 = 1 ft Average approach velocity, V1 = Q100/(y1 W1) = 1.7 * 34 = 58 ft/s
Critical approach velocity, Vc = 11.52 y1^(1/6) D50^(1/3) = 11.52 * 1^(1/6) * 1^(1/3) = 11.52 ft/s
If V1 < Vc and D50 >= 0.2 ft, use clear water equation below, otherwise use live bed scour equation above.
Dc50 = 0.0006 (q2/y1^(7/6))^3 = 0.0006 (125.6/1^(7/6))^3 = 0.0006 * 125.6^3 = 0.0006 * 1,980,000 = 1,188 ft
If D50 >= Dc50, chi = 0.0
Otherwise, chi = 0.122 y1 [q2 / (D50^(1/3) y1^(7/6))]^(6/7) - y1 = 0.122 * 1 * [125.6 / (1^(1/3) * 1^(7/6))]^(6/7) - 1 = 0.122 * 125.6^(6/7) - 1 = 0.122 * 100 - 1 = 12.2 - 1 = 11.2
From Figure 10, ycs = 7.9 ft

PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1), K2 = 1
Froude # at bridge = 0.35 Using pier width a on Figure 11, xi = 9.2 Pier scour yps = 7.9 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, yalT = 1.1 ft right abutment, yarT = 1.1 ft
Shape coefficient K1 = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
Using values for yalT and yarT on figure 12, psiLT = 4.7 and psiRT = 4.7
Left abutment scour, yas = psiLT (K1/0.55) = 4.7 ft Right abutment scour yas = psiRT (K1/0.55) = 4.7 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pier

PGRM: Abutment

SCOUR ANALYSIS AND REPORTING FORM

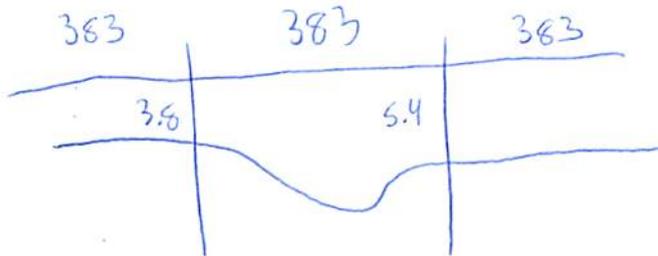
Bridge Structure No. 31040141 Date 6/5/12 Initials Rat Region (A B C D) D
 Site _____ Location 25810 416 Ave
 $Q_{500} = \underline{579007390}$ by: drainage area ratio not flood freq. anal. _____ regional regression eq. X
 Bridge discharge (Q_2) = 72176 (should be Q_{500} unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 383 ft. Flow angle at bridge = 10 ° Abut. Skew = 0 ° Effective Skew = 10 °
 Width (W_2) iteration = _____
 Avg. flow depth at bridge, y_2 iteration = _____
 Corrected channel width at bridge Section = W_2 times cos of flow angle = 377.18 ft* $q_2 = Q_2/W_2 = \underline{191.4}$ ft²/s
 Bridge Vel, $V_2 = \underline{9.8}$ ft/s Final $y_2 = q_2/V_2 = \underline{19.5}$ ft $\Delta h = \underline{2}$ ft
 Average main channel depth at approach section, $y_1 = \Delta h + y_2 = \underline{21.5}$ ft

* NOTE: repeat above calculations until y_2 changes by less than 0.2 Effective pier width = $L \sin(q) + a \cos(q)$
 If y_2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 41.5 ft
 Low Steel Elev. = 19.5 ft
 n (Channel) = 0.030
 n (LOB) = 0.035
 n (ROB) = 0.045
 Pier Width = 2.4 ft
 Pier Length = 2.4 ft
 # Piers for 500 yr = 4



CONTRACTION SCOUR

Width of main channel at approach section $W_1 = \underline{383}$ ft
 Width of left overbank flow at approach, $W_{lob} = \underline{383}$ ft Average left overbank flow depth, $y_{lob} = \underline{3.8}$ ft
 Width of right overbank flow at approach, $W_{rob} = \underline{383}$ ft Average right overbank flow depth, $y_{rob} = \underline{5.1}$ ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)
 $x = \underline{3.46}$ From Figure 9 W_2 (effective) = 367.6 ft $y_{cs} = \underline{4.1}$ ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)
 Estimated bed material $D_{50} = \underline{\quad}$ ft Average approach velocity, $V_1 = Q_{500}/(y_1 W_1) = \underline{\quad}$ ft/s
 Critical approach velocity, $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} = \underline{\quad}$ ft/s
 If $V_1 < V_c$ and $D_{50} \geq 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above.
 $D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 = \underline{\quad}$ ft If $D_{50} \geq D_{c50}$, $\chi = 0.0$
 Otherwise, $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 = \underline{\quad}$ From Figure 10, $y_{cs} = \underline{\quad}$ ft

PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1), $K_2 = \underline{1}$
 Froude # at bridge = 0.39 Using pier width a on Figure 11, $\xi = \underline{9.2}$ Pier scour $y_{ps} = \underline{8}$ ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, $y_{aLT} = \underline{3.8}$ ft right abutment, $y_{aRT} = \underline{5.4}$ ft
 Shape coefficient $K_1 = 1.00$ for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
 Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} = \underline{12.9}$ and $\psi_{RT} = \underline{15.7}$
 Left abutment scour, $y_{as} = \psi_{LT}(K_1/0.55) = \underline{12.9}$ ft Right abutment scour $y_{as} = \psi_{RT}(K_1/0.55) = \underline{15.7}$ ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pie

PGRM: Abutment

97.65664
43.64357

Route 416 Ave Stream James River MRM _____ Date 6/5/12 Initials RAT

Bridge Structure No. 3104 0141 Location 25810 416 Ave

GPS coordinates: N 43° 38' 57.9" taken from: USL abutment centerline of \uparrow MRM end _____
W 97° 53' 12.8" Datum of coordinates: WGS84 NAD27 _____

Drainage area = 17220.31 sq. mi. 17221.22

The average bottom of the main channel was 25 ft below top of guardrail at a point 158 ft from left abutment.

Method used to determine flood flows: _____ Freq. Anal. drainage area ratio regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q ₁₀₀ = 29700 <u>43300</u>			Q ₅₀ = <u>57900</u> <u>73900</u>		
Estimated flow passing through bridge	<u>43300</u>			<u>72178</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>1722</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Chance of Pressure flow		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

6/30

2	410
5	7660
10	19,000
25	43300
50	73900
100	118000
500	289000

Riprap at abutments? _____ Yes No _____ Marginal
 Evidence of past Scour? Yes _____ No _____ Don't know *piec*
 Debris Potential? _____ High _____ Med Low *contraction abutment*

Does scour countermeasure(s) appear to have been designed?

Riprap _____ Yes No _____ Don't know _____ NA
 Spur Dike _____ Yes No _____ Don't know _____ NA
 Other _____ Yes No _____ Don't know _____ NA

Bed Material Classification Based on Median Particle Size (D₅₀)

Material Silt/Clay Sand _____ Gravel _____ Cobbles _____ Boulders _____
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

*1. main channel
 2. piers
 3. left abutment
 4. right abutment
 5. left abutment
 6. right abutment*

*1. left CB
 2. right CB
 3. main channel*

Summary of Results

	Q ₁₀₀ Q ₂₅	Q ₅₀₀ Q ₅₀
Bridge flow evaluated	<u>43300</u>	<u>72178</u>
Flow depth at left abutment (yaLT), in feet	<u>1.1</u>	<u>3.8</u>
Flow depth at right abutment (yaRT), in feet	<u>1.1</u>	<u>5.4</u>
Contraction scour depth (y _{cs}), in feet	<u>3.2</u>	<u>4.1</u>
Pier scour depth (y _{ps}), in feet	<u>2.9</u>	<u>8</u>
Left abutment scour depth (y _{as}), in feet	<u>4.7</u>	<u>12.9</u>
Right abutment scour depth (y _{as}), in feet	<u>4.7</u>	<u>15.7</u>
IFlow angle of attack	<u>10</u>	<u>10</u>

See Comments/Diagram for justification where required