

OK RT check

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 39054040 Date 7/24/12 Initials RT Region (A B C D) B  
 Site \_\_\_\_\_ Location Just east of Bancroft on 200 St  
 $Q_{100} = Q_{50} 1620$  by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 1620 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 35 ft. Flow angle at bridge = 10 ° Abut. Skew = 0 ° Effective Skew = 10 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_  
 Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 34.77 ft\*  $q_2 = Q_2/W_2 = 47$  ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 = 4.9$  ft/s Final  $y_2 = q_2/V_2 = 9.7$  ft  $\Delta h = 0.5$  ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = 10.2$  ft  
 \*NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 3.1 ft *channel dry*  
 Low Steel Elev. = 10.6 ft  
 $n$  (Channel) = 0.035  
 $n$  (LOB) = 0.030  
 $n$  (ROB) = 0.030  
 Pier Width = \_\_\_\_\_ ft  
 Pier Length = \_\_\_\_\_ ft  
 # Piers for 100 yr = 2 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 = 66$  ft  
 Width of left overbank flow at approach,  $W_{lob} = 35$  ft Average left overbank flow depth,  $y_{lob} = 2.7$  ft  
 Width of right overbank flow at approach,  $W_{rob} = 35$  ft Average right overbank flow depth,  $y_{rob} = 2.7$  ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x = 11.97$  From Figure 9  $W_2$  (effective) = 34.5 ft  $y_{cs} = 13$  ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2 / y_1)^{7/6} =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = \_\_\_\_\_ Correction factor for flow angle of attack (from Table 1),  $K_2 =$  \_\_\_\_\_  
 Froude # at bridge = \_\_\_\_\_ Using pier width  $a$  on Figure 11,  $\xi =$  \_\_\_\_\_ Pier scour  $y_{ps} =$  \_\_\_\_\_ ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} = 2.7$  ft right abutment,  $y_{aRT} = 2.7$  ft  
 Shape coefficient  $K_1 = 1.00$  for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = 11$  and  $\psi_{RT} = 11$   
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) = 16.4$  ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) = 16.4$  ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"  
 PGRM: Contract  
 PGRM: CWCSNEW  
 PGRM: Pier  
 PGRM: Abutment

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 39054040 Date 7/24/12 Initials PAT Region (A B C D)
Site Location Just E of Bancroft on 200 St
Q500 = 4500 2180 by: drainage area ratio flood freq. anal. regional regression eq. X
Bridge discharge (Q2) = 1731 (should be Q500 unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 35 ft. Flow angle at bridge = 10 degrees Abut. Skew = 0 degrees Effective Skew = 10 degrees

Width (W2) iteration =

Avg. flow depth at bridge, y2 iteration =

Corrected channel width at bridge Section = W2 times cos of flow angle = 34.47 ft\* q2 = Q2/W2 = 50.2 ft^2/s

Bridge Vel, V2 = 3 ft/s Final y2 = q2/V2 = 10 ft Dh = 0.5 ft

Average main channel depth at approach section, y1 = Dh + y2 = 10.5 ft

\* NOTE: repeat above calculations until y2 changes by less than 0.2 Effective pier width = L sin(q) + a cos(q)

If y2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD,

Water Surface Elev. = 31.1 ft
Low Steel Elev. = 10 ft
n (Channel) = 0.035
n (LOB) = 0.030
n (ROB) = 0.030
Pier Width = 0 ft
Pier Length = C ft
# Piers for 500 yr = C ft



CONTRACTION SCOUR

Width of main channel at approach section W1 = 66 ft

Width of left overbank flow at approach, Wlob = 35 ft

Average left overbank flow depth, ylob = 3.0 ft

Width of right overbank flow at approach, Wrob = 35 ft

Average right overbank flow depth, yrob = 3.0 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

x = 12.69 From Figure 9 W2 (effective) = 34.5 ft ycs = 13.7 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material D50 = ft Average approach velocity, V1 = Q500/(y1W1) = ft/s

Critical approach velocity, Vc = 11.17y1^1/6 D50^1/3 = ft/s

If V1 < Vc and D50 >= 0.2 ft, use clear water equation below, otherwise use live bed scour equation above.

Dc50 = 0.0006(q2/y1^7/6)^3 = ft If D50 >= Dc50, chi = 0.0

Otherwise, chi = 0.122y1[q2/(D50^1/3 y1^7/6)]^6/7 - y1 = From Figure 10, ycs = ft

PIER SCOUR CALCULATIONS

L/a ratio =

Correction factor for flow angle of attack (from Table 1), K2 =

Froude # at bridge =

Using pier width a on Figure 11, xi = Pier scour yps = ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, yalT = 3.0 ft right abutment, yarT = 3.0 ft

Shape coefficient K1 = 1.00 for vertical-wall, 0.82 for vertical-wall-with-wingwalls, 0.55 for spill-through

Using values for yalT and yarT on figure 12, psiLT = 11.5 and psiRT = 11.5

Left abutment scour, yas = psiLT(K1/0.55) = 17.2 ft Right abutment scour yas = psiRT(K1/0.55) = 17.2 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCSNEW

PGRM: Pic

PGRM: Abutment



97.7H263  
44.4B436

440 29' 3.696"  
97 44' 39.3468"

440 29' 3.696"  
97 44' 39.3468"

Handwritten notes at the bottom of the page, including "300 ft" and "Bromine" written upside down.

Route 200 St Stream Redstone Ck MRM \_\_\_\_\_ Date 7/24/12 Initials Pat  
 Bridge Structure No. 39054040 Location Just E of Banaroff on 200 St  
 GPS coordinates: N 44° 29' 3.9" taken from: USL abutment X centerline of ↑ MRM end \_\_\_\_\_  
N 97° 44' 39.4" Datum of coordinates: WGS84 X NAD27 \_\_\_\_\_

Drainage area = 39.23 sq. mi.  
 The average bottom of the main channel was 14.4 ft below top of guardrail at a point 12 ft from left abutment.  
 Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio X regional regression equations.

**MISCELLANEOUS CONSIDERATIONS**

Flows	Q <sub>100</sub> = <u>Q<sub>50</sub> 1620</u>			Q <sub>500</sub> = <u>Q<sub>100</sub> 2180</u>		
Estimated flow passing through bridge				1731		
Estimated road overflow & overtopping	0			449		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<u>X</u>		<u>X</u>		
Chance of Pressure flow	<u>X</u>			<u>X</u>		
Armored appearance to channel		<u>X</u>			<u>X</u>	
Lateral instability of channel		<u>X</u>			<u>X</u>	

8/24  

2	232
5	738
10	1300
25	2340
50	3340
100	4570
500	8330

Riprap at abutments? \_\_\_ Yes X No \_\_\_ Marginal  
 Evidence of past Scour? X Yes \_\_\_ No \_\_\_ Don't know  
 Debris Potential? \_\_\_ High \_\_\_ Med X Low

*4ft of elevation drop under bridge-construction abutments submerged*

713  

2	126
5	384
10	662
25	1150
50	1620
100	2180
500	3850

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_ Yes X No \_\_\_ Don't know \_\_\_ NA  
 Spur Dike \_\_\_ Yes X No \_\_\_ Don't know \_\_\_ NA  
 Other \_\_\_ Yes X No X Don't know \_\_\_ NA

*wood beam at bottom of abutments*

**Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)**

Material Silt/Clay X Sand \_\_\_ Gravel \_\_\_ Cobbles \_\_\_ Boulders \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos  
 1) left ab  
 2) main channel  
 3) right ab  
 4-5) right abutment  
 6-7) left abutment  
 8) main channel

**Summary of Results**

	Q <sub>100</sub> <u>Q<sub>50</sub></u>	Q <sub>500</sub> <u>Q<sub>100</sub></u>
Bridge flow evaluated	1620	1731
Flow depth at left abutment (yaLT), in feet	2.7	3.0
Flow depth at right abutment (yaRT), in feet	2.7	3.0
Contraction scour depth (y <sub>cs</sub> ), in feet	13.0	13.7
Pier scour depth (y <sub>ps</sub> ), in feet	NA	NA
Left abutment scour depth (y <sub>as</sub> ), in feet	16.4	17.2
Right abutment scour depth (y <sub>as</sub> ), in feet	16.4	17.2
Flow angle of attack	10	10

See Comments/Diagram for justification where required