

**SCOUR ANALYSIS AND REPORTING FORM**

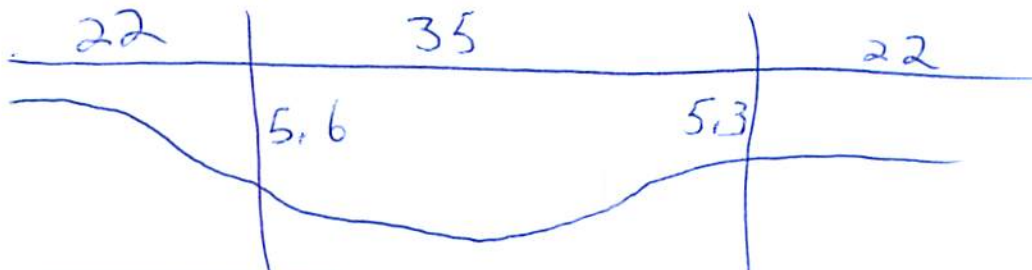
Bridge Structure No. 36100136 Date 10/14/11 Initials CW Region (A/B/C/D) \_\_\_\_\_  
 Site \_\_\_\_\_ Location ~2 mi W + ~2.5 mi S of Cactus Flatts on 207 Ave  
 $Q_{100} =$  704 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. \_\_\_\_\_  
 Bridge discharge ( $Q_2$ ) = 704 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 22 ft. Flow angle at bridge = 3 ° Abut. Skew = 0 ° Effective Skew = 3 °  
 Width ( $W_2$ ) iteration = 22  
 Avg. flow depth at bridge,  $y_2$  iteration = 6.6 → vert wall  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 21.97 ft\*  $q_2 = Q_2/W_2 =$  32 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  4.8 ft/s Final  $y_2 = q_2/V_2 =$  6.6 ft  $\Delta h =$  0.5 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  7.1 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(\alpha) + a \cos(\alpha)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = \_\_\_\_\_ ft  
 Low Steel Elev. = 6.6 ft  
 n (Channel) = 0.035  
 n (LOB) = ~~0.050~~ 0.050  
 n (ROB) = ~~0.06~~ 0.050  
 Pier Width = 0.85 ft  
 Pier Length = 27.0 ft  
 # Piers for 100 yr = 1.0 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  35 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  22 ft Average left overbank flow depth,  $y_{lob} =$  5.6 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  22 ft Average right overbank flow depth,  $y_{rob} =$  5.3 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  11.33 From Figure 9  $W_2$  (effective) = 21.1 ft  $y_{cs} =$  12.4 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} >= 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} >= D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 31.8 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1.3  
 Froude # at bridge = 0.33 Using pier width a on Figure 11,  $\xi =$  4.1 Pier scour  $y_{ps} =$  4.6 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  5.6 ft right abutment,  $y_{aRT} =$  5.3 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  16.1 and  $\psi_{RT} =$  15.6  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) =$  24.0 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) =$  23.2 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pier

PGRM: Abutment



**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 36100136 Date 10/14/11 Initials Cur Region (A B C D) B  
 Site \_\_\_\_\_ Location ~2.5 mi S + 2 mi W of Cactus Flatts on 207 Ave  
 $Q_{500} =$  1220 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. \_\_\_\_\_  
 Bridge discharge ( $Q_2$ ) = 696 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 22 ft. Flow angle at bridge = 3 ° Abut. Skew = 0 ° Effective Skew = 3 °  
 Width ( $W_2$ ) iteration = 22

Avg. flow depth at bridge,  $y_2$  iteration = 8.9 > 6.6

Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 21.97 ft\*  $q_2 = Q_2/W_2 =$  31.7 ft<sup>2</sup>/s

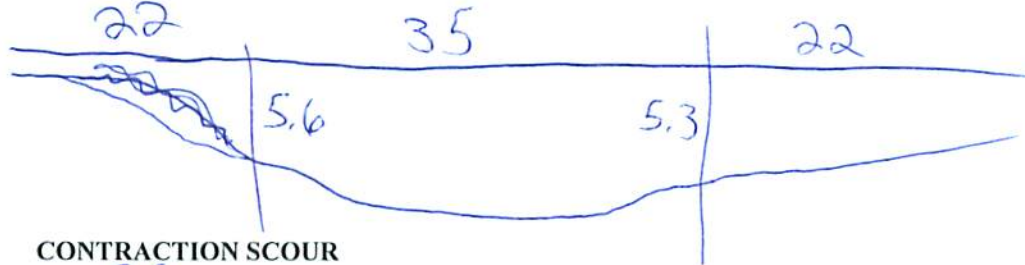
Bridge Vel,  $V_2 =$  4.8 ft/s Final  $y_2 = q_2/V_2 =$  6.6 ft  $\Delta h =$  0.5 ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  7.1 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = \_\_\_\_\_ ft  
 Low Steel Elev. = 6.6 ft  
 $n$  (Channel) = 0.035  
 $n$  (LOB) = 0.050  
 $n$  (ROB) = 0.050  
 Pier Width = 0.85 ft  
 Pier Length = 27 ft  
 # Piers for 500 yr = 1 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  35 ft

Width of left overbank flow at approach,  $W_{lob} =$  22 ft

Average left overbank flow depth,  $y_{lob} =$  5.6 ft

Width of right overbank flow at approach,  $W_{rob} =$  22 ft

Average right overbank flow depth,  $y_{rob} =$  5.3 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  11.33 From Figure 9  $W_2$  (effective) = 21.1 ft  $y_{cs} =$  12.4 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006(q_2/y_1)^{7/6} =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 31.8

Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1.3

Froude # at bridge = 0.33

Using pier width a on Figure 11,  $\xi =$  4.1 Pier scour  $y_{ps} =$  4.6 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{alT} =$  5.6 ft right abutment,  $y_{arT} =$  5.3 ft

Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through

Using values for  $y_{alT}$  and  $y_{arT}$  on figure 12,  $\psi_{LT} =$  161 and  $\psi_{RT} =$  15.6

Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  24.0 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  23.2 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Pie

PRGM: Abutment

Route 207 Ave Stream Big Buffalo ck MRM \_\_\_\_\_ Date 10/14/11 Initials EW  
 Bridge Structure No. 36100136 Location ~2mi W + 2.5mi S of Cactus Flats on 207 Ave  
 GPS coordinates: N 43° 49' 40.0" taken from: USL abutment  centerline of  $\uparrow$  MRM end \_\_\_\_\_  
W 101° 56' 23.0" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 3.00 sq. mi.  
 The average bottom of the main channel was 10.5 ft below top of guardrail at a point 5.0 ft from left abutment.  
 Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio \_\_\_ regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = <u>704</u>			Q <sub>500</sub> = <u>1220</u>		
Estimated flow passing through bridge	<u>704</u>			<u>696</u>		
Estimated road overflow & overtopping				<u>524</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Chance of Pressure flow			<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

Riprap at abutments? \_\_\_ Yes  No \_\_\_ Marginal  
 Evidence of past Scour? \_\_\_ Yes  No \_\_\_ Don't know  
 Debris Potential? \_\_\_ High  Med \_\_\_ Low

Does scour countermeasure(s) appear to have been designed?

Riprap \_\_\_ Yes \_\_\_ No \_\_\_ Don't know  NA  
 Spur Dike \_\_\_ Yes \_\_\_ No \_\_\_ Don't know  NA  
 Other \_\_\_ Yes \_\_\_ No \_\_\_ Don't know  NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay  Sand \_\_\_ Gravel \_\_\_ Cobbles \_\_\_ Boulders \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

10/4/11  

2	46.6	Photos	14- R. Abut		
5	137			15- US Face	
10	236				16- Woody debris
25	388				
50	534				
100	704				
500	1220				

2109- 1D  
 10- US  
 11- USRB  
 12- USLB  
 13- L. Abut

Summary of Results

	Q100	Q500
Bridge flow evaluated	<u>704</u>	<u>696</u>
Flow depth at left abutment (yaLT), in feet	<u>5.6</u>	<u>5.6</u>
Flow depth at right abutment (yaRT), in feet	<u>5.3</u>	<u>5.3</u>
Contraction scour depth (yes), in feet	<u>12.4</u>	<u>12.4</u>
Pier scour depth (yps), in feet	<u>4.6</u>	<u>4.6</u>
Left abutment scour depth (yas), in feet	<u>24.0</u>	<u>24.0</u>
Right abutment scour depth (yas), in feet	<u>23.2</u>	<u>23.2</u>
Flow angle of attack	<u>3°</u>	<u>3°</u>

See Comments/Diagram for justification where required