

I did the eastern of the 2 bridges close to each other ok-Rat

**SCOUR ANALYSIS AND REPORTING FORM**

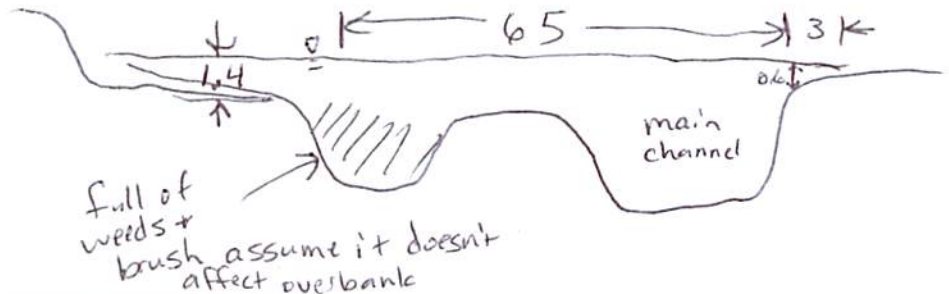
Bridge Structure No. 41256268 Date 9-20-12 Initials RFT Region (A B C D)  
 Site \_\_\_\_\_ Location 0.1 mi W of Boxelder Conservation Rd  
 $Q_{100} =$  2090 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq.   
 Bridge discharge ( $Q_2$ ) = 2090 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 65 ft. Flow angle at bridge = 10 ° Abut. Skew = 0 ° Effective Skew = 10 °  
 Width ( $W_2$ ) iteration = 47 59 52 54  
 Avg. flow depth at bridge,  $y_2$  iteration = 5.8 5.1 5.5 5.4  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 53.18 ft\*  $q_2 = Q_2/W_2 =$  39.3 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  7.3 ft/s Final  $y_2 = q_2/V_2 =$  5.4 ft  $\Delta h =$  1.1 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  6.5 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(a) + a \cos(a)$   
 If  $y_1$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = -0.1 ft  
 Low Steel Elev. = 8.3 ft  
 n (Channel) = 0.050  
 n (LOB) = 0.065  
 n (ROB) = 0.050  
 Pier Width = NA ft  
 Pier Length = NA ft  
 # Piers for 100 yr = 0 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  65 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  60 ft Average left overbank flow depth,  $y_{lob} =$  1.4 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  3 ft Average right overbank flow depth,  $y_{rob} =$  0.3 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  1 From Figure 9  $W_2$  (effective) = \_\_\_\_\_ ft  $y_{cs} =$  \_\_\_\_\_ ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  0.4 ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  2.51 ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  11.24 ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  0.052 ft

If  $D_{50} \geq D_{c50}$ ,  $\chi =$  0.0

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_

From Figure 10,  $y_{cs} =$  0 ft

**PIER SCOUR CALCULATIONS**

L/a ratio = \_\_\_\_\_ Correction-factor for flow angle of attack (from Table 1),  $K_2 =$  \_\_\_\_\_  
 Froude # at bridge = \_\_\_\_\_ Using pier width a on Figure 11,  $\xi =$  \_\_\_\_\_ Pier scour  $y_{ps} =$  \_\_\_\_\_ ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  1.4 ft right abutment,  $y_{aRT} =$  0.3 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  5.9 and  $\psi_{RT} =$  1.4  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) =$  5.9 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) =$  1.4 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"  
 PGRM: Contract  
 PGRM: CWCSNEW  
 PGRM: Pier  
 PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

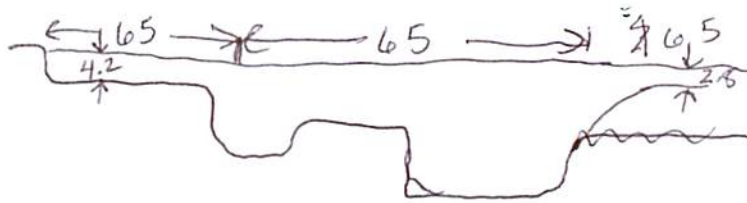
Bridge Structure No. 41250268 Date \_\_\_\_\_ Initials \_\_\_\_\_ Region (A)BCD  
 Site \_\_\_\_\_ Location 0.1 mi W of Boxelder Conservation Rd  
 $Q_{500} = 4800$  by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq.   
 Bridge discharge ( $Q_2$ ) = 4800 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 65 ft. Flow angle at bridge = 10° Abut. Skew = 0° Effective Skew = 10°  
 Width ( $W_2$ ) iteration = 7.7  
 Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 64.01 ft\*  $q_2 = Q_2/W_2 = 75$  ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 = 9.8$  ft/s Final  $y_2 = q_2/V_2 = 7.7$  ft  $\Delta h = 2.0$  ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = 9.6$  ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = -0.1 ft  
 Low Steel Elev. = 8.3 ft  
 n (Channel) = 0.050  
 n (LOB) = 0.065  
 n (ROB) = 0.050  
 Pier Width = NA ft  
 Pier Length = NA ft  
 # Piers for 500 yr = 0 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 = 65$  ft  
 Width of left overbank flow at approach,  $W_{lob} = 65$  ft Average left overbank flow depth,  $y_{lob} = 4.2$  ft  
 Width of right overbank flow at approach,  $W_{rob} = 65$  ft Average right overbank flow depth,  $y_{rob} = 2.8$  ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  \_\_\_\_\_ From Figure 9  $W_2$  (effective) = \_\_\_\_\_ ft  $y_{cs} =$  \_\_\_\_\_ ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} = 0.4$  ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) = 2.56$  ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} = 12.0$  ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 = 0.092$  ft

If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} = 0$  ft

**PIER SCOUR CALCULATIONS**

L/a ratio = \_\_\_\_\_ Correction factor for flow angle of attack (from Table 1),  $K_2 =$  \_\_\_\_\_  
 Froude # at bridge = \_\_\_\_\_ Using pier width a on Figure 11,  $\xi =$  \_\_\_\_\_ Pier scour  $y_{ps} =$  \_\_\_\_\_ ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} = 4.2$  ft right abutment,  $y_{aRT} = 2.8$  ft  
 Shape coefficient  $K_1 = 1.00$  for vertical-wall,  $0.82$  for vertical-wall with wingwalls, 0.55 for spill-through

Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = 13.6$  and  $\psi_{RT} = 11.2$

Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) = 13.6$  ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) = 11.2$  ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCSNEW

PRGM: Pie

PRGM: Abutment



Route Nano Rd Stream Boxelder Ck MRM \_\_\_\_\_ Date \_\_\_\_\_ Initials \_\_\_\_\_  
 Bridge Structure No. 41250268 Location 0.1 mi W of Boxelder Conservation Rd  
 GPS coordinates: 44° 12.980' taken from: USL abutment  centerline of  $\uparrow$  MRM end \_\_\_\_\_  
103° 33.158' Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 39.72 sq. mi.  
 The average bottom of the main channel was 13.2 ft below top of guardrail at a point 22 ft from left abutment.  
 Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio  regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> =			Q <sub>500</sub> =		
Estimated flow passing through bridge						
Estimated road overflow & overtopping						
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping						
Chance of Pressure flow						
Armored appearance to channel						
Lateral instability of channel						

713  
 2 | 71.3  
 5 | 22.5  
 10 | 42.4  
 25 | 84.5  
 50 | 137.0  
 100 | 209.0  
 500 | 480.0

Riprap at abutments? \_\_\_ Yes \_\_\_ No  Marginal native rock in bottom, crushed rock on left abut.  
 Evidence of past Scour? \_\_\_ Yes  No \_\_\_ Don't know  
 Debris Potential? \_\_\_ High \_\_\_ Med  Low trees, but no piers

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Spur Dike \_\_\_ Yes \_\_\_ No \_\_\_ Don't know  NA  
 Other \_\_\_ Yes \_\_\_ No \_\_\_ Don't know  NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay \_\_\_ Sand \_\_\_ Gravel \_\_\_ Cobbles  Boulders \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

rocks + cobble in channel bottom; assume cwcs

Comments, Diagrams & orientation of digital photos

str. no  
 approach from bridge  
 LOB from bridge  
 ROB from bridge  
 bridge from approach  
 left abut.  
 rt. abut.

Summary of Results

	Q <sub>100</sub>	Q <sub>500</sub>
Bridge flow evaluated	2090	4800
Flow depth at left abutment (yaLT), in feet	1.4	4.2
Flow depth at right abutment (yaRT), in feet	0.3	2.8
Contraction scour depth (y <sub>cs</sub> ), in feet	0	0
Pier scour depth (y <sub>ps</sub> ), in feet	NA	NA
Left abutment scour depth (y <sub>as</sub> ), in feet	5.9	13.6
Right abutment scour depth (y <sub>as</sub> ), in feet	1.4	11.2
IFlow angle of attack	10°	10°

See Comments/Diagram for justification where required

Garmin at  
West bridge  
44° 12.986'  
103° 33.291'

Garmin at  
East bridge  
44° 12.978'  
103° 33.151'

44° 12.96'  
103° 33.172'

