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SCOUR ANALYSIS AND REPORTING FORM

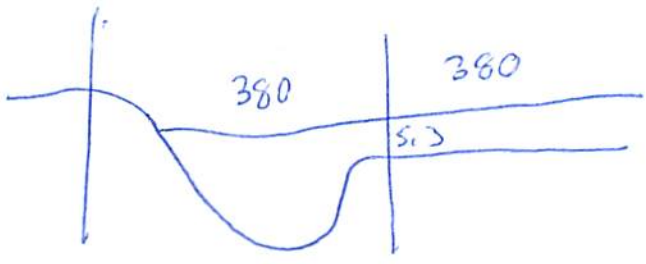
Bridge Structure No. 34162052 Date 6/6/12 Initials [signature] Region (A B C D)
Site Location nr Milltown on Keiper Rd
Q100 = 45300 by: drainage area ratio flood freq. anal. regional regression eq. X
Bridge discharge (Q2) = 45300 (should be Q100 unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 380 ft. Flow angle at bridge = 5 degrees Abut. Skew = 0 degrees Effective Skew = 5 degrees
Width (W2) iteration = 378.55 352.65 349 342.64
Avg. flow depth at bridge, y2 iteration = 15.4 16 15.5 W2 = 362.61
Corrected channel width at bridge Section = W2 times cos of flow angle = 378.55 ft\* q2 = Q2/W2 = 124.9 ft^2/s
Bridge Vel, V2 = 7.9 ft/s Final y2 = q2/V2 = 15.8 ft Delta h = 1.3 ft
Average main channel depth at approach section, y1 = Delta h + y2 = 17.0 ft

\*NOTE: repeat above calculations until y2 changes by less than 0.2 Effective pier width = L sin(q) + a cos(q)
If y2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 5.3 ft
Low Steel Elev. = 20.0 ft
n (Channel) = 0.040
n (LOB) = 0.040
n (ROB) = 0.035
Pier Width = 2.95 ft
Pier Length = 2.95 ft
# Piers for 100 yr = 4



CONTRACTION SCOUR

Width of main channel at approach section W1 = 380 ft
Width of left overbank flow at approach, Wlob = 0 ft Average left overbank flow depth, ylob = 0 ft
Width of right overbank flow at approach, Wrob = 380 ft Average right overbank flow depth, yrob = 5.3 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)
x = 4.43 From Figure 9 W2 (effective) = 350.8 ft ycs = 5.1 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)
Estimated bed material D50 = ft Average approach velocity, V1 = Q100/(y1W1) = ft/s
Critical approach velocity, Vc = 11.17y1^1/6 D50^1/3 = ft/s
If V1 < Vc and D50 >= 0.2 ft, use clear water equation below, otherwise use live bed scour equation above.
Dc50 = 0.0006(q2/y1^7/6)^3 = ft If D50 >= Dc50, chi = 0.0
Otherwise, chi = 0.122y1[q2/(D50^1/3 y1^7/6)]^6/7 - y1 = ft From Figure 10, ycs = ft

PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1), K2 = 1
Froude # at bridge = 0.35 Using pier width a on Figure 11, xi = 10.6 Pier scour yps = 9.1 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, yaLT = 1.0 ft right abutment, yaRT = 5.3 ft
Shape coefficient K1 = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
Using values for yaLT and yaRT on figure 12, psiLT = 4.3 and psiRT = 15.6
Left abutment scour, yas = psiLT(K1/0.55) = 4.3 ft Right abutment scour yas = psiRT(K1/0.55) = 15.6 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCSNEW

PRGM: Pier

PRGM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 34162052 Date 6/6/12 Initials RAV Region (A B C D) D  
 Site \_\_\_\_\_ Location nr Milltown on Keiper Rd  
 $Q_{500} = \underline{77300}$  by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = ~~76500~~ 76200 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

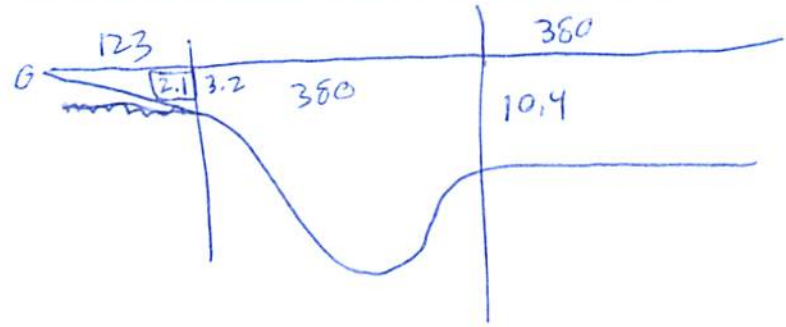
Bridge Width = 380 ft. Flow angle at bridge = 05° Abut. Skew = 0° Effective Skew = 05°  
 Width ( $W_2$ ) iteration = \_\_\_\_\_

Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 375.4 ft\*  $q_2 = Q_2/W_2 = \underline{20.3}$  ft<sup>2</sup>/s

Bridge Vel,  $V_2 = \underline{10.1}$  ft/s Final  $y_2 = q_2/V_2 = \underline{2.0}$  ft  $\Delta h = \underline{2.1}$  ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = \underline{2.1}$  ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 5.3 ft  
 Low Steel Elev. = 20.0 ft  
 n (Channel) = 0.040  
 n (LOB) = 0.040  
 n (ROB) = 0.035  
 Pier Width = 2.95 ft  
 Pier Length = 2.95 ft  
 # Piers for 500 yr = 4 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 = \underline{380}$  ft  
 Width of left overbank flow at approach,  $W_{lob} = \underline{123}$  ft Average left overbank flow depth,  $y_{lob} = \underline{2.1}$  ft  
 Width of right overbank flow at approach,  $W_{rob} = \underline{380}$  ft Average right overbank flow depth,  $y_{rob} = \underline{10.4}$  ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x = \underline{7.67}$  From Figure 9  $W_2$  (effective) = 375.8 ft  $y_{cs} = \underline{8.5}$  ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} = \underline{8.4}$  ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) = \underline{9.3}$  ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} = \underline{366.8}$  ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2 / y_1)^{7/6} = \underline{8.4}$  ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 = \underline{8.4}$  ft From Figure 10,  $y_{cs} = \underline{8.4}$  ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 = \underline{1}$   
 Froude # at bridge = 0.4 Using pier width a on Figure 11,  $\xi = \underline{10.6}$  Pier scour  $y_{ps} = \underline{9.2}$  ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} = \underline{2.1}$  ft right abutment,  $y_{aRT} = \underline{10.4}$  ft  
 Shape coefficient  $K_1 = 1.00$  for vertical-wall,  $0.82$  for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = \underline{8.6}$  and  $\psi_{RT} = \underline{21.7}$   
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) = \underline{8.6}$  ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) = \underline{21.7}$  ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"  
 PGRM: Contract  
 PGRM: CWCNEW  
 PGRM: Pier  
 PGRM: Abutment



6072h'4h  
61936L'2b

Route Keiper Rd Stream James River MRM \_\_\_\_\_ Date 6/6/12 Initials Pat

Bridge Structure No. 34162052 Location nr Milltown on Keiper Rd

GPS coordinates: N 43° 25' 33.711" taken from: USL abutment  centerline of ↑ MRM end \_\_\_\_\_  
W 97° 47' 37.211" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 17740.55 sq. mi.

The average bottom of the main channel was 16.3 ft below top of guardrail at a point 219 ft from left abutment.

Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio  regional regression equations.

**MISCELLANEOUS CONSIDERATIONS**

Flows	Q <sub>100</sub> = <u>Q<sub>25</sub> 45300</u>			Q <sub>500</sub> = <u>Q<sub>50</sub> 77300</u>		
Estimated flow passing through bridge	<u>45300</u>			<u>76200</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>192</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Chance of Pressure flow		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

5/26  
 2 1520  
 5 5000  
 10 18900  
 25 45300  
 50 77300  
 100 123000  
 500 303000

Riprap at abutments? \_\_\_ Yes \_\_\_ No  Marginal *along left abutment*  
 Evidence of past Scour?  Yes \_\_\_ No \_\_\_ Don't know *contraction*  
 Debris Potential? \_\_\_ High  Med \_\_\_ Low *quite a few unfallen dead trees*

Does scour countermeasure(s) appear to have been designed?  
 Riprap  Yes \_\_\_ No \_\_\_ Don't know \_\_\_ NA *along left abut. lose quartz*  
 Spur Dike \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Other \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA

**Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)**

Material Silt/Clay  Sand \_\_\_ Gravel \_\_\_ Cobbles \_\_\_ Boulders \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos  
 1) main channel  
 2) piers  
 3) right abut  
 4) left abut.  
 5) left abut  
 6) right abut.  
 7) right CB  
 8) main channel  
 9) left CB

**Summary of Results**

	Q <sub>100</sub> <u>Q<sub>25</sub></u>	Q <sub>500</sub> <u>Q<sub>50</sub></u>
Bridge flow evaluated	<u>45300</u>	<u>76200</u>
Flow depth at left abutment (yaLT), in feet	<u>0</u>	<u>2.1</u>
Flow depth at right abutment (yaRT), in feet	<u>5.3</u>	<u>10.4</u>
Contraction scour depth (y <sub>cs</sub> ), in feet	<u>5.1</u>	<u>8.5 9.3</u>
Pier scour depth (y <sub>ps</sub> ), in feet	<u>9.1</u>	<u>9.2</u>
Left abutment scour depth (y <sub>as</sub> ), in feet	<u>4.3</u>	<u>8.6</u>
Right abutment scour depth (y <sub>as</sub> ), in feet	<u>15.6</u>	<u>21.7</u>
IFlow angle of attack	<u>5</u>	<u>5</u>

See Comments/Diagram for justification where required