

Dup OK-RAT

308

### SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 33288023 Date 10-4-12 Initials RFT Region (A B C D) (D)

Site \_\_\_\_\_ Location nr Blunk on 308 Ave

$Q_{100} =$  4310 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X

Bridge discharge ( $Q_2$ ) = 4310 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 102 ft. Flow angle at bridge = 6 ° Abut. Skew = 0 ° Effective Skew = 6 °

Width ( $W_2$ ) iteration = 102

Avg. flow depth at bridge,  $y_2$  iteration = 9.2

Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 101.44 ft\*  $q_2 = Q_2/W_2 =$  42.5 ft<sup>2</sup>/s

Bridge Vel,  $V_2 =$  4.6 ft/s Final  $y_2 = q_2/V_2 =$  9.2 ft  $\Delta h =$  0.4 ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  9.6 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2

Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

$y_2 > 9$  is about to about. flow

Water Surface Elev. = 70.8 ft

Low Steel Elev. = 12.5 ft

n (Channel) = .045

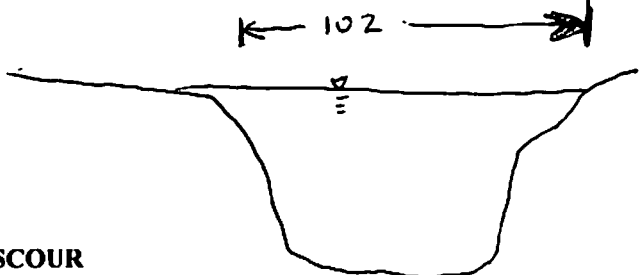
n (LOB) = .065 trees, scrub

n (ROB) = .030 grassy yard

Pier Width = 1.65 ft

Pier Length = 1.7 ft

# Piers for 100 yr = 4 ft



#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 =$  102 ft

Width of left overbank flow at approach,  $W_{lob} =$  12 ft

Average left overbank flow depth,  $y_{lob} =$  0.15 ft

Width of right overbank flow at approach,  $W_{rob} =$  0 ft

Average right overbank flow depth,  $y_{rob} =$  0 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  0.73 From Figure 9

$W_2$  (effective) = 94.8 ft  $y_{cs} =$  1.1 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} >= 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft

If  $D_{50} >= D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_

From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

#### PIER SCOUR CALCULATIONS

L/a ratio = 1

Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1

Froude # at bridge = 0.27

Using pier width a on Figure 11,  $\xi =$  6.9 Pier scour  $y_{ps} =$  5.7 ft

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} =$  0.15 ft right abutment,  $y_{aRT} =$  0 ft

Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through

Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  0.7 and  $\psi_{RT} =$  0

Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) =$  0.7 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) =$  0 ft

44° 30.45594'  
99° 59.3454'  
308 Ave

44.507599  
99.98909

103497 = L 1962

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pier

PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 33288023 Date \_\_\_\_\_ Initials \_\_\_\_\_ Region (A B C D) C  
 Site \_\_\_\_\_ Location \_\_\_\_\_  
 $Q_{500} = 10200$  by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 9713 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 102 ft. Flow angle at bridge = 6° Abut. Skew = 0° Effective Skew = 6°  
 Width ( $W_2$ ) iteration = 102

Avg. flow depth at bridge,  $y_2$  iteration = 13.8

Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 101.44 ft\*  $q_2 = Q_2/W_2 = 95.8$  ft<sup>2</sup>/s

Bridge Vel,  $V_2 = 6.9$  ft/s Final  $y_2 = q_2/V_2 = 13.8$  ft  $\Delta h = 1$  ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = 14.8$  ft

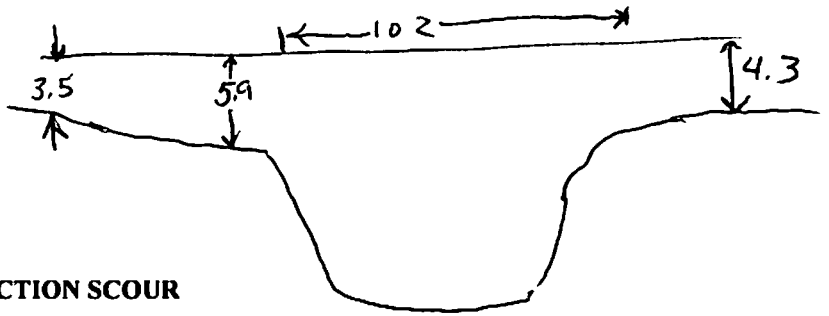
\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2

Effective pier width =  $L \sin(\theta) + a \cos(\theta)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

*road over flow begins at  $y_2 \approx 13.8$  assume this is  $Q_{max}$  scour*

Water Surface Elev. = 20.8 ft  
 Low Steel Elev. = 12.5 ft  
 n (Channel) = .045  
 n (LOB) = .065  
 n (ROB) = .030  
 Pier Width = 1.45 ft  
 Pier Length = 1.7 ft  
 # Piers for 500 yr = 4 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 = 102$  ft

Width of left overbank flow at approach,  $W_{lob} = 102$  ft

Average left overbank flow depth,  $y_{lob} = 4.7$  ft

Width of right overbank flow at approach,  $W_{rob} = 102$  ft

Average right overbank flow depth,  $y_{rob} = 4.3$  ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x = 5.79$  From Figure 9  $W_2$  (effective) = 94.8 ft  $y_{cs} = 6.5$  ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} >= 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1)^{7/6} =$  \_\_\_\_\_ ft

If  $D_{50} >= D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1

Correction factor for flow angle of attack (from Table 1),  $K_2 = 1$

Froude # at bridge = 0.33

Using pier width  $a$  on Figure 11,  $\xi = 6.9$  Pier scour  $y_{ps} = 5.8$  ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} = 4.7$  ft right abutment,  $y_{aRT} = 4.3$  ft

Shape coefficient  $K_1 = 1.00$  for vertical-wall,  $0.82$  for vertical-wall with wingwalls, 0.55 for spill-through

Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = 14.5$  and  $\psi_{RT} = 13.8$

Left abutment scour,  $y_{as} = \psi_{LT} (K_1/0.55) = 14.5$  ft Right abutment scour  $y_{as} = \psi_{RT} (K_1/0.55) = 13.8$  ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pie

PGRM: Abutment

Route 308 Ave Stream \_\_\_\_\_ MRM \_\_\_\_\_ Date \_\_\_\_\_ Initials \_\_\_\_\_  
 Bridge Structure No. 33288023 Location pr Blunt on 308 Ave  
 GPS coordinates: 44° 30.471' taken from: USL abutment  centerline of  $\uparrow$  MRM end \_\_\_\_\_  
99° 59.328' Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 103.69 sq. mi.  
 The average bottom of the main channel was 16.1 ft below top of guardrail at a point .35 ft from left abutment.  
 Method used to determine flood flows: \_\_\_\_\_ Freq. Anal. \_\_\_\_\_ drainage area ratio  regional regression equations.

**MISCELLANEOUS CONSIDERATIONS**

Flows	Q <sub>100</sub> = <u>4310</u>			Q <sub>25</sub> = <u>10200</u>		
Estimated flow passing through bridge	<u>4310</u>			<u>9713</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>486</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Chance of Pressure flow		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

Riprap at abutments? \_\_\_\_\_ Yes  No \_\_\_\_\_ Marginal  
 Evidence of past Scour? \_\_\_\_\_ Yes \_\_\_\_\_ No  Don't know *no obvious scour*  
 Debris Potential?  High  Med \_\_\_\_\_ Low *some trees, beaver activity at this bridge*  
*there is a low (~1ft) beaver dam near downstream face of bridge*  
 Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know \_\_\_\_\_ NA  
 Spur Dike \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know  NA  
 Other \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know  NA

**Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)**

Material Silt/Clay  Sand \_\_\_\_\_ Gravel \_\_\_\_\_ Cobbles \_\_\_\_\_ Boulders \_\_\_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

**Comments, Diagrams & orientation of digital photos**

*str. no approach from bridge*  
*LOB from bridge*  
*ROB from ~~bridge~~ road*  
*bridge section from LOB*  
*left abut. under bridge*  
*rt. abut. under bridge*

**Summary of Results**

	Q <sub>100</sub> = <u>10</u>	Q <sub>25</sub> = <u>25</u>
Bridge flow evaluated	<u>4310</u>	<u>9713</u>
Flow depth at left abutment (yaLT), in feet	<u>0.15</u>	<u>4.7</u>
Flow depth at right abutment (yaRT), in feet	<u>0</u>	<u>4.3</u>
Contraction scour depth (yca), in feet	<u>1.1</u>	<u>6.5</u>
Pier scour depth (yps), in feet	<u>5.7</u>	<u>5.8</u>
Left abutment scour depth (yas), in feet	<u>0.7</u>	<u>14.5</u>
Right abutment scour depth (yas), in feet	<u>0</u>	<u>13.8</u>
Flow angle of attack	<u>6°</u>	<u>6°</u>

See Comments/Diagram for justification where required