

Q50 =	SCOUR ANALYSIS AND REPORTING FORM  Bridge Structure No. $3226030$ Date $4600$ Date $4600$ Initials $600$ Region (ABCD)  Site Location $6.2 \text{ M}$ ; $6000$ My $6000$ My $6000$ Date $6000$				
PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"	Average main channel depth at approach section, $y_1 = \Delta h + y_2 = 9.6$ ft  *NOTE: repeat above calculations until $y_2$ changes by less than 0.2 Effective pier width = $L \sin(q) + a \cos(q)$ If $y_2$ is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD,				
30ft?	Water Surface Elev. = ft				
	Width of main channel at approach section $W_1 = 90$ ft				
ract	Width of left overbank flow at approach, $W_{lob} = \frac{40}{100}$ ft  Average left overbank flow depth, $y_{lob} = \frac{6.0}{100}$ ft				
PGRM: Contract	Width of right overbank flow at approach, $W_{rob} = 40$ ft Average right overbank flow depth, $y_{rob} = 5.7$ ft				
&M:	5.7 = 37				
PGR	Live Bed Contraction Scour (use if bed material is small cobbles or finer) $x = \frac{20.47}{\text{From Figure 9}}  \text{From Figure 9}  \text{W}_2 \text{ (effective)} = \frac{36.7}{\text{ft}}  \text{ft}  \text{y}_{cs} = \frac{17.9}{\text{ft}}  \text{ft}$				
>	Clear Water Contraction Scour (use if bed material is larger than small cobbles)				
PGRM: CWCSNEW	Estimated bed material $D_{50}$ = ft/s  Average approach velocity, $V_1 = Q_{500}/(y_1W_1) =ft/s$				
WC5	Estimated bed material $D_{50} = \underline{ ft}$ Average approach velocity, $V_1 = Q_{500}/(y_1W_1) = \underline{ ft/s}$ Critical approach velocity, $V_0 = 11.17y_1^{1/6}D_{50}^{1/3} = \underline{ ft/s}$				
A: C	If $V_1 < V_c$ and $D_{50} >= 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above.				
GR	$D_{c50} = 0.0006(q_2/v_1^{7/6})^3 = $ ft If $D_{50} >= D_{c50}$ , $\chi = 0.0$				
<u>a.</u>	$\begin{aligned} &D_{c50} = 0.0006(q_2/y_1^{7/6})^3 = \underbrace{\qquad \qquad \qquad }_{ft} & \text{If } D_{50} >= D_{c50},  \chi = 0.0 \\ &\text{Otherwise, } \chi = 0.122y_1[q_2/(D_{50}^{1/3}y_1^{7/6})]^{6/7} - y_1 = \underbrace{\qquad \qquad }_{ft} & \text{From Figure 10, } y_{cs} = \underbrace{\qquad \qquad }_{ft} & \text{ft} \end{aligned}$				
PGRM: Pic	Froude # at bridge = $0.37$ PIER SCOUR CALCULATIONS  Correction factor for flow angle of attack (from Table 1), $K2 = 1.0$ Using pier width a on Figure 11, $\xi = 4.4$ Pier scour $y_{ps} = 3.46$ ft				
	ARUTMENT SCOUR CALCULATIONS				
PGRM: Abutment	$G_{\text{out}}$ denote blooked by $G_{\text{out}}$ left obuttness $V_{\text{out}} = G_{\text{out}}$ of $G_{\text{out}}$ right abuttness $V_{\text{out}} = G_{\text{out}}$				
Abuti	Shape coefficient $K_1 = 1.00$ for vertical-wall, $0.82$ for vertical-wall with wingwalls, $0.55$ for spill-through				
M	Using values for $y_{aLT}$ and $y_{aRT}$ on figure 12, $\psi_{LT} = \frac{16.8}{16.8}$ and $\psi_{RT} = \frac{12.1}{16.8}$				
PGR	Shape coefficient $K_1$ = 1.00 for vertical-wall, Using values for $y_{aLT}$ and $y_{aRT}$ on figure 12, $\psi_{LT} = \frac{16.82}{16.82}$ for vertical-wall with wingwalls, 0.55 for spill-through Left abutment scour, $y_{as} = \psi_{LT}(K_1/0.55) = \frac{19.6}{16.82}$ ft Right abutment scour $y_{as} = \psi_{RT}(K_1/0.55) = \frac{19.6}{16.82}$ ft				
	3300				
	37 200				

Route FAS 6420 Stream Crooked C	Ck	MRM	Date 8/10	11 Initials Ch	e e		
Bridge Structure No. 32264 030 Loc	eation 6.2	- 6/ of 41	1485 m	FAS 6420			
GPS coordinates: $N'$ 45° 54′ 24.1″	taken from:	USL abutment X	centerline	of îl MRM end			
		ordinates: WGS84					
Drainage area = $32.53$ sq. mi.		STATE OF THE STATE					
The average bottom of the main channel was 14	Off below	v top of guardrail at	a point 13.0	ft from left abutment.			
Method used to determine flood flows:Freq.	Anal	drainage area ratio	regional reg	ression equations.	Flows Ca		
Wethod used to determine flood flows1req.		arming in a second		<b>2</b> 00 000 000 00 <b>1</b>	200		
MIS	SCELLANE	OUS CONSIDERA	ATIONS		"8/8		
Flows	$Q_{100} = 2720$		Q560=	Q50= 2030	-1 1/1		
Estimated flow passing through bridge	2193			2080 712 16			
Estimated road overflow & overtopping		527			5 546		
Consideration	Yes	No Pos	ssibly Yes	No Possibly	10 131		
Chance of overtopping	194		ζ	X			
Chance of Pressure flow	X				1200		
Armored appearance to channel		<u> </u>		X	0 222		
Lateral instability of channel		X		X	100 272		
	X	/ Marginal			500 4600		
Riprap at abutments? Yes	No						
Evidence of past Scour? Yes	No —	Don't know					
Debris Potential?High	MedX	Low					
D (2) and the bound have	dasianad?						
Does scour countermeasure(s) appear to have been	es X N	lo Don't kn	ow NA				
	and the same of th		1				
		loDon't kn					
OtherY	esN	loDon't kn	ow XNA				
	C1 'C' '	D 1 W 1:	D+:-1- C: (D	<b>X</b>			
		n Based on Median					
		Gravel	Cobbles_	Boulders	_		
Size range, in mm <0.062 0.062-2	.00	2.00-64	64-250	>250			
Comments, Diagrams & orientation of digital pho	tos	1	1.4 1	did individua	1 Piers		
Pier could be modeled	22 60.	ntinuous L	Jul 1	City Carried	( )		
Comments, Diagrams & orientation of digital photos  Pier could be modeled as continuous but I did individual piers.  See photos,  1447-10 51-Pier config  44-45 52-45 Fac. bridge  49-43 RB							
1447-10 51- Pier 6	iontis						
44-45 57-45 Far.	briday						
49-45 RB							
50-WSLB							
30- WLD							
Summary of Results							
	Q100			Q500 Q50			
Bridge flow evaluated	2/93			2080			
Flow depth at left abutment (yaLT), in feet	6.3			6.0			
Flow depth at right abutment (yaRT), in feet	4.0			3.7			
Contraction scour depth (ycs), in feet		18.4		3.8			
Pier scour depth (yps), in feet		3.8		25.1			
Left abutment scour depth (yas), in feet	19.8			19,0			
1Flow angle of attack		20					

See Comments/Diagram for justification where required

