

near Whitewood OK RJ

Whitewood Creek

### SCOUR ANALYSIS AND REPORTING FORM

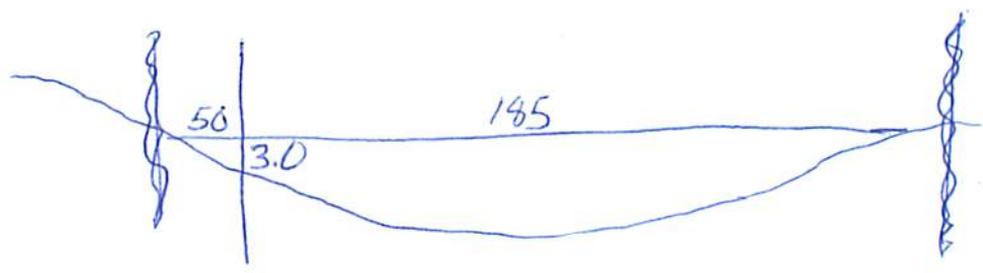
Bridge Structure No. 41212091 Date 7/12/11 Initials CW Region (A B C D) \_\_\_\_\_  
 Site \_\_\_\_\_ Location I-90 Exit 23, approx 1 E on Whitewood Valley Rd  
 $Q_{100} =$  7550 by: drainage area ratio  flood freq. anal. \_\_\_\_\_ regional regression eq. \_\_\_\_\_  
 Bridge discharge ( $Q_2$ ) = 7832 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)  
6890

#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = ~~145~~ 185 ft Flow angle at bridge = 20° Abut. Skew = 0° Effective Skew = 20°  
 Width ( $W_2$ ) iteration = 185  
 Avg. flow depth at bridge,  $y_2$  iteration = 5.7 > 5.4 → RD Overflow  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 173.84 ft\*  $q_2 = Q_2/W_2 =$  39.6 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  7.3 ft/s Final  $y_2 = q_2/V_2 =$  5.4 ft  $\Delta h =$  1.1 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  6.5 ft

\*NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = \_\_\_\_\_ ft  
 Low Steel Elev. = 5.4 ft  
 n (Channel) = 0.050  
 n (LOB) = 0.060  
 n (ROB) = 0.060  
 Pier Width = 1.85 ft  
 Pier Length = 1.85 ft  
 # Piers for 100 yr = 4



#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 =$  185 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  50 ft Average left overbank flow depth,  $y_{lob} =$  1.5 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  0 ft Average right overbank flow depth,  $y_{rob} =$  0 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  0.87 From Figure 9  $W_2$  (effective) = 166.4 ft  $y_{cs} =$  1.3 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  0.20 ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  4.51 ft/s  
 Critical approach velocity,  $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} =$  8.92 ft/s  
 If  $V_1 < V_c$  and  $D_{50} >= 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 =$  0.053 ft If  $D_{50} >= D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2/(D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  0.0 From Figure 10,  $y_{cs} =$  0.0 ft

#### PIER SCOUR CALCULATIONS

L/a ratio = 1.0 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1.0  
 Froude # at bridge = 0.55 Using pier width a on Figure 11,  $\xi =$  7.5 Pier scour  $y_{ps} =$  6.9 ft

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} =$  1.5 ft right abutment,  $y_{aRT} =$  0 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  6.3 and  $\psi_{RT} =$  0  
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  6.3 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  0 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCSNEW

PGRM: Pier

PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

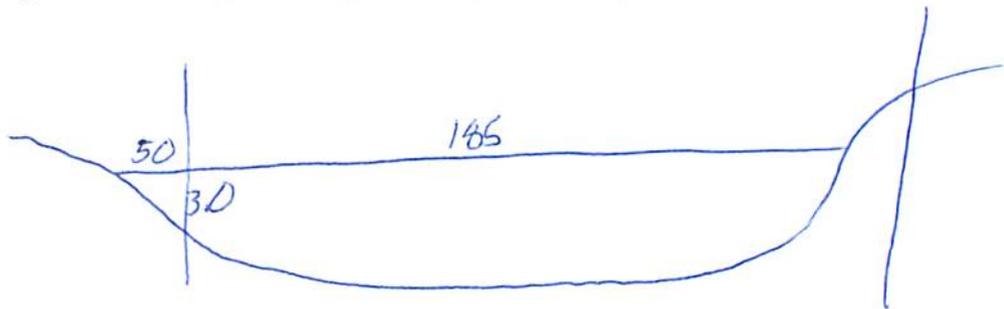
Bridge Structure No. 41212091 Date 7/12/11 Initials AW Region (A B C D) A  
 Site \_\_\_\_\_ Location I-90 Exit 23, Approach 1E on Whitewood Valley Rd.  
 $Q_{500} = 21400$  by: drainage area ratio  flood freq. anal. \_\_\_\_\_ regional regression eq. \_\_\_\_\_  
 Bridge discharge ( $Q_2$ ) = 6390 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 145 ft. Flow angle at bridge = 20° Abut. Skew = 0° Effective Skew = 20°  
 Width ( $W_2$ ) iteration = 145  
 Avg. flow depth at bridge,  $y_2$  iteration = 5.7 > 5.4  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 173.84 ft\*  $q_2 = Q_2/W_2 = 39.6$  ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 = 7.3$  ft/s Final  $y_2 = q_2/V_2 = 5.4$  ft  $\Delta h = 1.1$  ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = 6.5$  ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = \_\_\_\_\_ ft  
 Low Steel Elev. = 5.4 ft  
 n (Channel) = 0.050  
 n (LOB) = 0.060  
 n (ROB) = 0.060  
 Pier Width = 1.85 ft  
 Pier Length = 1.85 ft  
 # Piers for 500 yr = 4



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 = 145$  ft  
 Width of left overbank flow at approach,  $W_{lob} = 50$  ft Average left overbank flow depth,  $y_{lob} = 1.5$  ft  
 Width of right overbank flow at approach,  $W_{rob} = 0$  ft Average right overbank flow depth,  $y_{rob} = 0$  ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x = 0.87$  From Figure 9  $W_2$  (effective) = 166.7 ft  $y_{cs} = 1.3$  ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} = 0.20$  ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) = 4.51$  ft/s  
 Critical approach velocity,  $V_c = 11.52 y_1^{1/6} D_{50}^{1/3} = 4.92$  ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 = 0.053$  ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 = 0.0$  From Figure 10,  $y_{cs} = 0.0$  ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1.0 Correction factor for flow angle of attack (from Table 1),  $K_2 = 1.0$   
 Froude # at bridge = 0.55 Using pier width a on Figure 11,  $\xi = 7.5$  Pier scour  $y_{ps} = 6.9$  ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} = 1.5$  ft right abutment,  $y_{aRT} = 0$  ft  
 Shape coefficient  $K_1 = 1.00$  for vertical-wall,  $0.82$  for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = 6.3$  and  $\psi_{RT} = 0$   
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1/0.55) = 6.3$  ft Right abutment scour  $y_{as} = \psi_{RT} (K_1/0.55) = 0$  ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCSNEW

PRGM: Pier

PRGM: Abutment

Whiteward

Route Valley Rd Stream Whitewood Creek MRM Date 7/12/11 Initials Cc  
Bridge Structure No. 41212091 Location I-90 Exit 23, Approx. 1E on Whitewood Valley Rd  
GPS coordinates: N 44° 28' 22.5" taken from: USL abutment X centerline of MRM end  
W 103° 37' 31.4" Datum of coordinates: WGS84 X NAD27

Drainage area = 51.62 sq. mi.

The average bottom of the main channel was 9.4 ft below top of guardrail at a point 91 ft from left abutment.

Method used to determine flood flows: Freq. Anal. drainage area ratio regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Table with columns for Q100, Q500, and various considerations like 'Chance of overtopping', 'Chance of Pressure flow', etc.

Riprap at abutments? X Yes \_\_\_ No \_\_\_ Marginal  
Evidence of past Scour? \_\_\_ Yes X No \_\_\_ Don't know  
Debris Potential? X High \_\_\_ Med \_\_\_ Low

Does scour countermeasure(s) appear to have been designed?

Riprap X Yes \_\_\_ No \_\_\_ Don't know \_\_\_ NA  
Spur Dike \_\_\_ Yes \_\_\_ No \_\_\_ Don't know X NA  
Other \_\_\_ Yes \_\_\_ No \_\_\_ Don't know X NA

Bed Material Classification Based on Median Particle Size (D50)

Material Silt/Clay \_\_\_ Sand \_\_\_ Gravel \_\_\_ Cobbles X Boulders \_\_\_  
Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

Photos  
1765- IP  
66- US  
67- US RB  
68- US LB  
69- L. Abut  
70- R. Abut  
72- Piers  
73- US Face bridge  
74- US Face Bridge

Summary of Results

Table with columns for Q100 and Q500, listing various flow and scour measurements.

See Comments/Diagram for justification where required