

# False Bottom Creek

## SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 41165066 Date 4/11/12 Initials cu Region (A)BCD  
 Site \_\_\_\_\_ Location 2.5 mi S of St. Onge  
 $Q_{100} =$  \_\_\_\_\_ by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq.   
 Bridge discharge ( $Q_2$ ) = \_\_\_\_\_ (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 120 ft. Flow angle at bridge = 30 ° Abut. Skew = 0 ° Effective Skew = 30 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_

Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = \_\_\_\_\_ ft\*  $q_2 = Q_2/W_2 =$  \_\_\_\_\_ ft<sup>2</sup>/s

Bridge Vel,  $V_2 =$  \_\_\_\_\_ ft/s Final  $y_2 = q_2/V_2 =$  \_\_\_\_\_ ft  $\Delta h =$  \_\_\_\_\_ ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  \_\_\_\_\_ ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = \_\_\_\_\_ ft  
 Low Steel Elev. = 12.5 ft  
 n (Channel) = 0.02  
 n (LOB) = \_\_\_\_\_  
 n (ROB) = \_\_\_\_\_  
 Pier Width = \_\_\_\_\_ ft  
 Pier Length = \_\_\_\_\_ ft  
 # Piers for 100 yr = \_\_\_\_\_ ft

*Q500 passes through bridge  
 → no smaller flow calc'd*

### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 =$  \_\_\_\_\_ ft  
 Width of left overbank flow at approach,  $W_{lob} =$  \_\_\_\_\_ ft Average left overbank flow depth,  $y_{lob} =$  \_\_\_\_\_ ft  
 Width of right overbank flow at approach,  $W_{rob} =$  \_\_\_\_\_ ft Average right overbank flow depth,  $y_{rob} =$  \_\_\_\_\_ ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  \_\_\_\_\_ From Figure 9  $W_2$  (effective) = \_\_\_\_\_ ft  $y_{cs} =$  \_\_\_\_\_ ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2/y_1)^{7/6} =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

### PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1.0  
 Froude # at bridge = \_\_\_\_\_ Using pier width a on Figure 11,  $\xi =$  \_\_\_\_\_ Pier scour  $y_{ps} =$  \_\_\_\_\_ ft

### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} =$  \_\_\_\_\_ ft right abutment,  $y_{aRT} =$  \_\_\_\_\_ ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  \_\_\_\_\_ and  $\psi_{RT} =$  \_\_\_\_\_  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1/0.55) =$  \_\_\_\_\_ ft Right abutment scour  $y_{as} = \psi_{RT} (K_1/0.55) =$  \_\_\_\_\_ ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWC/SNEW

PRGM: Pier

PRGM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 41165066 Date 4/11/12 Initials CM Region (A)BCD  
 Site \_\_\_\_\_ Location 2.5 mi S of St. Onge  
 $Q_{500} = \underline{8310}$  by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq.   
 Bridge discharge ( $Q_2$ ) = 8310 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 120 ft. Flow angle at bridge = 30 ° Abut. Skew = 0 ° Effective Skew = 30 °  
 Width ( $W_2$ ) iteration = 120 102 107 105  
 Avg. flow depth at bridge,  $y_2$  iteration = 7.2 8.7 8.4 8.5  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 90.93 ft\*  $q_2 = Q_2/W_2 = \underline{91.4}$  ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 = \underline{10.7}$  ft/s Final  $y_2 = q_2/V_2 = \underline{8.5}$  ft  $\Delta h = \underline{2.7}$  ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = \underline{10.9}$  ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = \_\_\_\_\_ ft  
 Low Steel Elev. = 12.5 ft  
 $n$  (Channel) = 0.035  
 $n$  (LOB) = 0.037  
 $n$  (ROB) = 0.035  
 Pier Width = 0.8 ft  
 Pier Length = 0.8 ft  
 # Piers for 500 yr = 4 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 = \underline{150}$  ft  
 Width of left overbank flow at approach,  $W_{lob} = \underline{23}$  ft Average left overbank flow depth,  $y_{lob} = \underline{1.15}$  ft  
 Width of right overbank flow at approach,  $W_{rob} = \underline{120}$  ft Average right overbank flow depth,  $y_{rob} = \underline{5.5}$  ft

~~Live Bed Contraction Scour (use if bed material is small cobbles or finer)~~

~~$x =$  \_\_\_\_\_ From Figure 9  $W_2$  (effective) = \_\_\_\_\_ ft  $y_{cs} =$  \_\_\_\_\_ ft~~

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} = \underline{0.2}$  ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) = \underline{2.6}$  ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} = \underline{9.73}$  ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006(q_2/y_1^{7/6})^3 = \underline{0.107}$  ft

If  $D_{50} \geq D_{c50}$ ,  $\chi = \underline{0.0}$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 = \underline{X}$

From Figure 10,  $y_{cs} = \underline{0.0}$  ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1.0

Correction factor for flow angle of attack (from Table 1),  $K_2 = \underline{1.0}$

Froude # at bridge = 0.65

Using pier width  $a$  on Figure 11,  $\xi = \underline{3.9}$  Pier scour  $y_{ps} = \underline{3.6}$  ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} = \underline{1.15}$  ft right abutment,  $y_{aRT} = \underline{5.5}$  ft

Shape coefficient  $K_1 = 1.00$  for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through

Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = \underline{4.9}$  and  $\psi_{RT} = \underline{15.9}$

Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) = \underline{4.9}$  ft

Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) = \underline{15.9}$  ft



Route St. Onge Rd Stream False Bottom Ck MRM \_\_\_\_\_ Date 4/11/12 Initials CU  
 Bridge Structure No. 41165066 Location 2.5 mi S of St. Onge  
 GPS coordinates: N 44° 30' 32.00" taken from: USL abutment  centerline of MRM end \_\_\_\_\_  
W 103° 43' 10.0" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 29.05 sq. mi.  
 The average bottom of the main channel was 16.5 ft below top of guardrail at a point 43 ft from left abutment.  
 Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio  regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> =			Q <sub>500</sub> = <u>8310</u>		
Estimated flow passing through bridge				<u>8310</u>		
Estimated road overflow & overtopping						
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping					<input checked="" type="checkbox"/>	
Chance of Pressure flow					<input checked="" type="checkbox"/>	
Armored appearance to channel					<input checked="" type="checkbox"/>	
Lateral instability of channel					<input checked="" type="checkbox"/>	

Riprap at abutments? \_\_\_ Yes \_\_\_ No  Marginal  
 Evidence of past Scour?  Yes \_\_\_ No \_\_\_ Don't know *channel is a little incised*  
 Debris Potential? \_\_\_ High  Med \_\_\_ Low

Does scour countermeasure(s) appear to have been designed?  
 Riprap  Yes \_\_\_ No \_\_\_ Don't know \_\_\_ NA  
 Spur Dike \_\_\_ Yes \_\_\_ No \_\_\_ Don't know  NA  
 Other \_\_\_ Yes \_\_\_ No \_\_\_ Don't know  NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material	Silt/Clay ___	Sand ___	Gravel ___	Cobbles <input checked="" type="checkbox"/>	Boulders ___
Size range, in mm	<0.062	0.062-2.00	2.00-64	64-250	>250

Comments, Diagrams & orientation of digital photos

*10/2/12*  

2	75.3	<i>Photos</i> 2199 - 1D 2000 - US 01 - US RB 02 - US LB 03 - US Face 04 - L. App XS	05 - RB App XS 06 - L. Abut 07 - R. Abut 08 - Piers
5	274		
10	561		
25	1200		
50	2050		
100	3260		
500	8310		

Summary of Results

	Q100	Q500
Bridge flow evaluated		<u>8310</u>
Flow depth at left abutment (yaLT), in feet		<u>1.15</u>
Flow depth at right abutment (yaRT), in feet		<u>5.5</u>
Contraction scour depth (yca), in feet		<u>0.0</u>
Pier scour depth (yps), in feet		<u>3.6</u>
Left abutment scour depth (yas), in feet		<u>4.9</u>
Right abutment scour depth (yas), in feet		<u>15.9</u>
Flow angle of attack		<u>30°</u>

See Comments/Diagram for justification where required