

OK RT

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 3424611 Date 6/7/12 Initials Lat Region (A B D)
 Site _____ Location nr Wolf Ck colony, Wolf Meano
 $Q_{100} = \underline{81000}$ by: drainage area ratio _____ flood freq. anal. _____ regional regression eq. X
 Bridge discharge (Q_2) = 81000 (should be Q_{100} unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 373.6 ft. Flow angle at bridge = 15 ° Abut. Skew = 0 ° Effective Skew = 15 °
 Width (W_2) iteration = _____

Avg. flow depth at bridge, y_2 iteration = _____
 Corrected channel width at bridge Section = W_2 times cos of flow angle = 331.21 ft* $q_2 = Q_2/W_2 = \underline{242.4}$ ft²/s

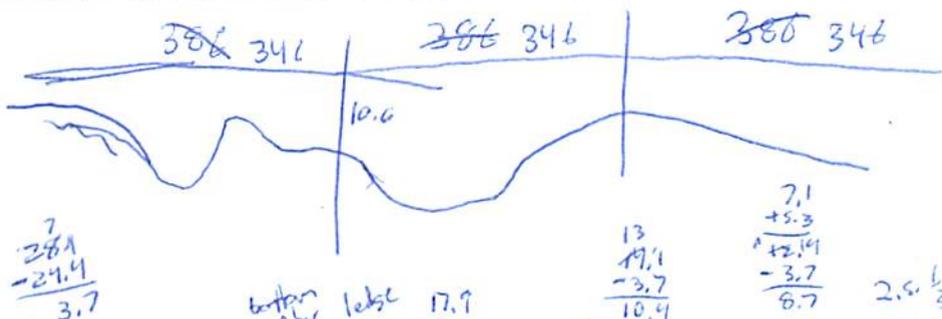
Bridge Vel, $V_2 = \underline{11}$ ft/s Final $y_2 = q_2/V_2 = \underline{21.9}$ ft $\Delta h = \underline{2.5}$ ft

Average main channel depth at approach section, $y_1 = \Delta h + y_2 = \underline{24.4}$ ft

* NOTE: repeat above calculations until y_2 changes by less than 0.2 Effective pier width = $L \sin(q) + a \cos(q)$

If y_2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0-5.0 ft
 Low Steel Elev. = 22.5 ft
 n (Channel) = 0.033
 n (LOB) = 0.050
 n (ROB) = 0.080
 Pier Width = 2.2 ft
 Pier Length = 2.3 ft
 # Piers for 100 yr = 4



CONTRACTION SCOUR

Width of main channel at approach section $W_1 = \underline{346}$ ft
 Width of left overbank flow at approach, $W_{lob} = \underline{346}$ ft Average left overbank flow depth, $y_{lob} = \underline{10.6}$ ft
 Width of right overbank flow at approach, $W_{rob} = \underline{346}$ ft Average right overbank flow depth, $y_{rob} = \underline{10.0}$ ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x = \underline{7.77}$ From Figure 9 W_2 (effective) = 325.4 ft $y_{cs} = \underline{8.6}$ ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material $D_{50} = \underline{\hspace{2cm}}$ ft Average approach velocity, $V_1 = Q_{100}/(y_1 W_1) = \underline{\hspace{2cm}}$ ft/s

Critical approach velocity, $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} = \underline{\hspace{2cm}}$ ft/s

If $V_1 < V_c$ and $D_{50} > 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 = \underline{\hspace{2cm}}$ ft If $D_{50} > D_{c50}$, $\chi = 0.0$

Otherwise, $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 = \underline{\hspace{2cm}}$ From Figure 10, $y_{cs} = \underline{\hspace{2cm}}$ ft

PIER SCOUR CALCULATIONS

L/a ratio = 1.14 Correction factor for flow angle of attack (from Table 1), $K_2 = \underline{1}$
 Froude # at bridge = 0.41 Using pier width a on Figure 11, $\xi = \underline{8.6}$ Pier scour $y_{ps} = \underline{7.5}$ ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, $y_{aLT} = \underline{9.9}$ ft right abutment, $y_{aRT} = \underline{10.0}$ ft
 Shape coefficient $K_1 = 1.00$ for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
 Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} = \underline{21.3}$ and $\psi_{RT} = \underline{21.3}$
 Left abutment scour, $y_{as} = \psi_{LT}(K_1/0.55) = \underline{21.3}$ ft Right abutment scour $y_{as} = \psi_{RT}(K_1/0.55) = \underline{21.3}$ ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCSNEW

PRGM: Pier

PRGM: Abutment

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 34246111 Date 6/2/12 Initials Lat Region (A B C D) D
 Site _____ Location nr Wolf ck Colony, NW of Mennr
 $Q_{500} =$ 129000 by: drainage area ratio _____ flood freq. anal. _____ regional regression eq. X
 Bridge discharge (Q_2) = 84936 (should be Q_{500} unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 346 ft. Flow angle at bridge = 15 ° Abut. Skew = 0 ° Effective Skew = 15 °
 Width (W_2) iteration = _____

Avg. flow depth at bridge, y_2 iteration = _____

Corrected channel width at bridge Section = W_2 times cos of flow angle = 334.21 ft* $q_2 = Q_2/W_2 =$ 254.1 ft²/s

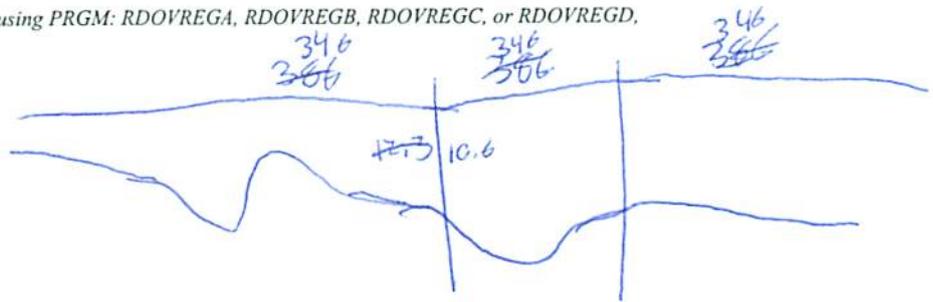
Bridge Vel, $V_2 =$ 11.3 ft/s Final $y_2 = q_2/V_2 =$ 22.5 ft $\Delta h =$ 2.6 ft

Average main channel depth at approach section, $y_1 = \Delta h + y_2 =$ 25.1 ft

* NOTE: repeat above calculations until y_2 changes by less than 0.2 Effective pier width = $L \sin(q) + a \cos(q)$

If y_2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0-5.0 ft
 Low Steel Elev. = 22.5 ft
 n (Channel) = 0.033
 n (LOB) = 0.050
 n (ROB) = 0.030
 Pier Width = 2.2 ft
 Pier Length = 2.5 ft
 # Piers for 500 yr = 4



CONTRACTION SCOUR

Width of main channel at approach section $W_1 =$ 346 ft
 Width of left overbank flow at approach, $W_{lob} =$ 346 ft Average left overbank flow depth, $y_{lob} =$ 10.6 ft
 Width of right overbank flow at approach, $W_{rob} =$ 346 ft Average right overbank flow depth, $y_{rob} =$ 10.7 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$ 8.43 From Figure 9 W_2 (effective) = 325.4 ft $y_{cs} =$ 9.3 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material $D_{50} =$ _____ ft Average approach velocity, $V_1 = Q_{500}/(y_1 W_1) =$ _____ ft/s

Critical approach velocity, $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$ _____ ft/s

If $V_1 < V_c$ and $D_{50} \geq 0.2$ ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1)^{7/6} =$ _____ ft If $D_{50} \geq D_{c50}$, $\chi = 0.0$

Otherwise, $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$ _____ From Figure 10, $y_{cs} =$ ✓ ft

PIER SCOUR CALCULATIONS

L/a ratio = 1.14 Correction factor for flow angle of attack (from Table 1), $K_2 =$ 1
 Froude # at bridge = 0.42 Using pier width a on Figure 11, $\xi =$ 8.6 Pier scour $y_{ps} =$ 7.6 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, $y_{aLT} =$ 10.6 ft right abutment, $y_{aRT} =$ 10.7 ft
 Shape coefficient $K_1 =$ 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through
 Using values for y_{aLT} and y_{aRT} on figure 12, $\psi_{LT} =$ 21.8 and $\psi_{RT} =$ 21.9
 Left abutment scour, $y_{as} = \psi_{LT}(K_1/0.55) =$ 21.8 ft Right abutment scour $y_{as} = \psi_{RT}(K_1/0.55) =$ 21.9 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCSNEW

PRGM: Pier

PRGM: Abutment

43.21355

16529.76



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Route Colony RD Stream James River MRM _____ Date 6/7/12 Initials Pat
 Bridge Structure No. 3424611 Location nr Wolf Ck colony NW of Menno
 GPS coordinates: N 43° 20' 37.0" taken from: USL abutment centerline of ↑ MRM end _____
W 97° 57' 33.4" Datum of coordinates: WGS84 NAD27 _____
 Drainage area = 18364.39 sq. mi.
 The average bottom of the main channel was 28.1 ft below top of guardrail at a point 183 ft from left abutment.
 Method used to determine flood flows: ___ Freq. Anal. ___ drainage area ratio regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q ₁₀₀ = <u>81000</u>			Q ₅₀₀ = <u>129000</u>		
Estimated flow passing through bridge	<u>81000</u>			<u>84936</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>44064</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping			<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>
Chance of Pressure flow	<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>

5/26
 2 | 1640
 5 | 6550
 10 | 19500
 25 | 47500
 50 | 81000
 100 | 129000
 500 | 318000

Riprap at abutments? Yes ___ No ___ Marginal
 Evidence of past Scour? Yes ___ No ___ Don't know *Pier contraction*
 Debris Potential? ___ High ___ Med Low

Does scour countermeasure(s) appear to have been designed?
 Riprap Yes ___ No ___ Don't know ___ NA *rose quartz*
 Spur Dike ___ Yes No ___ Don't know ___ NA
 Other ___ Yes No ___ Don't know ___ NA

Bed Material Classification Based on Median Particle Size (D₅₀)

Material Silt/Clay Sand ___ Gravel ___ Cobbles ___ Boulders ___
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos
 1) main channel
 2) piers
 3-4) right abutment
 4-7) left abutment
 8) right abutment
 9) pier Scour
 10) right CB
 11) main channel
 12) left CB
 13) lateral instability

Summary of Results

	Q ₁₀₀ ⁵⁰	Q ₅₀₀ ¹⁰⁰
Bridge flow evaluated	<u>81000</u>	<u>84936</u>
Flow depth at left abutment (yaLT), in feet	<u>9.9</u>	<u>10.6</u>
Flow depth at right abutment (yaRT), in feet	<u>10.0</u>	<u>10.7</u>
Contraction scour depth (yca), in feet	<u>8.6</u>	<u>9.3</u>
Pier scour depth (yca), in feet	<u>7.5</u>	<u>7.6</u>
Left abutment scour depth (yca), in feet	<u>21.3</u>	<u>21.8</u>
Right abutment scour depth (yca), in feet	<u>21.3</u>	<u>21.9</u>
Flow angle of attack	<u>15</u>	<u>15</u>

See Comments/Diagram for justification where required