

ok-Rat

SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 41126089 Date 9-18-12 Initials RFT Region (A B C D)
Site Location SE of Spearfish
Q100 = 2600 by: drainage area ratio flood freq. anal. regional regression eq.
Bridge discharge (Q2) = 2600 (should be Q100 unless there is a relief bridge, road overflow, or bridge overtopping)

Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 94 ft. Flow angle at bridge = 12 degrees Abut. Skew = 5 degrees Effective Skew = 7 degrees
Width (W2) iteration = 94 79 80
Avg. flow depth at bridge, y2 iteration = 4.5 4.9 4.9
Corrected channel width at bridge Section = W2 times cos of flow angle = 78.25 ft\* q2 = Q2/W2 = 33.2 ft^2/s
Bridge Vel, V2 = 6.8 ft/s Final y2 = q2/V2 = 4.9 ft Delta h = 0.9 ft
Average main channel depth at approach section, y1 = Delta h + y2 = 5.8 ft

\* NOTE: repeat above calculations until y2 changes by less than 0.2 Effective pier width = L sin(q) + a cos(q) y2 > 7.3 is abut, to abut.
If y2 is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.
road overflow begins approximately at y2 = 11.8 ft

Water Surface Elev. = dry ft
Low Steel Elev. = 10.0 ft
n (Channel) = .035
n (LOB) = .033
n (ROB) = .033
Pier Width = 1.0 ft
Pier Length = 36 ft
# Piers for 100 yr = 2



CONTRACTION SCOUR

Width of main channel at approach section W1 = 101 ft
Width of left overbank flow at approach, Wlob = 9 ft Average left overbank flow depth, ylob = 0.8 ft
Width of right overbank flow at approach, Wrob = 61 ft Average right overbank flow depth, yrob = 0.8 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

x = From Figure 9 W2 (effective) = ft ycs = ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material D50 = 0.2 ft Average approach velocity, V1 = Q100/(y1 W1) = 2.62 ft/s

Critical approach velocity, Vc = 11.17 y1^(1/6) D50^(1/3) = 8.76 ft/s

If V1 < Vc and D50 >= 0.2 ft, use clear water equation below, otherwise use live bed scour equation above.

Dc50 = 0.0006 (q2/y1^(7/6))^3 = .047 ft

If D50 >= Dc50, chi = 0.0

Otherwise, chi = 0.122 y1 [(q2/(D50^(1/3) y1^(7/6)))^(6/7) - y1 =

From Figure 10, ycs = 0 ft

PIER SCOUR CALCULATIONS

L/a ratio = 36

Correction factor for flow angle of attack (from Table 1), K2 = 1.6

Froude # at bridge = 0.54

Using pier width a on Figure 11, xi = 4.9 Pier scour yps = 7.1 ft

ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment, yalT = 0.8 ft right abutment, yarT = 0.8 ft

Shape coefficient K1 = 1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through

Using values for yalT and yarT on figure 12, psiLT = 3.5 and psiRT = 3.5

Left abutment scour, yas = psiLT (K1/0.55) = 3.5 ft Right abutment scour yas = psiRT (K1/0.55) = 3.5 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCSNEW

PGRM: Pier

PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 41126089 Date \_\_\_\_\_ Initials \_\_\_\_\_ Region (A)BCD  
 Site \_\_\_\_\_ Location SE of Spearfish  
 $Q_{500} =$  6770 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq.   
 Bridge discharge ( $Q_2$ ) = 6770 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

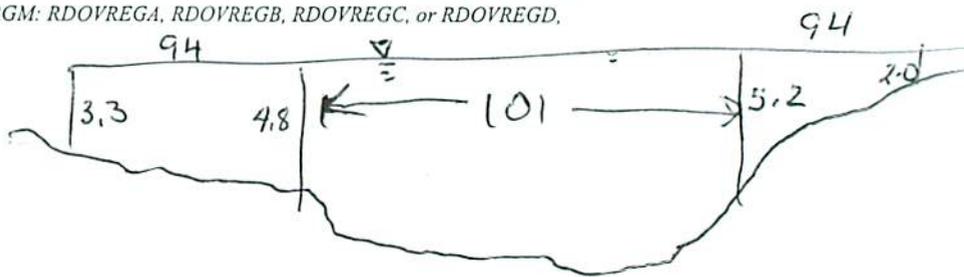
**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 94 ft. Flow angle at bridge = 12 ° Abut. Skew = 5 ° Effective Skew = 7 °  
 Width ( $W_2$ ) iteration = 94  $Q_{500}$  is about, to about.  
 Avg. flow depth at bridge,  $y_2$  iteration = 7.6  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 91.95 ft\*  $q_2 = Q_2/W_2 =$  73.6 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  9.7 ft/s Final  $y_2 = q_2/V_2 =$  7.6 ft  $\Delta h =$  1.9 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  9.5 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(\alpha) + a \cos(\alpha)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

Water Surface Elev. = dry ft  
 Low Steel Elev. = 10.0 ft  
 $n$  (Channel) = .035  
 $n$  (LOB) = .033  
 $n$  (ROB) = .033  
 Pier Width = 1.0 ft  
 Pier Length = 36 ft  
 # Piers for 500 yr = 2 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  101 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  94 ft Average left overbank flow depth,  $y_{lob} =$  4.05 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  94 ft Average right overbank flow depth,  $y_{rob} =$  3.55 ft  
3.6

PGRM: Contract

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  \_\_\_\_\_ From Figure 9  $W_2$  (effective) = \_\_\_\_\_ ft  $y_{cs} =$  \_\_\_\_\_ ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  0.2 ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  2.47 ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  9.51 ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 =$  .091 ft If  $D_{50} \geq D_{c50}$ ,  $\chi =$  0.0  
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  0 ft

PGRM: CWCSNEW

**PIER SCOUR CALCULATIONS**

L/a ratio = 36 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1.6  
 Froude # at bridge = 0.62 Using pier width  $a$  on Figure 11,  $\xi =$  4.9 Pier scour  $y_{ps} =$  7.2 ft

PGRM: Pie

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  4.05 ft right abutment,  $y_{aRT} =$  3.6 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  13.3 and  $\psi_{RT} =$  12.6  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1/0.55) =$  13.3 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1/0.55) =$  12.6 ft

PGRM: Abutment

Route Colorado Blvd Stream False Bottom Ck MRM \_\_\_\_\_ Date \_\_\_\_\_ Initials \_\_\_\_\_  
 Bridge Structure No. 41126089 Location SE of Spearfish  
 GPS coordinates: N 44° 28.491' taken from: USL abutment  centerline of  $\uparrow$  MRM end \_\_\_\_\_  
W 103° 47.775' Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 14.94 sq. mi.

The average bottom of the main channel was 13.8 ft below top of guardrail at a point 26 ft from left abutment.  
 Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio  regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = <u>2600</u>			Q <sub>500</sub> = <u>6770</u>		
Estimated flow passing through bridge	<u>2600</u>			<u>6770</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>0</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Chance of Pressure flow		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Armored appearance to channel			<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>
Lateral instability of channel			<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>

713  
 2 55.7  
 5 209  
 10 436  
 25 946  
 50 1630  
 100 2600  
 500 6770

Riprap at abutments?  Yes \_\_\_ No \_\_\_ Marginal Gabion baskets  
 Evidence of past Scour?  Yes \_\_\_ No \_\_\_ Don't know possibly pier scour  
 Debris Potential? \_\_\_ High \_\_\_ Med  Low a few small trees upstream

Does scour countermeasure(s) appear to have been designed?

Riprap  Yes \_\_\_ No \_\_\_ Don't know \_\_\_ NA  
 Spur Dike \_\_\_ Yes \_\_\_ No \_\_\_ Don't know  NA  
 Other \_\_\_ Yes \_\_\_ No \_\_\_ Don't know  NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay \_\_\_ Sand \_\_\_ Gravel \_\_\_ Cobbles  Boulders \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

str. no  
 approach from bridge  
 LOB from channel  
 ROB from channel  
 Bridge from approach

assume CWCS  
 left abut.  
 rt. abut.  
 band of riprap in front of bridge

Summary of Results

	Q100	Q500
Bridge flow evaluated	<u>2600</u>	<u>6770</u>
Flow depth at left abutment (yaLT), in feet	<u>0.8</u>	<u>4.05</u>
Flow depth at right abutment (yaRT), in feet	<u>0.8</u>	<u>3.6</u>
Contraction scour depth (yca), in feet	<u>0</u>	<u>0</u>
Pier scour depth (yps), in feet	<u>7.1</u>	<u>7.2</u>
Left abutment scour depth (yas), in feet	<u>3.5</u>	<u>13.3</u>
Right abutment scour depth (yas), in feet	<u>3.5</u>	<u>12.6</u>
Flow angle of attack	<u>12° (7° off)</u>	<u>12° (7° off)</u>

See Comments/Diagram for justification where required