

OK RT

### SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 39353040 Date 5-17-12 Initials CW/RAT Region (A B C D) B  
 Site \_\_\_\_\_ Location 2.1 mi E of Badger on 200 St  
 $Q_{100} =$  55,71500 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. \_\_\_\_\_  
 Bridge discharge ( $Q_2$ ) = 55,71500 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 55 ft. Flow angle at bridge = 25 ° Abut. Skew = 0 ° Effective Skew = 25 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_  
 Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 49.85 ft\*  $q_2 = Q_2/W_2 =$  30.1 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  3.9 ft/s Final  $y_2 = q_2/V_2 =$  4.577 ft  $\Delta h =$  0.3 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  10.8 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2  
 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0.2 ft  
 Low Steel Elev. = 8 ft  
 n (Channel) = 0.033  
 n (LOB) = 0.035  
 n (ROB) = 0.033  
 Pier Width = 1.6 ft  
 Pier Length = 1.6 ft  
 # Piers for 100 yr = 2 ft

*Stream Stats seems wrong as there are high water marks above 1.5. Used crest of road*

#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 =$  110 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  55 ft Average left overbank flow depth,  $y_{lob} =$  8.4 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  55 ft Average right overbank flow depth,  $y_{rob} =$  9.2 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  65.75 From Figure 9  $W_2$  (effective) = 46.7 ft  $y_{cs} =$  11.2 ft

~~Clean Water Contraction Scour (use if bed material is larger than small cobbles)~~  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clean water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2/y_1)^{7/6} =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

#### PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.25 Using pier width a on Figure 11,  $\xi =$  6.7 Pier scour  $y_{ps} =$  5.5 ft

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} =$  4.4 ft right abutment,  $y_{aRT} =$  9.2 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  20.1 and  $\psi_{RT} =$  20.7  
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  36.5 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  37.7 ft

*Handwritten calculations:*  
 $4.4 \times 2.1 = 9.24$   
 $9.24 / 2.1 = 4.4$

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pier

PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 39353040 Date \_\_\_\_\_ Initials \_\_\_\_\_ Region (A B C D)  
 Site \_\_\_\_\_ Location 2.1 mi E of Badger on 200 St  
 $Q_{500} =$  82.3 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. \_\_\_\_\_  
 Bridge discharge ( $Q_2$ ) = 82.3 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 35 ft. Flow angle at bridge = 25 ° Abut. Skew = 0 ° Effective Skew = 25 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_

Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 49.85 ft\*  $q_2 = Q_2/W_2 =$  1.7 ft<sup>2</sup>/s

Bridge Vel,  $V_2 =$  0.9 ft/s Final  $y_2 = q_2/V_2 =$  1.8 ft  $\Delta h =$  0 ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  1.8 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0.4 ft  
 Low Steel Elev. = 0 ft  
 n (Channel) = 0.033  
 n (LOB) = 0.035  
 n (ROB) = 0.033  
 Pier Width = 1.6 ft  
 Pier Length = 1.6 ft  
 # Piers for 500 yr = 2 ft

**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  \_\_\_\_\_ ft  
 Width of left overbank flow at approach,  $W_{lob} =$  \_\_\_\_\_ ft Average left overbank flow depth,  $y_{lob} =$  \_\_\_\_\_ ft  
 Width of right overbank flow at approach,  $W_{rob} =$  \_\_\_\_\_ ft Average right overbank flow depth,  $y_{rob} =$  \_\_\_\_\_ ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  \_\_\_\_\_ From Figure 9  $W_2$  (effective) = \_\_\_\_\_ ft  $y_{cs} =$  \_\_\_\_\_ ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006(q_2/y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = \_\_\_\_\_ Using pier width a on Figure 11,  $\xi =$  \_\_\_\_\_ Pier scour  $y_{ps} =$  \_\_\_\_\_ ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  \_\_\_\_\_ ft right abutment,  $y_{aRT} =$  \_\_\_\_\_ ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  \_\_\_\_\_ and  $\psi_{RT} =$  \_\_\_\_\_  
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  \_\_\_\_\_ ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  \_\_\_\_\_ ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCSNEW

PRGM: Pie

PRGM: Abutment

Route 200 St Stream MRM Date \_\_\_\_\_ Initials \_\_\_\_\_  
 Bridge Structure No. 39353040 Location 2.1 mi. E of Badger on 200 St  
 GPS coordinates: N 44° 29' 06.9" taken from: USL abutment \_\_\_\_\_ centerline of  $\uparrow$  MRM end \_\_\_\_\_  
W 97° 04' 35.7" Datum of coordinates: WGS84 \_\_\_\_\_ NAD27 \_\_\_\_\_

Drainage area = 50.4 sq. mi.  
 The average bottom of the main channel was 11.3 ft below top of guardrail at a point 15 ft from left abutment.  
 Method used to determine flood flows: \_\_\_\_\_ Freq. Anal. \_\_\_\_\_ drainage area ratio \_\_\_\_\_ regional regression equations.

MISCELLANEOUS CONSIDERATIONS Crest of Road 5/17

Flows	$Q_{100} = Q_{max\ scour}$			$Q_{500} =$		
Estimated flow passing through bridge	<u>1500</u>					
Estimated road overflow & overtopping	<u>0</u>					
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping	<input checked="" type="checkbox"/>					
Chance of Pressure flow	<input checked="" type="checkbox"/>					
Armored appearance to channel		<input checked="" type="checkbox"/>				
Lateral instability of channel		<input checked="" type="checkbox"/>				

2 4.61  
 5 13.6  
 10 21.8  
 25 31.4  
 50 44.7  
 100 55.7  
 500 82.3

Riprap at abutments? \_\_\_\_\_ Yes  No \_\_\_\_\_ Marginal  
 Evidence of past Scour?  Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know Abutments  
 Debris Potential? \_\_\_\_\_ High \_\_\_\_\_ Med  Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know  NA  
 Spur Dike \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know  NA  
 Other \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know  NA

Bed Material Classification Based on Median Particle Size ( $D_{50}$ )  
 Material Silt/Clay  Sand \_\_\_\_\_ Gravel \_\_\_\_\_ Cobbles \_\_\_\_\_ Boulders \_\_\_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos  
 2302 Str. no.  
 2303 approach from bridge  
 2304 ROB from bridge  
 2305 LOB from bridge  
 2306 erosion at abutment toe under bridge  
 2307 erosion at abutment toe under bridge  
 2308 bridge section from left abutment  
 2309 bridge section from ROB

Summary of Results

	$Q_{100} Q_{max\ scour}$	$Q_{500}$
Bridge flow evaluated		
Flow depth at left abutment (yaLT), in feet	<u>8.4</u>	
Flow depth at right abutment (yaRT), in feet	<u>9.2</u>	
Contraction scour depth (yca), in feet	<u>11.724</u>	
Pier scour depth (yca), in feet	<u>5.5</u>	
Left abutment scour depth (yca), in feet	<u>36.5</u>	
Right abutment scour depth (yca), in feet	<u>37.7</u>	
Flow angle of attack	<u>25°</u>	

See Comments/Diagram for justification where required