

Dup OK-Rat

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 42020156 Date 10-16-12 Initials RFT Region (A B C D) C  
 Site \_\_\_\_\_ Location 4.7 mi S Lenoxx on 466 Ave  
 $Q_{100} =$  5600 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 5600 (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 92 ft. Flow angle at bridge = 18 ° Abut. Skew = 0 ° Effective Skew = 18 °  
 Width ( $W_2$ ) iteration = 92

Avg. flow depth at bridge,  $y_2$  iteration = 11.3

Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 87.5 ft\*  $q_2 = Q_2/W_2 =$  64.0 ft<sup>2</sup>/s

Bridge Vel,  $V_2 =$  5.7 ft/s Final  $y_2 = q_2/V_2 =$  11.3 ft  $\Delta h =$  0.7 ft

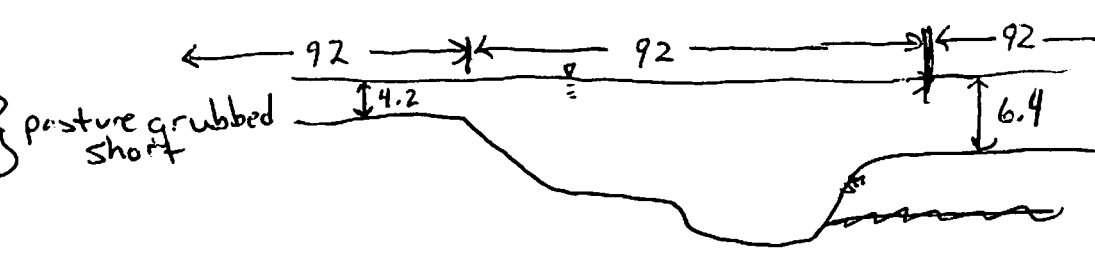
Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  11.9 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

Water Surface Elev. = no flow ft  
 Low Steel Elev. = 14.0 ft  
 $n$  (Channel) = .030  
 $n$  (LOB) = .027  
 $n$  (ROB) = .027  
 Pier Width = 1.67 ft  
 Pier Length = 1.67 ft  
 # Piers for 100 yr = 3



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  92 ft

Width of left overbank flow at approach,  $W_{lob} =$  92 ft Average left overbank flow depth,  $y_{lob} =$  4.2 ft

Width of right overbank flow at approach,  $W_{rob} =$  92 ft Average right overbank flow depth,  $y_{rob} =$  6.4 ft

**Live Bed Contraction Scour** (use if bed material is small cobbles or finer)

$x =$  9.22 From Figure 9  $W_2$  (effective) = 82.5 ft  $y_{cs} =$  10.1 ft

**Clear Water Contraction Scour** (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} >= 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006(q_2/y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} >= D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

PGRM: Contract

PGRM: CWCSNEW

**PIER SCOUR CALCULATIONS**

L/a ratio = 1

Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1

Froude # at bridge = 0.30

Using pier width  $a$  on Figure 11,  $\xi =$  7 Pier scour  $y_{ps} =$  5.8 ft

PGRM: Pier

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  4.2 ft right abutment,  $y_{aRT} =$  6.4 ft

Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through

Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  13.6 and  $\psi_{RT} =$  17.5

Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  13.6 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  17.5 ft

PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 42020156 Date \_\_\_\_\_ Initials \_\_\_\_\_ Region (A B C D)

Site \_\_\_\_\_ Location \_\_\_\_\_

$Q_{500} =$  10100 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X

Bridge discharge ( $Q_2$ ) = \_\_\_\_\_ (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 92 ft. Flow angle at bridge = 18 ° Abut. Skew = 0 ° Effective Skew = 18 °

Width ( $W_2$ ) iteration = 92

Avg. flow depth at bridge,  $y_2$  iteration = 15.2

Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 87.5 ft\*  $q_2 = Q_2/W_2 =$  115.4 ft<sup>2</sup>/s

Bridge Vel,  $V_2 =$  7.6 ft/s Final  $y_2 = q_2/V_2 =$  15.2 ft  $\Delta h =$  1.2 ft

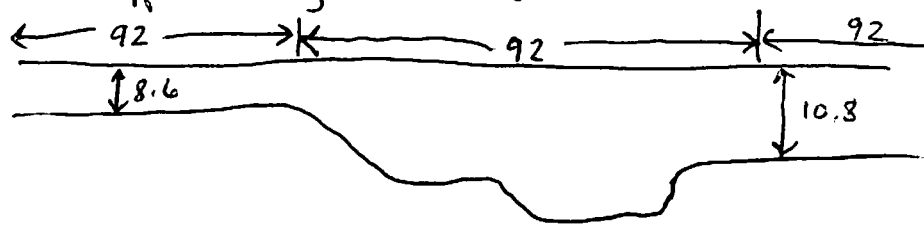
Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  16.3 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

*Handwritten note:*  $y_2$  for  $Q_{500}$  is approximately at the verge of road overflow

Water Surface Elev. = no flow ft  
 Low Steel Elev. = 14.0 ft  
 n (Channel) = .030  
 n (LOB) = .027  
 n (ROB) = .027  
 Pier Width = 1.67 ft  
 Pier Length = 1.67 ft  
 # Piers for 500 yr = 3 ft



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  92 ft

Width of left overbank flow at approach,  $W_{lob} =$  92 ft

Average left overbank flow depth,  $y_{lob} =$  8.6 ft

Width of right overbank flow at approach,  $W_{rob} =$  92 ft

Average right overbank flow depth,  $y_{rob} =$  10.8 ft

**Live Bed Contraction Scour** (use if bed material is small cobbles or finer)

$x =$  19.01 From Figure 9  $W_2$  (effective) = 82.5 ft  $y_{cs} =$  17.2 ft

**Clear Water Contraction Scour** (use if bed material is larger than small cobbles)

Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s

Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s

If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.

$D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$

Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.34 Using pier width a on Figure 11,  $\xi =$  7 Pier scour  $y_{ps} =$  5.9 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  8.6 ft right abutment,  $y_{aRT} =$  10.8 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  20.2 and  $\psi_{RT} =$  22.0  
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  20.2 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  22.0 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNEW

PRGM: Pic

PRGM: Abutment

Route 466 Ave Stream Long Creek MRM \_\_\_\_\_ Date \_\_\_\_\_ Initials \_\_\_\_\_  
 Bridge Structure No. 42020156 Location 4.7 mi S Lenox on 466 Ave  
 GPS coordinates: N 43° 16.599' taken from: USL abutment  centerline of ft MRM end \_\_\_\_\_  
W 96° 53.141' Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 75.39 sq. mi.

The average bottom of the main channel was 17.9 ft below top of guardrail at a point 34 ft from left abutment.  
 Method used to determine flood flows: \_\_\_\_\_ Freq. Anal. \_\_\_\_\_ drainage area ratio  regional regression equations.

**MISCELLANEOUS CONSIDERATIONS**

Flows	Q <sub>100</sub> = <u>5600</u>			Q <sub>500</sub> = <u>10100</u>		
Estimated flow passing through bridge	<u>5600</u>			<u>? 10100</u>		
Estimated road overflow & overtopping				<u>? 0</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Chance of Pressure flow		<input checked="" type="checkbox"/>		<input checked="" type="checkbox"/>		
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

Riprap at abutments?  Yes \_\_\_\_\_ No \_\_\_\_\_ Marginal \_\_\_\_\_  
 Evidence of past Scour?  Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know \_\_\_\_\_ possibly some contraction; a small amount of pier scour at center pier  
 Debris Potential? \_\_\_\_\_ High \_\_\_\_\_ Med  Low

Does scour countermeasure(s) appear to have been designed?

Riprap  Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know \_\_\_\_\_ NA  
 Spur Dike \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know  NA  
 Other \_\_\_\_\_ Yes \_\_\_\_\_ No \_\_\_\_\_ Don't know  NA

**Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)**

Material Silt/Clay  Sand \_\_\_\_\_ Gravel \_\_\_\_\_ Cobbles \_\_\_\_\_ Boulders \_\_\_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

Comments, Diagrams & orientation of digital photos

Str. No.  
 str. no. on bridge  
 approach from bridge  
 LOB from ditch  
 ROB from ditch  
 bridge from upstream  
 left abut.  
 rt. abut.  
 old pier scour hole

**Summary of Results**

	Q100	Q500
Bridge flow evaluated	<u>5600</u>	<u>10100</u>
Flow depth at left abutment (yaLT), in feet	<u>4.2</u>	<u>8.6</u>
Flow depth at right abutment (yaRT), in feet	<u>6.4</u>	<u>10.8</u>
Contraction scour depth (y <sub>c</sub> ), in feet	<u>10.1</u>	<u>17.2</u>
Pier scour depth (y <sub>p</sub> ), in feet	<u>5.8</u>	<u>5.9</u>
Left abutment scour depth (y <sub>a</sub> ), in feet	<u>13.6</u>	<u>20.2</u>
Right abutment scour depth (y <sub>a</sub> ), in feet	<u>17.5</u>	<u>22.0</u>
Flow angle of attack	<u>18°</u>	<u>18°</u>

See Comments/Diagram for justification where required