

OK RT

East to West Flow

SCOUR ANALYSIS AND REPORTING FORM

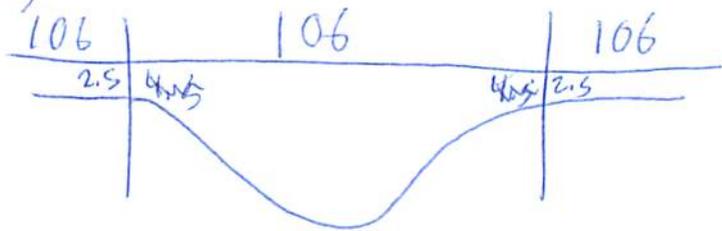
Bridge Structure No. 34200064 Date 6/17/12 Initials RAT Region (A B C D) C
Site Location 0.3 mi S of int of 424 Ave & CR11
Q100 = 4483321 by: drainage area ratio flood freq. anal. regional regression eq. X
Bridge discharge (Q2) = 44821221 (should be Q100 unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 106 ft. Flow angle at bridge = 450 degrees Abut. Skew = 0 degrees Effective Skew = 450 degrees
Width (W2) iteration =
Avg. flow depth at bridge, y2 iteration =
Corrected channel width at bridge Section = W2 times cos of flow angle = 74.95 ft\* q2 = Q2/W2 = 16.3 ft^2/s
Bridge Vel, V2 = 2.9 ft/s Final y2 = q2/V2 = 5.7 ft Delta h = 0.2 ft
Average main channel depth at approach section, y1 = Delta h + y2 = 5.9 ft

\*NOTE: repeat above calculations until y2 changes by less than 0.2 Effective pier width = L sin(q) + a cos(q)
If y2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 6.5 ft
Low Steel Elev. = 5.7 ft
n (Channel) = 0.035
n (LOB) = 0.035
n (ROB) = 0.035
Pier Width = 1.35 ft
Pier Length = 1.35 ft
# Piers for 100 yr = 5



CONTRACTION SCOUR

Width of main channel at approach section W1 = 106 ft
Width of left overbank flow at approach, Wlob = 106 ft Average left overbank flow depth, ylob = 2.5 ft
Width of right overbank flow at approach, Wrob = 106 ft Average right overbank flow depth, yrob = 2.5 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)
x = 9.53 From Figure 9 W2 (effective) = 60.2 ft ycs = 10.5 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)
Estimated bed material D50 = ft Average approach velocity, V1 = Q100/(y1W1) = ft/s
Critical approach velocity, Vc = 11.17y1^1/6 D50^1/3 = ft/s
If V1 < Vc and D50 >= 0.2 ft, use clear water equation below, otherwise use live bed scour equation above.
Dc50 = 0.0006(q2/y1^7/6)^3 = ft If D50 >= Dc50, chi = 0.0
Otherwise, chi = 0.122y1[q2/(D50^1/3 y1^7/6)]^6/7 - y1 = From Figure 10, ycs = ft

PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1), K2 = 1
Froude # at bridge = 0.21 Using pier width a on Figure 11, xi = 6 Pier scour yps = 4.7 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, yaLT = 4.5 ft right abutment, yaRT = 4.5 ft
Shape coefficient K1 = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
Using values for yaLT and yaRT on figure 12, psiLT = 10.2 and psiRT = 10.2
Left abutment scour, yas = psiLT(K1/0.55) = 18.6 ft Right abutment scour yas = psiRT(K1/0.55) = 18.6 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"
PGRM: Contract
PGRM: CWCSNEW
PGRM: Pier
PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

West to East Flow

Bridge Structure No. 34200064 Date 8/7/12 Initials RAT Region (A B C D) (C)  
 Site \_\_\_\_\_ Location 0.3 mi S of 424 Ave & CR11  
 $Q_{500} =$  2100 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 1221 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 106 ft. Flow angle at bridge = 45 ° Abut. Skew = 0 ° Effective Skew = 45 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_

Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 74.95 ft\*  $q_2 = Q_2/W_2 =$  16.3 ft<sup>2</sup>/s

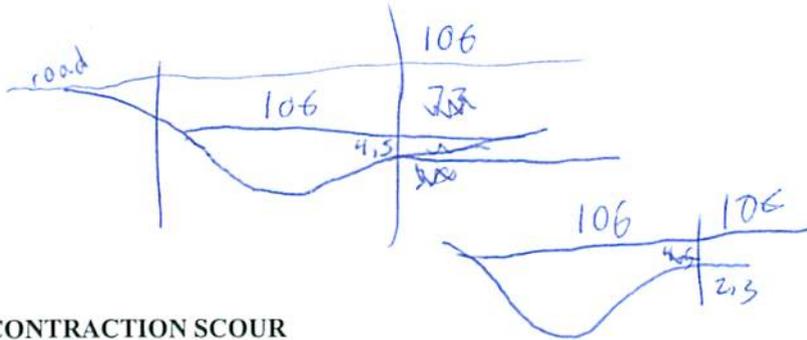
Bridge Vel,  $V_2 =$  2.9 ft/s Final  $y_2 = q_2/V_2 =$  5.7 ft  $\Delta h =$  0.2 ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  5.9 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0.5 ft  
 Low Steel Elev. = 5.7 ft  
 $n$  (Channel) = 0.035  
 $n$  (LOB) = 0.035  
 $n$  (ROB) = 0.035  
 Pier Width = 1.35 ft  
 Pier Length = 1.35 ft  
 # Piers for 500 yr = 5



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  106 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  0 ft Average left overbank flow depth,  $y_{lob} =$  0 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  106 ft Average right overbank flow depth,  $y_{rob} =$  2.5 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  6.4 From Figure 9  $W_2$  (effective) = 68.2 ft  $y_{cs} =$  7.2 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} >= 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} >= D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

$L/a$  ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.21 Using pier width  $a$  on Figure 11,  $\xi =$  6 Pier scour  $y_{ps} =$  4.7 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  1.5 ft right abutment,  $y_{aRT} =$  2.5 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  6.3 and  $\psi_{RT} =$  10.2  
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  11.4 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  18.6 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"  
 PRGM: Contract  
 PRGM: CWCSNEW  
 PRGM: Pie  
 PRGM: Abutment

430 241 33.624  
970 431 6.4124  
60.43

97.

43.40034  
97.71647

Route 424 Ave Stream MRM Date 6/7/12 Initials RAT

Bridge Structure No. 34200064 Location 0.3 mi S of 424 Ave & CR11

GPS coordinates: N 43° 24' 33.0" taken from: USL abutment  centerline of ↑ MRM end \_\_\_\_\_  
W 97° 43' 6.99" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 0.07 *← from Stream Stats* sq. mi.

The average bottom of the main channel was 10.0 ft below top of guardrail at a point 50 ft from left abutment.

Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio  regional regression equations.

**MISCELLANEOUS CONSIDERATIONS**

Flows	Q <sub>100</sub> = West → East			Q <sub>500</sub> = East → West		
	Yes	No	Possibly	Yes	No	Possibly
Estimated flow passing through bridge						
Estimated road overflow & overtopping						
Chance of overtopping	<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>
Chance of Pressure flow	<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

Riprap at abutments? \_\_\_ Yes \_\_\_ No  Marginal  
 Evidence of past Scour?  Yes \_\_\_ No \_\_\_ Don't know  
 Debris Potential?  High \_\_\_ Med \_\_\_ Low

*depending on James River floods otherwise low*

Does scour countermeasure(s) appear to have been designed?  
 Riprap  Yes \_\_\_ No \_\_\_ Don't know \_\_\_ NA  
 Spur Dike \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Other \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA

*rose quartz along left abutment*

**Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)**

Material Silt/Clay \_\_\_ Sand  Gravel \_\_\_ Cobbles \_\_\_ Boulders \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos  
 1-2), left abutment  
 3), piers  
 4-5), right abutment  
 6-9) debris

*Note channel is dry and road map not high enough resolution to determine upstream/downstream. Assumed flow towards James River Stream state also showed two culverts crossing the road at this point. Used lower flows. It is likely this bridge would receive some flow from James River in the event of a flood, which would explain the*

**Summary of Results**

	Q <sub>100</sub> West → East	Q <sub>500</sub> East → West
Bridge flow evaluated	1221	1221
Flow depth at left abutment (yaLT), in feet	2.5	0
Flow depth at right abutment (yaRT), in feet	2.5	2.5
Contraction scour depth (y <sub>cs</sub> ), in feet	10.5	7.2
Pier scour depth (y <sub>ps</sub> ), in feet	4.7	7.7
Left abutment scour depth (y <sub>as</sub> ), in feet	12.6	11.1
Right abutment scour depth (y <sub>rs</sub> ), in feet	18.6	18.6
Flow angle of attack	7	45

*debris and possibly change flow direction. Ran calculations at low level road. And calculated to both directions.*

See Comments/Diagram for justification where required

*West → East  
 ↑  
 East → West*

*5/24*

*2 4.7  
 5 11.1  
 10 17.1  
 25 26.6  
 50 34.9  
 100 44.2  
 500 69.1*

*0.1  
 5/24*

*2 1960  
 5 8230  
 10 19203  
 25 46000  
 50 75500  
 100 125000  
 500 308000*