

OK RT

### SCOUR ANALYSIS AND REPORTING FORM

Bridge Structure No. 42020144 Date 5/25/12 Initials Pat Region (A B C D) (D)  
 Site \_\_\_\_\_ Location 3.4 mi S of Lennox on 466 Ave  
 $Q_{100} = Q_{75} = 2760$  by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 2760 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

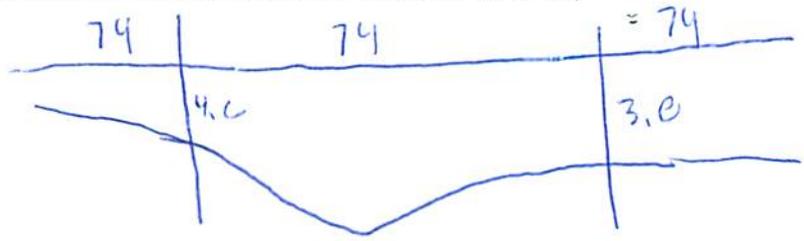
#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 74 ft. Flow angle at bridge = 30 ° Abut. Skew = 0 ° Effective Skew = 30 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_  
 Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_

Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 64.05 ft\*  $q_2 = Q_2/W_2 = 43.1$  ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 = 4.7$  ft/s Final  $y_2 = q_2/V_2 = 9.3$  ft  $\Delta h = 0.4$  ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = 9.7$  ft

\*NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0 ft  
 Low Steel Elev. = 10.5 ft  
 n (Channel) = 0.030  
 n (LOB) = 0.030  
 n (ROB) = 0.030  
 Pier Width = 1.7 ft  
 Pier Length = 1.7 ft  
 # Piers for 100 yr = 4



#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 = 74$  ft  
 Width of left overbank flow at approach,  $W_{lob} = 74$  ft Average left overbank flow depth,  $y_{lob} = 4.6$  ft  
 Width of right overbank flow at approach,  $W_{rob} = 74$  ft Average right overbank flow depth,  $y_{rob} = 3.0$  ft

$5.3 = 3.9 + 1.4$   
 $-1.4 = -1.4$   
 $= 4.6$

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x = 8.22$  From Figure 9  $W_2$  (effective) = 57.3 ft  $y_{cs} = 9.1$  ft

~~Clear Water Contraction Scour~~ (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

#### PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 = 1$   
 Froude # at bridge = 0.27 Using pier width a on Figure 11,  $\xi = 7$  Pier scour  $y_{ps} = 5.8$  ft

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} = 4.6$  ft right abutment,  $y_{aRT} = 3.0$  ft  
 Shape coefficient  $K_1 = 1.00$  for vertical-wall,  $0.82$  for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = 14.5$  and  $\psi_{RT} = 11.5$   
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) = 14.3$  ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) = 11.5$  ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCSNEW

PRGM: Pier

PRGM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 42020144 Date 5/25/12 Initials Rat Region (A B C D)  
 Site \_\_\_\_\_ Location 3.4 mi S of Lennox on 466 Ave  
 $Q_{500} = Q_2 =$  3770 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 3549 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 74 ft. Flow angle at bridge = 30 ° Abut. Skew = 0 ° Effective Skew = 30 °  
 Width ( $W_2$ ) iteration = \_\_\_\_\_

Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 64.08 ft\*  $q_2 = Q_2/W_2 =$  52.1 ft<sup>2</sup>/s

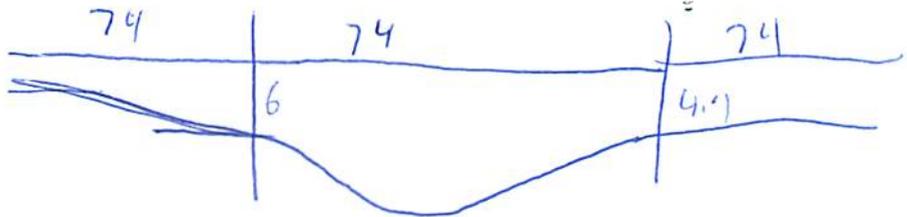
Bridge Vel,  $V_2 =$  5.3 ft/s Final  $y_2 = q_2/V_2 =$  10.5 ft  $\Delta h =$  0.6 ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  11.1 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0 ft  
 Low Steel Elev. = 10.5 ft  
 $n$  (Channel) = 0.030  
 $n$  (LOB) = 0.030  
 $n$  (ROB) = 0.030  
 Pier Width = 1.7 ft  
 Pier Length = 1.7 ft  
 # Piers for 500 yr = 4 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  74 ft  $1.0 \frac{2}{3} = 0.7$   
 Width of left overbank flow at approach,  $W_{lob} =$  74 ft Average left overbank flow depth,  $y_{lob} =$  6 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  74 ft Average right overbank flow depth,  $y_{rob} =$  4.4 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)

$x =$  11.45 From Figure 9  $W_2$  (effective) = 57.3 ft  $y_{cs} =$  12.5 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{cs0} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{cs0}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6.7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.29 Using pier width  $a$  on Figure 11,  $\xi =$  7 Pier scour  $y_{ps} =$  5.9 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  6 ft right abutment,  $y_{aRT} =$  4.4 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  16.8 and  $\psi_{RT} =$  14  
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1 / 0.55) =$  16.8 ft Right abutment scour  $y_{as} = \psi_{RT} (K_1 / 0.55) =$  14 ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWCNEW

PGRM: Pie:

PGRM: Abutment

Route 466 Ave Stream Long Ck MRM \_\_\_\_\_ Date 5/25/12 Initials Kat  
 Bridge Structure No. 42020/44 Location 3.4 mi S of Lennox on 466 Ave  
 GPS coordinates: N 43° 17' 46" W 96° 53' 9.54" taken from: USL abutment  centerline of  MRM end \_\_\_\_\_  
 Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 53.55 sq. mi.  
 The average bottom of the main channel was 14.4 ft below top of guardrail at a point 35 ft from left abutment.  
 Method used to determine flood flows: \_\_\_\_\_ Freq. Anal. \_\_\_\_\_ drainage area ratio  regional regression equations.

MISCELLANEOUS CONSIDERATIONS

Flows	Q <sub>25</sub> <sup>25</sup> = <u>2760</u>			Q <sub>500</sub> <sup>500</sup> = <u>3770</u>		
Estimated flow passing through bridge	<u>2760</u>			<u>3549</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>221</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>				<input checked="" type="checkbox"/>
Chance of Pressure flow		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

8/24  
 2 | 779  
 5 | 2050  
 10 | 3300  
 25 | 5430  
 50 | 7420  
 100 | 9780  
 500 | 16800

Riprap at abutments?  Yes \_\_\_\_\_ No \_\_\_\_\_ Marginal \_\_\_\_\_  
 Evidence of past Scour?  Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know plg/contraction  
 Debris Potential? \_\_\_\_\_ High \_\_\_\_\_ Med  Low

5/22  
 2 | 403  
 5 | 1050  
 10 | 1690  
 25 | 2760  
 50 | 3770  
 100 | 4950  
 500 | 8460

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know \_\_\_\_\_ NA  
 Spur Dike \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know \_\_\_\_\_ NA  
 Other \_\_\_\_\_ Yes  No \_\_\_\_\_ Don't know \_\_\_\_\_ NA

Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)

Material Silt/Clay  Sand  Gravel \_\_\_\_\_ Cobbles \_\_\_\_\_ Boulders \_\_\_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

- 1). main channel
- 2). piers
- 3). debris
- 4). pier scour
- 5). Lab
- 6). Rat
- 7). R. ab
- 8). main channel
- 9). Lab

Summary of Results

	Q <sub>100</sub> <u>25</u>	Q <sub>500</sub> <u>50</u>
Bridge flow evaluated	<u>2760</u>	<u>3549</u>
Flow depth at left abutment (yaLT), in feet	<u>4.6</u>	<u>4.6</u>
Flow depth at right abutment (yaRT), in feet	<u>3.0</u>	<u>4.4</u>
Contraction scour depth (y <sub>cs</sub> ), in feet	<u>9.1</u>	<u>12.5</u>
Pier scour depth (y <sub>ps</sub> ), in feet	<u>5.8</u>	<u>5.9</u>
Left abutment scour depth (y <sub>as</sub> ), in feet	<u>14.3</u>	<u>16.5</u>
Right abutment scour depth (y <sub>as</sub> ), in feet	<u>11.5</u>	<u>14</u>
Flow angle of attack	<u>30</u>	<u>30</u>

See Comments/Diagram for justification where required