

OK RT

check pier pic

### SCOUR ANALYSIS AND REPORTING FORM

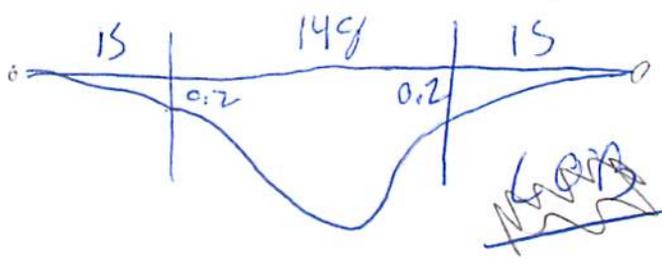
Bridge Structure No. 42020201 Date 5/25/12 Initials Pat Region (A B C D) C  
 Site \_\_\_\_\_ Location 9.1 mi S of Lennox on 466 Ave  
 $Q_{100} = 5840$  by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. \_\_\_\_\_  
 Bridge discharge ( $Q_2$ ) = \_\_\_\_\_ (should be  $Q_{100}$  unless there is a relief bridge, road overflow, or bridge overtopping)

#### Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method

Bridge Width = 148 ft. Flow angle at bridge = 0° Abut. Skew = 0° Effective Skew = 0°  
 Width ( $W_2$ ) iteration = 148 120 125  
 Avg. flow depth at bridge,  $y_2$  iteration = 8.9 9.8 9.6  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 125 ft\*  $q_2 = Q_2/W_2 = 46.7$  ft<sup>2</sup>/s  
 Bridge Vel,  $V_2 = 4.8$  ft/s Final  $y_2 = q_2/V_2 = 9.6$  ft  $\Delta h = 0.5$  ft  
 Average main channel depth at approach section,  $y_1 = \Delta h + y_2 = 10.1$  ft

\*NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$   
 If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0 ft  
 Low Steel Elev. = 14.5 ft 19.7  
 $n$  (Channel) = 0.030 -5.4  
 $n$  (LOB) = 0.030 14.5  
 $n$  (ROB) = 0.030  
 Pier Width = 3 ft  
 Pier Length = 3 ft  
 # Piers for 100 yr = 2 ft



#### CONTRACTION SCOUR

Width of main channel at approach section  $W_1 = 148$  ft  
 Width of left overbank flow at approach,  $W_{lob} = 15$  ft Average left overbank flow depth,  $y_{lob} = 0.2$  ft  
 Width of right overbank flow at approach,  $W_{rob} = 15$  ft Average right overbank flow depth,  $y_{rob} = 0.2$  ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x = 2.47$  From Figure 9  $W_2$  (effective) = 119 ft  $y_{cs} = 3$  ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{100}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} > 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2/y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} > D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

#### PIER SCOUR CALCULATIONS

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 = 1$   
 Froude # at bridge = 0.21 Using pier width  $a$  on Figure 11,  $\xi = 10.7$  Pier scour  $y_{ps} = 9.8$  ft

#### ABUTMENT SCOUR CALCULATIONS

Average flow depth blocked by: left abutment,  $y_{aLT} = 0.2$  ft right abutment,  $y_{aRT} = 0.2$  ft  
 Shape coefficient  $K_1 = 1.00$  for vertical-wall,  $0.82$  for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} = 1$  and  $\psi_{RT} = 1$   
 Left abutment scour,  $y_{as} = \psi_{LT} (K_1/0.55) = 1$  ft Right abutment scour  $y_{as} = \psi_{RT} (K_1/0.55) = 1$  ft

PGRM: "RegionA", "RegionB", "RegionC", or "RegionD"

PGRM: Contract

PGRM: CWC/SNEW

PGRM: Pier

PGRM: Abutment

**SCOUR ANALYSIS AND REPORTING FORM**

Bridge Structure No. 42020201 Date 5/25/12 Initials Rai Region (A B C D) D  
 Site \_\_\_\_\_ Location 9.1 mi S of Lennox on 466 Ave  
 $Q_{500} =$  11200 by: drainage area ratio \_\_\_\_\_ flood freq. anal. \_\_\_\_\_ regional regression eq. X  
 Bridge discharge ( $Q_2$ ) = 11200 (should be  $Q_{500}$  unless there is a relief bridge, road overflow, or bridge overtopping)

**Analytical Procedure for Estimating Hydraulic Variables Needed to Apply Method**

Bridge Width = 146 ft. Flow angle at bridge = 0 ° Abut. Skew = 0 ° Effective Skew = 0 °  
 Width ( $W_2$ ) iteration = 1

Avg. flow depth at bridge,  $y_2$  iteration = \_\_\_\_\_  
 Corrected channel width at bridge Section =  $W_2$  times cos of flow angle = 146 ft\*  $q_2 = Q_2/W_2 =$  75.7 ft<sup>2</sup>/s

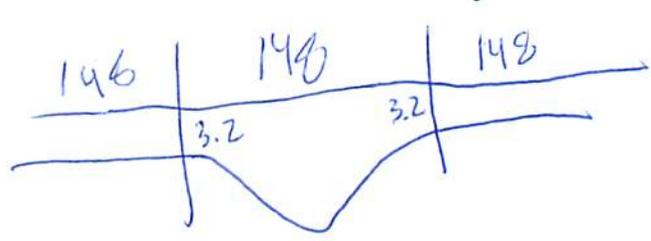
Bridge Vel,  $V_2 =$  6.2 ft/s Final  $y_2 = q_2/V_2 =$  12.3 ft  $\Delta h =$  0.9 ft

Average main channel depth at approach section,  $y_1 = \Delta h + y_2 =$  13.1 ft

\* NOTE: repeat above calculations until  $y_2$  changes by less than 0.2 Effective pier width =  $L \sin(q) + a \cos(q)$

If  $y_2$  is above LS, then account for Road Overflow using PRGM: RDOVREGA, RDOVREGB, RDOVREGC, or RDOVREGD.

Water Surface Elev. = 0 ft  
 Low Steel Elev. = 14.6 ft  
 n (Channel) = 0.030  
 n (LOB) = 0.030  
 n (ROB) = 0.030  
 Pier Width = 3 ft  
 Pier Length = 3 ft  
 # Piers for 500 yr = 2



**CONTRACTION SCOUR**

Width of main channel at approach section  $W_1 =$  148 ft  
 Width of left overbank flow at approach,  $W_{lob} =$  146 ft Average left overbank flow depth,  $y_{lob} =$  3.2 ft  
 Width of right overbank flow at approach,  $W_{rob} =$  144 ft Average right overbank flow depth,  $y_{rob} =$  3.2 ft

Live Bed Contraction Scour (use if bed material is small cobbles or finer)  
 $x =$  3.16 From Figure 9  $W_2$  (effective) = 142 ft  $y_{cs} =$  3.7 ft

Clear Water Contraction Scour (use if bed material is larger than small cobbles)  
 Estimated bed material  $D_{50} =$  \_\_\_\_\_ ft Average approach velocity,  $V_1 = Q_{500}/(y_1 W_1) =$  \_\_\_\_\_ ft/s  
 Critical approach velocity,  $V_c = 11.17 y_1^{1/6} D_{50}^{1/3} =$  \_\_\_\_\_ ft/s  
 If  $V_1 < V_c$  and  $D_{50} \geq 0.2$  ft, use clear water equation below, otherwise use live bed scour equation above.  
 $D_{c50} = 0.0006 (q_2 / y_1^{7/6})^3 =$  \_\_\_\_\_ ft If  $D_{50} \geq D_{c50}$ ,  $\chi = 0.0$   
 Otherwise,  $\chi = 0.122 y_1 [q_2 / (D_{50}^{1/3} y_1^{7/6})]^{6/7} - y_1 =$  \_\_\_\_\_ From Figure 10,  $y_{cs} =$  \_\_\_\_\_ ft

**PIER SCOUR CALCULATIONS**

L/a ratio = 1 Correction factor for flow angle of attack (from Table 1),  $K_2 =$  1  
 Froude # at bridge = 0.31 Using pier width a on Figure 11,  $\xi =$  10.7 Pier scour  $y_{ps} =$  9 ft

**ABUTMENT SCOUR CALCULATIONS**

Average flow depth blocked by: left abutment,  $y_{aLT} =$  3.2 ft right abutment,  $y_{aRT} =$  3.2 ft  
 Shape coefficient  $K_1 =$  1.00 for vertical-wall, 0.82 for vertical-wall with wingwalls, 0.55 for spill-through  
 Using values for  $y_{aLT}$  and  $y_{aRT}$  on figure 12,  $\psi_{LT} =$  11.9 and  $\psi_{RT} =$  11.9  
 Left abutment scour,  $y_{as} = \psi_{LT}(K_1/0.55) =$  11.9 ft Right abutment scour  $y_{as} = \psi_{RT}(K_1/0.55) =$  11.9 ft

PRGM: "RegionA", "RegionB", "RegionC", or "RegionD"

PRGM: Contract

PRGM: CWCNSWE

PRGM: Pie

PRGM: Abutment

Route 466 Ave Stream Saddle Ck MRM Date 5/25/12 Initials RAT  
 Bridge Structure No. 42020201 Location 9.1 mi S of Lennox on 466 Ave  
 GPS coordinates: N 43° 12' 46.9" taken from: USL abutment  centerline of fl MRM end \_\_\_\_\_  
W 96° 53' 7.2" Datum of coordinates: WGS84  NAD27 \_\_\_\_\_

Drainage area = 96.98 sq. mi.  
 The average bottom of the main channel was 19.6 ft below top of guardrail at a point 60 ft from left abutment.  
 Method used to determine flood flows: \_\_\_ Freq. Anal. \_\_\_ drainage area ratio  regional regression equations.

**MISCELLANEOUS CONSIDERATIONS**

Flows	Q <sub>100</sub> = <u>5840</u>			Q <sub>500</sub> = <u>11200</u>		
Estimated flow passing through bridge	<u>5840</u>			<u>11200</u>		
Estimated road overflow & overtopping	<u>0</u>			<u>0</u>		
Consideration	Yes	No	Possibly	Yes	No	Possibly
Chance of overtopping		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Chance of Pressure flow		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Armored appearance to channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	
Lateral instability of channel		<input checked="" type="checkbox"/>			<input checked="" type="checkbox"/>	

8/24  
 2 | 1060  
 5 | 2740  
 10 | 4490  
 25 | 7420  
 50 | 10200  
 100 | 13500  
 500 | 23500

Riprap at abutments? \_\_\_ Yes \_\_\_ No  Marginal  
 Evidence of past Scour?  Yes \_\_\_ No \_\_\_ Don't know contraction pie  
 Debris Potential? \_\_\_ High \_\_\_ Med  Low

5/22  
 2 | 304  
 5 | 904  
 10 | 1590  
 25 | 2600  
 50 | 4190  
 100 | 5840  
 500 | 11200

Does scour countermeasure(s) appear to have been designed?  
 Riprap \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Spur Dike \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA  
 Other \_\_\_ Yes  No \_\_\_ Don't know \_\_\_ NA

**Bed Material Classification Based on Median Particle Size (D<sub>50</sub>)**

Material Silt/Clay  Sand  Gravel \_\_\_ Cobbles \_\_\_ Boulders \_\_\_  
 Size range, in mm <0.062 0.062-2.00 2.00-64 64-250 >250

**Comments, Diagrams & orientation of digital photos**

- 1). main channel
- 2). R. ab
- 3). Piers
- 4). L ab
- 5). Lab
- 6). Pier Scour
- 7). ROPS
- 8). Main channel
- 9). Left Main channel
- 10). LOPS

**Summary of Results**

	Q <sub>100</sub>	Q <sub>500</sub>
Bridge flow evaluated	<u>5840</u>	<u>11200</u>
Flow depth at left abutment (yaLT), in feet	<u>0.2</u>	<u>3.2</u>
Flow depth at right abutment (yaRT), in feet	<u>0.2</u>	<u>3.2</u>
Contraction scour depth (y <sub>cs</sub> ), in feet	<u>3</u>	<u>3.7</u>
Pier scour depth (y <sub>ps</sub> ), in feet	<u>6.8</u>	<u>9</u>
Left abutment scour depth (y <sub>as</sub> ), in feet	<u>1</u>	<u>11.9</u>
Right abutment scour depth (y <sub>as</sub> ), in feet	<u>1</u>	<u>11.9</u>
Flow angle of attack	<u>0</u>	<u>0</u>

See Comments/Diagram for justification where required