

# Crooked Creek

## SCOUR ANALYSIS AND REPORTING FORM

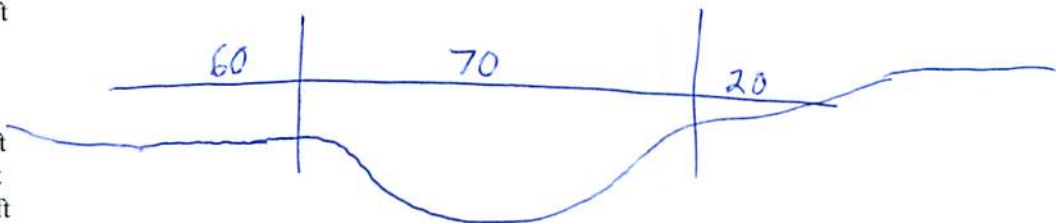
Bridge Structure No. 32305028 Date 10/29/11 Initials CW Region (A B C D) B  
 Site \_\_\_\_\_ Location 2.5 mi W of US 85 on Cox Rd  
 $Q_{100} =$  3430 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. \_\_\_\_\_  
 Bridge discharge ( $Q_2$ ) = 3430 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 60 ft. Flow angle at bridge = 2 ° Abut. Skew = 0 ° Effective Skew = 2 °  
 Width ( $W_2$ ) iteration = 60 → Vert Wall  
 Avg. flow depth at bridge,  $y_2$  iteration = 9.0  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 59.96 ft\*  $q_2 = Q_2/W_2 =$  57.2 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  6.4 ft/s Final  $y_2 = q_2/V_2 =$  9.0 ft  $\Delta h =$  0.8 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  9.8 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = \_\_\_\_\_ ft  
 Low Steel Elev. = 11.5 ft  
 $n$  (Channel) = 0.033  
 $n$  (LOB) = 0.035  
 $n$  (ROB) = 0.035  
 Pier Width = 1.0 ft  
 Pier Length = 1.0 ft  
 # Piers for 100 yr = 2 ft



### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 =$  70 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  60 ft Average left overbank flow depth,  $y_{lob} =$  3.7 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  20 ft Average right overbank flow depth,  $y_{rob} =$  0.9 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  3.98 From Figure 9  $W_2$  (effective) = 58 ft  $y_{cs} =$  4.6 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

### PIER SCOUR CALCULATIONS

L/a ratio = 1.0 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1.0  
 Froude # at bridge = 0.38 Using pier width  $a$  on Figure 11,  $\xi =$  4.9 Pier scour  $y_{ps} =$  4.2 ft

### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{alT} =$  3.7 ft right abutment,  $y_{arT} =$  0.9 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{alT}$  and  $y_{arT}$  on figure 12,  $\psi_{LT} =$  12.7 and  $\psi_{RT} =$  3.9  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) =$  19.0 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) =$  5.8 ft

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 32305028 Date 10/29/11 Initials GW Region (A B C D) B  
 Site \_\_\_\_\_ Location 2.5 mi W of US 85 on Cox Rd  
 $Q_{500} = 5780$  by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. \_\_\_\_\_  
 Bridge discharge ( $Q_2$ ) = 5456 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 60 ft. Flow angle at bridge = 2 ° Abut. Skew = 0 ° Effective Skew = 2 °  
 Width ( $W_2$ ) iteration = 60

Avg. flow depth at bridge,  $y_2$  iteration = 11.9 → RD Overflow  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 59.96 ft\*  $q_2 = Q_2/W_2 = 91$  ft<sup>2</sup>/s

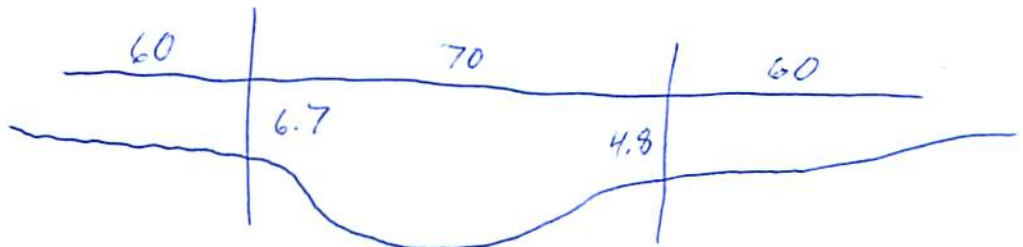
Bridge Vel,  $V_2 = 7.9$  ft/s Final  $y_2 = q_2/V_2 = 11.5$  ft  $\Delta h = 1.3$  ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = 12.8$  ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD,

Water Surface Elev. = \_\_\_\_\_ ft  
 Low Steel Elev. = 11.5 ft  
 $n$  (Channel) = 0.033  
 $n$  (LOB) = 0.035  
 $n$  (ROB) = 0.035  
 Pier Width = 1.6 ft  
 Pier Length = 1.0 ft  
 # Piers for 500 yr = 1 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 = 70$  ft  
 Width of left overbank flow at approach,  $W_{lob} = 60$  ft Average left overbank flow depth,  $y_{lob} = 6.7$  ft  
 Width of right overbank flow at approach,  $W_{rob} = 60$  ft Average right overbank flow depth,  $y_{rob} = 4.8$  ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x = 8.97$  From Figure 9  $W_2$  (effective) = 59 ft  $y_{cs} = 9.9$  ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1.0 Correction factor for flow angle of attack (from Table 1),  $K_2 = 1.0$   
 Froude # at bridge = 0.41 Using pier width  $a$  on Figure 11,  $\xi = 4.9$  Pier scour  $y_{ps} = 4.3$  ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{alT} = 6.7$  ft right abutment,  $y_{arT} = 4.8$  ft  
 Shape coefficient  $K_1 = 1.00$  for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{alT}$  and  $y_{arT}$  on figure 12,  $\psi_{LT} = 18.1$  and  $\psi_{RT} = 14.7$   
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) = 26.9$  ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) = 21.9$  ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Pie

PRGM: Abutment



Route Cox Rd Stream Crooked Ck MRM \_\_\_\_\_ Date 10/29/11 Initials Cz  
 Bridge Structure No. 32305028 Location 2.5 mi W of US 85 on Cox Rd  
 GPS coordinates: N 45° 54' 32.2" taken from: USL abutment X centerline of  $\uparrow$  MRM end \_\_\_\_\_  
W 103° 25' 43.6" Datum of coordinates: WGS84 X NAD27 \_\_\_\_\_  
 Drainage area = 49.02 sq. mi.  
 The average bottom of the main channel was 16.5 ft below top of guardrail at a point 12 ft from left abutment.  
 Method used to determine flood flows: \_\_\_\_\_ Freq. Anal. \_\_\_\_\_ drainage area ratio \_\_\_\_\_ regional regression equations.

**MISCELLANEOUS CONSIDERATIONS**

Flows	Q <sub>100</sub> = <u>3430</u>			Q <sub>500</sub> = <u>5780</u>		
Estimated flow passing through bridge	<u>3430</u>			<u>5456</u>		
Estimated road overflow & overtopping	<u>        </u>			<u>524</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<u>X</u>		<u>X</u>		
Chance of Pressure flow		<u>X</u>				<u>X</u>
Armored appearance to channel		<u>X</u>			<u>X</u>	
Lateral instability of channel		<u>X</u>			<u>X</u>	

Riprap at abutments? \_\_\_\_\_ Yes X No \_\_\_\_\_ Marginal  
 Evidence of past Scour? X Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know Cattle on banks  
 Debris Potential? \_\_\_\_\_ High \_\_\_\_\_ Med X Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know X NA  
 Spur Dike \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know X NA  
 Other \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know X NA

**Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)**

Material Silt/Clay X Sand X Gravel \_\_\_\_\_ Cobbles \_\_\_\_\_ Boulders \_\_\_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

**Comments, Diagrams & orientation of digital photos**

10/4/11  
2 229  
5 688  
10 1190  
25 1430  
50 2630  
100 3430  
500 5780  
Photos  
 2169 - ID  
 70 - US  
 71 - US RB  
 72 - US LB  
 73 - US Face  
 74 - ~~US~~

**Summary of Results**

	Q100	Q500
Bridge flow evaluated	<u>3430</u>	<u>5456</u>
Flow depth at left abutment (yaLT), in feet	<u>3.7</u>	<u>6.7</u>
Flow depth at right abutment (yaRT), in feet	<u>0.9</u>	<u>4.8</u>
Contraction scour depth (yca), in feet	<u>4.6</u>	<u>9.9</u>
Pier scour depth (yps), in feet	<u>4.2</u>	<u>4.3</u>
Left abutment scour depth (yas), in feet	<u>19.0</u>	<u>26.9</u>
Right abutment scour depth (yas), in feet	<u>5.8</u>	<u>21.9</u>
If low angle of attack	<u>2</u>	<u>2</u>

See Comments/Diagram for justification where required