

DUP ok-Rat

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 41093081 Date 9-18-12 Initials RFT Region (A)BCD  
 Site \_\_\_\_\_ Location In Spearfish on Grant St between Meier & 3rd St  
 $Q_{100} =$  9250 by: drainage area ratio  flood freq. anal. \_\_\_\_\_ regional regression eq. \_\_\_\_\_  
 Bridge discharge ( $Q_2$ ) = 7859 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

↑ estimated  $Q_{max\ scour}$

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 80 ft. Flow angle at bridge = 5 ° Abut. Skew = 0 ° Effective Skew = 5 °  
 Width ( $W_2$ ) iteration = 80

Avg. flow depth at bridge,  $y_2$  iteration = 8.9

Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 79.7 ft\*  $q_2 = Q_2/W_2 =$  98.6 ft<sup>2</sup>/s

Bridge Vel,  $V_2 =$  11.1 ft/s Final  $y_2 = q_2/V_2 =$  8.9 ft  $\Delta h =$  2.5 ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  11.4 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

$y_{max\ scour} \approx 8.9$ , flow overtops rt bank above this

Water Surface Elev. = 0.1 ft

Low Steel Elev. = 7.6 ft

n (Channel) = 0.045 straight, flat, rocky

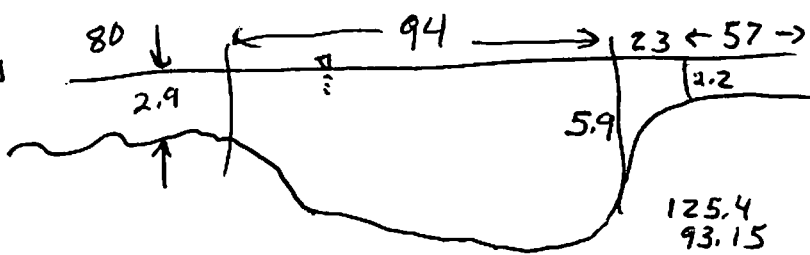
n (LOB) = 0.095 wooded

n (ROB) = 0.045 grass & trees

Pier Width = NA ft

Pier Length = NA ft

# Piers for 100 yr = 0



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  94 ft

Width of left overbank flow at approach,  $W_{lob} =$  80 ft Average left overbank flow depth,  $y_{lob} =$  2.9 ft

Width of right overbank flow at approach,  $W_{rob} =$  80 ft Average right overbank flow depth,  $y_{rob} =$  2.73 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  3.66 From Figure 9  $W_2$  (effective) = 79.7 ft  $y_{cs} =$  4.3 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  0.2 ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  2.71 ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  9.8 ft/s

If  $V_1 < V_c$  and  $D_{50} >= 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1)^{7/6} =$  .115 ft

If  $D_{50} >= D_{c50}$ ,  $\chi =$  0.0

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  0 ft

**PIER SCOUR CALCULATIONS**

L/a ratio = \_\_\_\_\_

Correction factor for flow angle of attack (from Table 1),  $K_2 =$  \_\_\_\_\_

Froude # at bridge = \_\_\_\_\_

Using pier width  $a$  on Figure 11,  $\xi =$  \_\_\_\_\_ Pier scour  $y_{ps} =$  \_\_\_\_\_ ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  2.9 ft right abutment,  $y_{aRT} =$  2.73 ft

Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through

Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  11.3 and  $\psi_{RT} =$  11.1

Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  11.3 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  11.1 ft

7.69  
 PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"  
 PGRM: Contract  
 PGRM: CWCSNEW  
 PGRM: Pier  
 PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 41093081 Date \_\_\_\_\_ Initials \_\_\_\_\_ Region (A)BCD  
 Site \_\_\_\_\_ Location \_\_\_\_\_

$Q_{500} =$ 23900 $$ by: drainage area ratio  flood freq. anal. \_\_\_\_\_ regional regression eq. \_\_\_\_\_  
 Bridge discharge ( $Q_2$ ) = 7859 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = \_\_\_\_\_ ft. Flow angle at bridge = \_\_\_\_\_ ° Abut. Skew = \_\_\_\_\_ ° Effective Skew = \_\_\_\_\_ °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_

Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_

Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = \_\_\_\_\_ ft\*  $q_2 = Q_2/W_2 =$  \_\_\_\_\_ ft<sup>2</sup>/s

Bridge Vel,  $V_2 =$  \_\_\_\_\_ ft/s Final  $y_2 = q_2/V_2 =$  \_\_\_\_\_ ft  $\Delta h =$  \_\_\_\_\_ ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  \_\_\_\_\_ ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

Water Surface Elev. = 0.1 ft  
 Low Steel Elev. = 7.16 ft  
 n (Channel) = .045  
 n (LOB) = .075  
 n (ROB) = .045  
 Pier Width = NA ft  
 Pier Length = NA ft  
 # Piers for 500 yr = 0 ft

See  $Q_{100}$  calcs

**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  \_\_\_\_\_ ft  
 Width of left overbank flow at approach,  $W_{lob} =$  \_\_\_\_\_ ft Average left overbank flow depth,  $y_{lob} =$  \_\_\_\_\_ ft  
 Width of right overbank flow at approach,  $W_{rob} =$  \_\_\_\_\_ ft Average right overbank flow depth,  $y_{rob} =$  \_\_\_\_\_ ft

**Live Bed Contraction Scour** (use if bed material is small cobbles or finer)

$x =$  \_\_\_\_\_ From Figure 9  $W_2$  (effective) = \_\_\_\_\_ ft  $y_{cs} =$  \_\_\_\_\_ ft

**Clear Water Contraction Scour** (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006(q_2/y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{5/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

PRGM: Contract

PRGM: CWCNEW

**PIER SCOUR CALCULATIONS**

L/a ratio = \_\_\_\_\_ Correction factor for flow angle of attack (from Table 1),  $K_2 =$  \_\_\_\_\_  
 Froude # at bridge = \_\_\_\_\_ Using pier width NA on Figure 11,  $\xi =$  \_\_\_\_\_ Pier scour  $y_{ps} =$  \_\_\_\_\_ ft

PRGM: Pie

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  \_\_\_\_\_ ft right abutment,  $y_{aRT} =$  \_\_\_\_\_ ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  \_\_\_\_\_ and  $\psi_{RT} =$  \_\_\_\_\_  
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  \_\_\_\_\_ ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  \_\_\_\_\_ ft

PRGM: Abutment

Route Grant St Stream Spearfish Ck MRM \_\_\_\_\_ Date 9-18-12 Initials RFT  
 Bridge Structure No. 41093081 Location in Spearfish, on Grant St between Meier & 3rd  
 GPS coordinates: N 44° 29.233' taken from: 'USL abutment  centerline of fl MRM end \_\_\_\_\_  
W 103° 51.795' Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 164.98 sq. mi.  
 The average bottom of the main channel was 14.4 ft below top of guardrail at a point 32 ft from left abutment.  
 Method used to determine flood flows: \_\_\_\_\_ Freq. Anal.  drainage area ratio \_\_\_\_\_ regional regression equations.

**MISCELLANEOUS CONSIDERATIONS**

Flows	Q <sub>100</sub> = <u>9250</u>			Q <sub>500</sub> = <u>23900</u>		
Estimated flow passing through bridge	<u>7859</u>			<u>7859</u>		
Estimated road overflow & overtopping	<u>1391</u>			<u>16041</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>				<input checked="" type="checkbox"/>
Chance of Pressure flow	<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>		
Armored appearance to channel	<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>		
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

*road overflow likely for Q<sub>100</sub>*

Riprap at abutments?  Yes  No  Marginal  
 Evidence of past Scour?  Yes  No  Don't know *none obvious*  
 Debris Potential?  High  Med  Low *many trees, but no piers to catch debris*  
*riprap has been placed at both abutments, upstream, under bridge, and downstream*  
 Does scour countermeasure(s) appear to have been designed?  
 Riprap  Yes  No  Don't know  NA  
 Spur Dike  Yes  No  Don't know  NA  
 Other armored rt bank  Yes  No  Don't know  NA

**Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)**

Material Silt/Clay \_\_\_\_\_ Sand \_\_\_\_\_ Gravel  Cobbles  Boulders \_\_\_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250  
*low flow channel bottom is gravel & cobbles, assume CWCS*

Comments, Diagrams & orientation of digital photos  
*str. no. approach from bridge left about, under bridge*  
*LOB from bridge rt about, under bridge*  
*ROB from bridge*  
*bridge from near rt. about*  
*armored rt. bank upstream*

**Summary of Results**

	Q <sub>100</sub>	Q <sub>500</sub>
Bridge flow evaluated	<u>7859 = Q<sub>max</sub> scour</u>	
Flow depth at left abutment (yaLT), in feet	<u>2.9</u>	
Flow depth at right abutment (yaRT), in feet	<u>2.7</u>	
Contraction scour depth (y <sub>cs</sub> ), in feet	<u>4.3</u>	
Pier scour depth (y <sub>ps</sub> ), in feet	<u>NA</u>	<u>NA</u>
Left abutment scour depth (y <sub>as</sub> ), in feet	<u>11.3</u>	
Right abutment scour depth (y <sub>rs</sub> ), in feet	<u>11.1</u>	
Flow angle of attack	<u>5°</u>	

See Comments/Diagram for justification where required