

OK RT check

Check Flows...

### SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 33288023 Date 7/16/12 Initials Rat Region (A B C D) D  
 Site \_\_\_\_\_ Location nr Blunt on 308 Ave  
 $Q_{100} =$  90 4310 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 4310 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 104 ft. Flow angle at bridge = 5 ° Abut. Skew = 0 ° Effective Skew = 5 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_

Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 103.6 ft\*  $q_2 = Q_2/W_2 =$  41.6 ft<sup>2</sup>/s

Bridge Vel,  $V_2 =$  4.6 ft/s Final  $y_2 = q_2/V_2 =$  9.1 ft  $\Delta h =$  0.4 ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  9.5 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0-1.0 ft  
 Low Steel Elev. = 12.6 ft  
 n (Channel) = 0.043  
 n (LOB) = 0.070  
 n (ROB) = 0.030  
 Pier Width = 1.65 ft  
 Pier Length = 1.7 ft  
 # Piers for 100 yr = 34



#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 =$  104 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  0 ft Average left overbank flow depth,  $y_{lob} =$  0 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  0 ft Average right overbank flow depth,  $y_{rob} =$  0 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  0.69 From Figure 9  $W_2$  (effective) = 97 ft  $y_{cs} =$  1.1 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006(q_2/y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

#### PIER SCOUR CALCULATIONS

L/a ratio = 1.03 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.27 Using pier width a on Figure 11,  $\xi =$  6.9 Pier scour  $y_{ps} =$  5.7 ft

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} =$  0 ft right abutment,  $y_{aRT} =$  0 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  0 and  $\psi_{RT} =$  0  
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  0 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  0 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCSNEW

PRGM: Pier

PRGM: Abutment



**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 33288023 Date 7/10/12 Initials RL Region (A B C D) D  
 Site \_\_\_\_\_ Location nr Blunt on 308 Ave  
 $Q_{500} =$  625 10200 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 8268 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 104 ft. Flow angle at bridge = 5 ° Abut. Skew = 0 ° Effective Skew = 5 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_

Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 103.6 ft\*  $q_2 = Q_2/W_2 =$  79.8 ft<sup>2</sup>/s

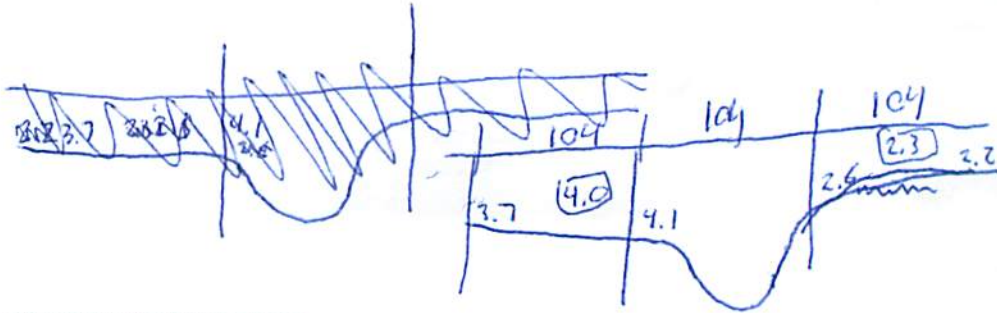
Bridge Vel,  $V_2 =$  6.3 ft/s Final  $y_2 = q_2/V_2 =$  12.6 ft  $\Delta h =$  0.9 ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  13.4 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0-1.0 ft  
 Low Steel Elev. = 12.6 ft  
 $n$  (Channel) = 0.040  
 $n$  (LOB) = 0.070  
 $n$  (ROB) = 0.030  
 Pier Width = 1.65 ft  
 Pier Length = 1.70 ft  
 # Piers for 500 yr = 4



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  104 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  104 ft Average left overbank flow depth,  $y_{lob} =$  4.0 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  104 ft Average right overbank flow depth,  $y_{rob} =$  2.3 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  3.08 From Figure 9  $W_2$  (effective) = 97 ft  $y_{cs} =$  3.7 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1)^{7/6} =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

$L/a$  ratio = 103 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.31 Using pier width  $a$  on Figure 11,  $\xi =$  6.9 Pier scour  $y_{ps} =$  5.8 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  4.0 ft right abutment,  $y_{aRT} =$  2.3 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  13.3 and  $\psi_{RT} =$  9.4  
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  13.3 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  9.4 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Pie

PRGM: Abutment

Route 308 Arc Stream MRM Date 7/10/12 Initials Rat  
 Bridge Structure No. 33294023 Location nr Blunt on 308 Arc  
 GPS coordinates: N 44° 30' 27.9" taken from: USL abutment  centerline of ↑ MRM end \_\_\_\_\_  
W 99° 59' 20.8" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 103.69 sq. mi.  
 The average bottom of the main channel was 16.1 ft below top of guardrail at a point 30 ft from left abutment.  
 Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio  regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	$Q_{100} = Q_{10} \quad 4310$			$Q_{500} = Q_{25} \quad 10200$		
Estimated flow passing through bridge	4310			8268		
Estimated road overflow & overtopping	0			1932		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Chance of Pressure flow		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

8/24  

2	411
5	1900
10	4310
25	10200
50	17300
100	27500
500	64700

2	236
5	10.9
10	24.7
25	58.5
50	99.2
100	155
500	394

Riprap at abutments? \_\_\_ Yes  No \_\_\_ Marginal  
 Evidence of past Scour?  Yes \_\_\_ No \_\_\_ Don't know *minor pier/contraction*  
 Debris Potential? \_\_\_ High \_\_\_ Med  Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Spur Dike \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Other \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA

Bed Material Classification Based on Median Particle Size ( $D_{50}$ )

Material Silt/Clay  Sand \_\_\_ Gravel \_\_\_ Cobbles \_\_\_ Boulders \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos  
 1). left ab  
 2). main channel  
 3). right ab  
 4). piers  
 5). right abutment  
 6-7). left abutment  
 8). right abutment  
 9). main channel - too many trees for proper picture.

Summary of Results

	$Q_{100} \quad Q_{10}$	$Q_{500} \quad Q_{25}$
Bridge flow evaluated	4310	8268
Flow depth at left abutment (yaLT), in feet	0	4.0
Flow depth at right abutment (yaRT), in feet	0	2.3
Contraction scour depth (yca), in feet	6.1	3.7
Pier scour depth (yca), in feet	5.7	5.8
Left abutment scour depth (yca), in feet	0	13.3
Right abutment scour depth (yca), in feet	0	9.4
Flow angle of attack	5	5

See Comments/Diagram for justification where required