

OK-Rat

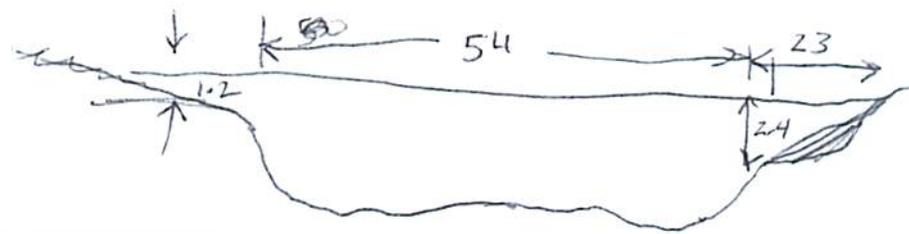
### SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 41280298 Date 9-20-12 Initials RTT Region (A)BCD  
 Site \_\_\_\_\_ Location 0.1 mi E of Roberts Drain  
 $Q_{100} =$  992 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq.   
 Bridge discharge ( $Q_2$ ) = 992 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 50 ft. Flow angle at bridge = 0° Abut. Skew = 0° Effective Skew = 0°  
 Width ( $W_2$ ) iteration = 34 40 39  
 Avg. flow depth at bridge,  $y_2$  iteration = 4.6 4.2 4.2  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 39 ft\*  $q_2 = Q_2/W_2 =$  25.4 ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 =$  6.0 ft/s Final  $y_2 = q_2/V_2 =$  4.2 ft  $\Delta h =$  0.7 ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  5.0 ft  
 \*NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = \_\_\_\_\_ ft  
 Low Steel Elev. = 5.6 ft  
 n (Channel) = 0.040  
 n (LOB) = 0.035  
 n (ROB) = 0.060  
 Pier Width = NA ft  
 Pier Length = NA ft  
 # Piers for 100 yr = 0 ft



#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 =$  54 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  40 ft Average left overbank flow depth,  $y_{lob} =$  1.2 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  23 ft Average right overbank flow depth,  $y_{rob} =$  1.2 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  \_\_\_\_\_ From Figure 9  $W_2$  (effective) = \_\_\_\_\_ ft  $y_{cs} =$  \_\_\_\_\_ ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  0.4 ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  1.7 ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  10.76 ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2/y_1)^{7/6} =$  0.035 ft If  $D_{50} \geq D_{c50}$ ,  $\chi =$  0.0  
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  0 ft

#### PIER SCOUR CALCULATIONS

L/a ratio = \_\_\_\_\_ Correction-factor for flow angle of attack (from Table 1),  $K_2 =$  \_\_\_\_\_  
 Froude # at bridge = \_\_\_\_\_ Using pier width a on Figure 11,  $\xi =$  \_\_\_\_\_ Pier scour  $y_{ps} =$  \_\_\_\_\_ ft

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} =$  1.2 ft right abutment,  $y_{aRT} =$  1.2 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  5.1 and  $\psi_{RT} =$  5.1  
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  5.1 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  5.1 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"  
 PGRM: Contract  
 PGRM: CWCSNEW  
 PGRM: Pier  
 PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 41280298 Date \_\_\_\_\_ Initials \_\_\_\_\_ Region (A B C D)

Site \_\_\_\_\_ Location 0.1 mi E of Roberts Draw

$Q_{500} = 2360$  by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq.

Bridge discharge ( $Q_2$ ) = 2360 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 50 ft. Flow angle at bridge = 0 ° Abut. Skew = 0 ° Effective Skew = 0 °

Width ( $W_2$ ) iteration = 50

Avg. flow depth at bridge,  $y_2$  iteration = 5.9

Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 50 ft\*  $q_2 = Q_2/W_2 = 47.2$  ft<sup>2</sup>/s

Bridge Vel,  $V_2 = 7.9$  ft/s Final  $y_2 = q_2/V_2 = 5.9$  ft  $\Delta h = 1.3$  ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = 7.2$  ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(\alpha) + a \cos(\alpha)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = \_\_\_\_\_ ft

Low Steel Elev. = 5.6 ft

n (Channel) = 0.040

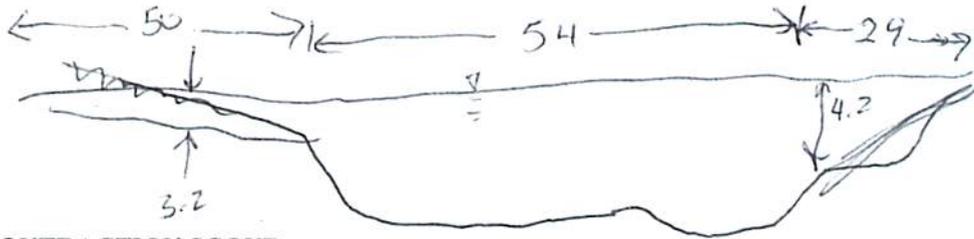
n (LOB) = 0.035

n (ROB) = 0.060

Pier Width = NA ft

Pier Length = NA ft

# Piers for 500 yr = 0



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 = 54$  ft

Width of left overbank flow at approach,  $W_{lob} = 50$  ft Average left overbank flow depth,  $y_{lob} = 3.2$  ft

Width of right overbank flow at approach,  $W_{rob} = 29$  ft Average right overbank flow depth,  $y_{rob} = 2.1$  ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  \_\_\_\_\_ From Figure 9  $W_2$  (effective) = \_\_\_\_\_ ft  $y_{cs} =$  \_\_\_\_\_ ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} = 0.4$  ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) = 2.46$  ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} = 11.44$  ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2/y_1)^{7/6} = 0.063$  ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} = 0$  ft

**PIER SCOUR CALCULATIONS**

L/a ratio = \_\_\_\_\_ Correction factor for flow angle of attack (from Table 1),  $K_2 =$  \_\_\_\_\_

Froude # at bridge = \_\_\_\_\_ Using pier width  $a$  on Figure 11,  $\xi =$  \_\_\_\_\_ Pier scour  $y_{ps} =$  \_\_\_\_\_ ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} = 3.2$  ft right abutment,  $y_{aRT} = 2.1$  ft

Shape coefficient  $K_1 = 1.00$  for vertical-wall,  $0.82$  for vertical-wall with wingwalls,  $0.55$  for spill-through

Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = 11.9$  and  $\psi_{RT} = 8.6$

Left abutment scour,  $y_{as} = \psi_{LT} (K_1/0.55) = 11.9$  ft Right abutment scour  $y_{as} = \psi_{RT} (K_1/0.55) = 8.6$  ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCSNEW

PRGM: Pie

PRGM: Abutment

Route Nemo Rd Stream Estes CK MRM \_\_\_\_\_ Date \_\_\_\_\_ Initials \_\_\_\_\_  
 Bridge Structure No. 41290298 Location 0.1 mi E of Roberts Draw  
 GPS coordinates: N 44° 10.366' taken from: USL abutment \_\_\_\_\_ centerline of ↑ MRM end \_\_\_\_\_  
W 103° 29.581' Datum of coordinates: WGS84 \_\_\_\_\_ NAD27 \_\_\_\_\_

Drainage area = 6.02 sq. mi.  
 The average bottom of the main channel was 11.8 ft below top of guardrail at a point 18 ft from left abutment.  
 Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio  regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>100</sub> = <u>992</u>			Q <sub>500</sub> = <u>2360</u>		
Estimated flow passing through bridge	<u>992</u>			<u>2360</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>0</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Chance of Pressure flow		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

713  
 2 29.2  
 3 97.5  
 10 191  
 25 391  
 50 645  
 100 992  
 500 2360.

Riprap at abutments?  Yes \_\_\_ No \_\_\_ Marginal bridge is totally lined with riprap  
 Evidence of past Scour? \_\_\_ Yes  No \_\_\_ Don't know assume CWCS  
 Debris Potential? \_\_\_ High  Med \_\_\_ Low trees, but no piers

Does scour countermeasure(s) appear to have been designed?  
 Riprap  Yes \_\_\_ No \_\_\_ Don't know \_\_\_ NA  
 Spur Dike \_\_\_ Yes \_\_\_ No \_\_\_ Don't know  NA  
 Other \_\_\_\_\_ \_\_\_ Yes \_\_\_ No \_\_\_ Don't know  NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay \_\_\_ Sand \_\_\_ Gravel \_\_\_ Cobbles  Boulders \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

str. no.  
 approach  
 LOB  
 ROB  
 Bridge from approach  
 under bridge

Summary of Results

	Q100	Q500
Bridge flow evaluated	<u>992</u>	<u>2360</u>
Flow depth at left abutment (yaLT), in feet	<u>1.2</u>	<u>3.2</u>
Flow depth at right abutment (yaRT), in feet	<u>1.2</u>	<u>2.1</u>
Contraction scour depth (yca), in feet	<u>0</u>	<u>0</u>
Pier scour depth (yps), in feet	<u>NA</u>	<u>NA</u>
Left abutment scour depth (yas), in feet	<u>5.1</u>	<u>11.9</u>
Right abutment scour depth (yas), in feet	<u>5.1</u>	<u>8.6</u>
Flow angle of attack	<u>0°</u>	<u>0°</u>

See Comments/Diagram for justification where required