	SCOUR ANALYSIS AND REPORTING FORM							
	Bridge Structure No. 32395080 Date 0/29/11 Initials (Region (ABCD)							
	Site Location 6.5 m; Ft of US 85 ou Ludlow Rd Q ₁₀₀ = 862 by: drainage area ratio flood freq. anal regional regression eq.							
25	Q ₁₀₀ =							
	Bridge discharge $(Q_2) = 2$ (should be Q_{100} unless there is a relief bridge, road overflow, or bridge overtopping)							
	Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method							
PGRM: "RegionA", "RegionB", 'RegionC", or "RegionD"	Bridge Width = $\frac{32}{3}$ ft. Flow angle at bridge = $\frac{33}{3}$ Abut. Skew = $\frac{33}{3}$ ° Effective Skew = $\frac{33}{3}$ ° Width (W ₂) iteration = $\frac{33}{3}$							
Reginup"	Avg. flow depth at bridge, y_2 iteration = $\frac{1}{2} \frac{1}{2} \frac{1}{2}$							
A", "A	Corrected channel width at bridge Section = W_2 times cos of flow angle = 31.96 ft* $q_2 = Q_2/W_2 = 27.0$ ft ² /s							
PGRM: "RegionA", "Regi 'RegionC", or "RegionD"	Corrected channel width at bridge Section = W_2 times cos of flow angle = 31.96 ft* $q_2 = Q_2/W_2 = 27.0$ ft²/s Bridge Vel, $V_2 = 4.0$ ft $\Delta h = 0.0$ ft							
"."Re	Average main channel depth at approach section, $y_1 = \Delta h + y_2 = 6.5$ ft							
RM	* NOTE: repeat above calculations until y $_2$ changes by less than 0.2 Effective pier width = $L \sin(q) + a \cos(q)$							
P. R.	If y 2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD,							
	Water Surface Elev. = $\frac{1}{20}$ ft $\frac{1}{20}$ ft $\frac{1}{20}$ ft $\frac{1}{20}$ $\frac{1}{20}$ ft $\frac{1}{20}$							
٠	n (Channel) = 0.045							
	n(LOB) = 0.035 3.6							
	n (ROB) = 0.635 Pier Width = ft							
	Pier Length =ft							
	# Piers for $100 \text{ yr} = $ ft							
	CONTRACTION SCOUR							
PGRM: Contract	Width of main channel at approach section $W_1 = 35$ ft Width of left overbank flow at approach, $W_{lob} = 32$ ft Average left overbank flow depth, $y_{lob} = 3.6$ ft							
	Width of left overbank flow at approach, $W_{lob} = 52$ it Average left overbank flow depth, $y_{lob} = 5.8$ it							
	Width of right overbank flow at approach, $W_{rob} = 32$ ft Average right overbank flow depth, $y_{rob} = 4.0$ ft							
PGI	Live Bed Contraction Scour (use if bed material is small cobbles or finer)							
	$x = $ From Figure 9 W_2 (effective) =ft $y_{cs} = $ ft							
WE	Clear Water Contraction Scour (use if bed material is larger than small cobbles)							
PGRM: CWCSNEW	Estimated bed material $D_{50} = 0$ ft Average approach velocity, $V_1 = Q_{100}/(y_1W_1) = 1.34$ ft/s							
CW	Critical approach velocity, $Vc = 11.17y_1^{1/6}D_{50}^{1/3} = 11.2 \mu$ ft/s							
RM:	If $V_1 < V_c$ and $D_{50} >= 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above.							
PG	$D_{c50} = 0.0006(q_2/y_1^{7/6})^3 = 0.007$ ft If $D_{50} > D_{c50}$, $\sqrt{0.0}$							
	Otherwise, $\chi = 0.122y_1[q_2/(D_{50}^{1/3}y_1^{7/6})]^{6/7} - y_1 = $ From Figure 10, $y_{cs} = $ ft							
cr	PIER SCOUR CALCULATIONS							
PGRM: Pier	L/a ratio = Correction factor for flow angle of attack (from Table 1), K2=							
PGR	L/a ratio = Correction factor for flow angle of attack (from Table 1), $K2$ = Froude # at bridge = Using pier width a on Figure 11, ξ = Pier scour y_{ps} =ft							
Ħ	ABUTMENT SCOUR CALCULATIONS							
PGRM: Abutment	Average flow depth blocked by: left abutment, $y_{aLT} = 3.6$ ft right abutment, $y_{aRT} = 4.0$ ft							
: Abı	Shape coefficient K ₁ = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through							
RM	Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} = 12.6$ and $\psi_{RT} = 13.3$ Left abutment scour, $y_{as} = \psi_{LT}(K_1/0.55) = 22.8$ ft Right abutment scour $y_{as} = \psi_{RT}(K_1/0.55) = 24.1$ ft							

Route Livelon Ro Stream Coal Bank Ck MRM Date $\frac{10}{29}$ Initials Cm Bridge Structure No. $\frac{32395080}{32395080}$ Location 6.5 m' 5 of Livelon on Livelon Rd GPS coordinates: $\frac{745^{\circ}50'04'4''}{103^{\circ}14'36.3''}$ taken from: USL abutment centerline of $\frac{10}{103}$ MRM end Datum of coordinates: WGS84 NAD27 Drainage area = $\frac{12.08}{12.08}$ sq. mi. The average bottom of the main channel was $\frac{9}{11.1}$ ft below top of guardrail at a point $\frac{9}{11.1}$ ft from left abutment.								
Method used to determine flood flows:Freq.	Method used to determine flood flows:Freq. Analdrainage area ratioregional regression equations.							
MIS	MISCELLANEOUS CONSIDERATIONS 50							
Flows 35	\$62			- OSO0 = 1180				
Estimated flow passing through bridge	860			1133				
Estimated road overflow & overtopping	766			47				
Consideration	Yes	No	Possibly	Yes	No	Possibly		
Chance of overtopping		X	1 0331019	X	110	Tossiony		
Chance of Pressure flow		X				X		
Armored appearance to channel		X			V			
Lateral instability of channel		\rightarrow			-			
Eateral instability of channel		$\overline{}$						
Riprap at abutments?								
500 2650 74-R. Abut								
Summary of Results								
	Q196			Q 500_ 50				
Bridge flow evaluated	25			50				
Flow depth at left abutment (yaLT), in feet	2 6			46				
Flow depth at right abutment (yaRT), in feet	40			60				
Contraction scour depth (ycs), in feet	7.0			0.0				
Pier scour depth (yps), in feet	0.0			0.0				
Left abutment scour depth (yas), in feet	22.8			200				
Right abutment scour depth (yas), in feet	22.8			26.2				
1Flow angle of attack	241			3				