Q<sub>100</sub> = 1940 by: drainage area ratio flood freq. anal. regional regression eq. \_\_

Bridge discharge  $(Q_2) = (Q_1 \cup Q_2)$  (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 54 ft. Flow angle at bridge = 16° Abut. Skew = 0° Effective Skew = 16°

Width  $(W_2)$  iteration = 52 50 51 Avg. flow depth at bridge,  $y_2$  iteration = 8.8 9.0 8.9

Corrected channel width at bridge Section =  $W_2$  times cos of flow angle =  $\frac{49.0 \text{ Z}}{100}$  ft\*  $q_2 = Q_2/W_2 = \frac{39.6}{100}$  ft<sup>2</sup>/s

Bridge Vel,  $V_2 = 4.5$  ft/s Final  $y_2 = q_2/V_2 = 8.9$  ft  $\Delta h = 0.4$  ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = 9.3$  ft

\* NOTE: repeat above calculations until y 2 changes by less than 0.2 Effective pier width = L sin(q) + a cos(q)

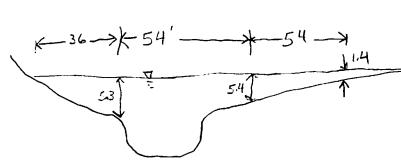
If y ; is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD,

Water Surface Elev. = d(い Low Steel Elev. = 14.0 n (Channel) = \_\_\_\_\_040

 $n \text{ (LOB)} = \frac{0.3^{\circ}}{10.00}$ n(ROB) = .035

Pier Width = 1.6 ft est = 2.50

Pier Length = 3.5# Piers for 100 yr = |



## CONTRACTION SCOUR

Width of main channel at approach section  $W_1 = 5^{14}$  ft

Width of right overbank flow at approach,  $W_{mb} = 5^{\mu}$ 

Width of left overbank flow at approach,  $W_{lob} = 36$  ft Average left overbank flow depth,  $y_{lob} = 2.65$  ft

Average right overbank flow depth,  $y_{rob} = 3.4$ 

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$$x = 4.82$$
 From Figure 9

$$W_2$$
 (effective) =  $4 \frac{5}{100}$  ft  $y_{cs} = \frac{5.5}{100}$  ft

$$y_{cs} = 5.5$$
 fr

Clear Water Contraction Scour (use if bed material is larger than small-cobbles)

Estimated bed material  $D_{50} = 1$  Average approach velocity,  $V_1 = Q_{100}/(y_1W_1) = 1$ 

Critical approach velocity,  $Vc = 11.17y_1^{1/6}D_{50}^{1/6} =$ If  $V_1 < V_c$  and  $D_{50} >= 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$$D_{c50} = 0.0006(q_2/y_1^{7/6})^3 = f$$

If  $D_{50} >= D_{c50}$ ,  $\chi = 0.0$ 

Otherwise,  $\chi = 0.122y_1[q_2/(D_{50}^{1/3}y_1^{7/6})]^{6/7} - y_1 =$ 

From Figure 10, y<sub>cs</sub> =

## PIER SCOUR CALCULATIONS

L/a ratio =  $\frac{2 \cdot 2}{\text{Froude # at bridge = } 2.27}$ 

Correction factor for flow angle of attack (from Table 1), K2 = 1.3Using pier width a on Figure 11,  $\xi = 6$ , 7 Pier scour  $y_{ps} = 7$ , 2 ft

## ABUTMENT SCOUR CALCULATIONS

left abutment,  $y_{aLT} = 2.65$  ft right abutment,  $y_{aRT} = 3.4$ Average flow depth blocked by: Shape coefficient  $K_1$ = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls,

Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = 10.8$  and  $\psi_{RT} = 12.2$ 

Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) = 10.8$  ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) = 12.2$  ft

PGRM: Contract

PGRM: CWCSNEW

Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) = 15.5$  ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) = 20.2$  ft

Route 418 Avc Stream S. Brand	2 Dry Cl	MRM	Da	ite	Init	tials_	
Bridge Structure No. 34140101 L	ocation 2	278/n 4	118 Ave				_
GPS coordinates: N 43° 21.272' taken from: USL abutment centerline of \(\hat{\cappa}\) MRM end							_
W97. 50.214		ordinates: W	GS84	. NAD27_			
Drainage area = $25.76$ sq. m							
The average bottom of the main channel was	8,9_ft below	v top of guard	rail at a poin	ıt <u>17                                    </u>	_ft from lef	ft abutment.	
Method used to determine flood flows:Fre	q. Anai	drainage area	ratio	regional reg	ression equ	ations.	
M	IISCELLANE	OUS CONSI	DERATIO	NS			
Flows	Q <sub>100</sub> = 1940			Q <sub>500</sub> = 4810			1
Estimated flow passing through bridge	1940			4810			ĺ
Estimated road overflow & overtopping		Ü			$\mathcal{O}$		
Consideration	Yes	No	Possibly	Yes	No	Possibly	
Chance of overtopping					1		
Chance of Pressure flow							
Armored appearance to channel							
Lateral instability of channel							
							•
Riprap at abutments? Yes	No	Marginal			7 .	0 1:-	avanset
Evidence of past Scour? Yes	No	Don't knov	v mutrad	ion Scou	r: bi	er tooting	3 exposes
Debris Potential?High	MedX	Low	it 100	ks like	the ac	erfooting outment	5 were
			Scouri	ry ceto	ice the	cibrof	s was
Does scour countermeasure(s) appear to have be	en designed?		b,acsc	. •		ŕ	
Riprap	YesN	lo Do	n't know	NA			
Spur Dike	Yes N		n't know	NA			
<del></del>			n't know	NA NA			
<u> </u>		D0	ii t Kilow				
Bed Materi	al Classificatio	n Based on M	edian Partic	le Size (D.	ı		
		Gravel		Cobbles		Boulders	
Size range, in mm <0.062 0.062-	<del>-,</del>	2.00-64		64-250		>250	
5120 runge, in min	2.00	2.00-04		04-230		-230	
Comments, Diagrams & orientation of digital ph	otos						
Str. no.	left	abut-					
bridge from approach	·	abut					
LOB							
	Piel	r footin	٩				
ROB	•		$\sim$	. 1			
	$\circ bbc$	sach ?	com pa	iage			
Summary of Results	3.4						
outlines) of resource	1	Q100		Ī	Q500		
Bridge flow evaluated	1940			H810			
Flow depth at left abutment (yaLT), in feet	2,65			5,25			
Flow depth at right abutment (yaRT), in feet			8,6				
Contraction scour depth (ycs), in feet	<del></del>	3.4 5.5			13.3		İ
Pier scour depth (yps), in feet	<del> </del>	7.2		<u> </u>	7,4		
Left abutment scour depth (yas), in feet							
Right abutment scour depth (yas), in feet	1	10.8			15.5 20.2		

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1Flow angle of attack